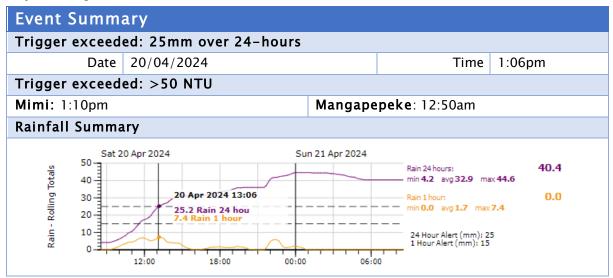




## **Trigger Inspection Report**

This report summarises the monitoring required under Consent Condition SED.11(b) and relevant Project Management Plans.



Visual Inspection SED.11b (i		
Area	Comments	
Mimi Stream	As expected for the rainfall	
Mangapepeke Stream	As expected for the rainfall	
SRP-1	SRP working well, no concerns	
SRP-6D	SRP working well, no concerns	
SCY-SRP	SRP working well, no concerns	
SRP4700E	SRP working well, no concerns	
DEB-F12-1	Catchment cut off & directed to SRP 2920N	
SRP-2920N	Not discharging at time of inspection	
SRP-3180S	Batch dosed & decant raised	
DEB-F13	SRP working well, no concerns	
DEB-3980E	SRP working well, no concerns	

## moling ESC Davi

Manual Sampiir	Aanual Sampling: ESC Devices SED. (1)				
Device Name	рН		NTU		Discharging?
Device Maine	Inlet	Outlet	Inlet	Outlet	Discharging
SRP-1	7.72	7.75	173	71.3	Yes
SCY-SRP	7.13	7.07	48.4	31.3	Yes
SRP-6D	6.72	7.62	122	44.7	Yes
SRP4700E	7.41	7.28	700	44.2	Yes
SRP2920N	7.25	7.42	723	244	No
SRP3180S	7.21	7.21	880	840	Yes
DEB-F13	7.6	7.53	367	286	Yes
DEB3980E	8.26	8.16	96.7	85.3	Yes

## In-Stream Sampling (WQ1 - WQ5)

In-stream samples are collected at the earliest convenience, once water levels recede and it is safe to do so. Samples are analysed at an accredited third-party laboratory.

Location	NTU	рН	<b>TSS</b> (g/m <sup>3</sup> )
WQ3 Mimi Upstream	77	6.9	220
WQ5 Mimi Downstream	210	6.9	630
WQ1 Mangapepeke Upstream	153	6.8	620
WQ2b Mangapepeke Downstream	173	6.9	370
Comments			

WQ4 Static sampler was missing from the instream sampler.

## Sediment Deposition Monitoring

Sediment deposition data is collected once it is safe to do so. All measurements are in mm. Data collected on 22/04/2024.

Measured 22/04/2024 Baseline Stake top to ground level Variation from previous reading Variation form baseline (+ or -)   ST1(1) 906 932 -1 -26   ST1(2) 928 905 14 23   ST1(3) 923 895 5 28   ST1(4) 926 901 1 25   ST1(5) 900 926 -25 -26   ST1(ave) 917 912 -1 5   ST2(1) 1160 1150 2 10   ST2(2) 1190 1181 -1 9   ST2(3) 1295 1264 2 31   ST2(4) 1323 1310 -1 13   ST3(2) 1090 1040 6 50   ST3(2) 1090 1040 6 50   ST3(3) 1131 1147 3 -16   ST3(4) 1142 1126 0 16   ST3(5) 1100	-	1 - 1 -				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			Baseline	to ground	from previous	fom baseline
ST1(3) 923 895 5 28   ST1(4) 926 901 1 25   ST1(5) 900 926 -25 -26   ST1(ave) 917 912 -1 5   ST2(1) 1160 1150 2 10   ST2(2) 1190 1181 -1 9   ST2(3) 1295 1264 2 31   ST2(4) 1323 1310 -1 13   ST2(5) 1290 1290 1 0   ST3(2) 1090 1040 6 50   ST3(3) 1131 1147 3 -16   ST3(4) 1142 1126 0 16   ST3(5) 1100 1108 -8 -8   ST3(6) 1222 1237 1 -15   ST3(6) 1222 1237 1 -15   ST4(1) 1240 1225 -1 15   ST4(2		ST1(1)	906	932	-1	-26
ST1(4)926901125ST1(5)900926-25-26ST1 (ave)917912-15ST2(1)11601150210ST2(2)11901181-19ST2(3)12951264231ST2(4)13231310-113ST2(5)1290129010ST2(ave)12521239113ST3(1)11331123410ST3(2)10901040650ST3(3)113111473-16ST3(3)113111473-16ST3(4)11421126016ST3(5)11001108-8-8ST3(6)122212371-15ST3(7)1380137199ST3(ave)1171116527ST4(1)12401225-115ST4(2)12721259-1613ST4(3)12041186-118ST4(4)13421321-721ST4(5)12801219761ST4(6)12431226317ST4(ave)12641239-324ST5(1)965933132ST5(3)110010491451ST5(4)13601322-238ST5(5)1223 <td< td=""><td></td><td>ST1(2)</td><td>928</td><td>905</td><td>14</td><td>23</td></td<>		ST1(2)	928	905	14	23
ST1(5)900926 $-25$ $-26$ ST1 (ave)917912-15ST2(1)11601150210ST2(2)11901181-19ST2(3)12951264231ST2(4)13231310-113ST2(5)1290129010ST3(2)10901040650ST3(2)10901040650ST3(3)113111473-16ST3(4)11421126016ST3(5)11001108-8-8ST3(6)122212371-15ST3(7)1380137199ST3(ave)1171116527ST4(1)12401225-115ST4(2)12721259-1613ST4(3)12041186-118ST4(4)13421321-721ST4(5)12801219761ST4(6)12431226317ST4(6)12431226317ST5(1)965933132ST5(3)110010491451ST5(4)13601322-238ST5(5)12231168-255ST5(6)13911370021		ST1(3)	923	895	5	28
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ST1(4)	926	901	1	25
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ST1(5)	900	926	-25	-26
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ST1 (ave)	917	912	-1	5
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ST2(1)	1160	1150	2	10
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ST2(2)	1190	1181	-1	9
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ST2(3)	1295	1264	2	31
ST2(ave) 1252 1239 1 13   ST3(1) 1133 1123 4 10   ST3(2) 1090 1040 6 50   ST3(2) 1090 1040 6 50   ST3(3) 1131 1147 3 -16   ST3(4) 1142 1126 0 16   ST3(5) 1100 1108 -8 -8   ST3(6) 1222 1237 1 -15   ST3(7) 1380 1371 9 9   ST3(ave) 1171 1165 2 7   ST4(1) 1220 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   <		ST2(4)	1323	1310	-1	13
ST3(1) 1133 1123 4 10   ST3(2) 1090 1040 6 50   ST3(2) 1090 1040 6 50   ST3(3) 1131 1147 3 -16   ST3(4) 1142 1126 0 16   ST3(5) 1100 1108 -8 -8   ST3(6) 1222 1237 1 -15   ST3(7) 1380 1371 9 9   ST3(ave) 1171 1165 2 7   ST4(1) 1240 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24		ST2(5)	1290	1290	1	0
ST3(2) 1090 1040 6 50   ST3(3) 1131 1147 3 -16   ST3(4) 1142 1126 0 16   ST3(5) 1100 1108 -8 -8   ST3(6) 1222 1237 1 -15   ST3(7) 1380 1371 9 9   ST3(ave) 1171 1165 2 7   ST4(1) 1240 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39		ST2(ave)	1252	1239	1	13
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		ST3(1)	1133	1123	4	10
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ST3(5) 1100 1108 -8 -8   ST3(5) 1222 1237 1 -15   ST3(6) 1222 1237 1 -15   ST3(7) 1380 1371 9 9   ST3(ave) 1171 1165 2 7   ST4(1) 1240 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51 <t< td=""><td></td><td>ST3(3)</td><td>1131</td><td>1147</td><td>3</td><td>-16</td></t<>		ST3(3)	1131	1147	3	-16
ST3(6) 1222 1237 1 -15   ST3(6) 1222 1237 1 -15   ST3(7) 1380 1371 9 9   ST3(ave) 1171 1165 2 7   ST4(1) 1240 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(5) 1280 1219 7 61   ST4(5) 1280 1219 7 61   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51 <t< td=""><td></td><td>ST3(4)</td><td>1142</td><td>1126</td><td>0</td><td>16</td></t<>		ST3(4)	1142	1126	0	16
ST3(7) 1380 1371 9 9   ST3(ave) 1171 1165 2 7   ST4(1) 1240 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST3(5)	1100	1108	-8	-8
ST3(ave) 1171 1165 2 7   ST4(1) 1240 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST3(6)	1222	1237	1	-15
ST4(1) 1240 1225 -1 15   ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST3(7)	1380	1371	9	9
ST4(2) 1272 1259 -16 13   ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST3(ave)	1171	1165	2	7
ST4(3) 1204 1186 -1 18   ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST4(1)	1240	1225	-1	15
ST4(4) 1342 1321 -7 21   ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST4(2)	1272	1259	-16	13
ST4(5) 1280 1219 7 61   ST4(6) 1243 1226 3 17   ST4(6) 1243 1226 3 17   ST4(eve) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST4(3)	1204	1186	-1	18
ST4(6) 1243 1226 3 17   ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST4(4)	1342	1321	-7	21
ST4(ave) 1264 1239 -3 24   ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST4(5)	1280	1219	7	61
ST5(1) 965 933 1 32   ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST4(6)	1243	1226	3	17
ST5(2) 979 940 0 39   ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST4(ave)	1264	1239	-3	24
ST5(3) 1100 1049 14 51   ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST5(1)	965	933	1	32
ST5(4) 1360 1322 -2 38   ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST5(2)	979	940	0	39
ST5(5) 1223 1168 -2 55   ST5(6) 1391 1370 0 21		ST5(3)	1100	1049	14	51
ST5(6) 1391 1370 0 21		ST5(4)	1360	1322	-2	38
		ST5(5)	1223	1168	-2	55
ST5(ave) 1170 1130 2 39		ST5(6)	1391	1370	0	21
		ST5(ave)	1170	1130	2	39



