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Action	Name	Signed	Date
Prepared by	Graeme Ridley,		26 March 2012
	Director, (Ridley Dunphy	65. Riolley	
	Environmental Limited)		
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#### 1 **Introduction and Project Description**

The purpose of this report is to describe the methods and practices to be implemented to minimise the effects of sediment generation and yield on the aquatic receiving environments associated with the MacKays to Peka Peka Project (the "Project"). This Erosion and Sediment Control Plan (ESCP) is prepared to support the assessment of environmental effects (AEE) and to provide guidance to the Mackays to Peka Peka Project Team<sup>1</sup>. Further this ESCP, while referred to as an ESCP, also provides environmental guidance on a number of other activities associated with the Project including but not limited to dust management, concrete works and the use of bentonite.

The Project sector diagram is included in Appendix H.A of this ESCP, and provides an overview of the extent and works for the Project. This ESCP covers all sectors of the Project. For the purposes of the construction methodology and this ESCP, the Project is split into 4 specific sectors referred to as follows:

#### Sector One Raumati South

This sector includes chainage 1900 to 4500 and includes the following specific construction stages:

- Poplar Avenue (POP)
- Poplar Avenue-Raumati Road (POP-RAU)

#### **Sector Two** Raumati / Paraparaumu

This sector includes chainage 4500 to 8300 and includes the following specific construction stages:

- Raumati Road/Wharemauku Stream/Ihakara Street (RAU-IHA)
- Ihakara Street/Wharemauku Stream-Kāpiti Road (IHA-KAP)
- Kāpiti Road-Mazengarb Road (KAP-MAZ)
- Mazengarb Road-plus 300m (MAZ-OT)

#### Sector Three Otaihanga / Waikanae

This sector includes chainage 8300 to 12400 and includes the following specific construction stages

- Mazengarb Road-plus 300m to-Otaihanga Road (MAZ-OT)
- Otaihanga Road-Waikanae River (OT-WAI)
- Waikanae River-Te Moana Road (WAI-TEM)

<sup>&</sup>lt;sup>1</sup> This Management Plan refers to the Project team as carrying out works on behalf of and as contracted by NZTA. The NZTA is the requiring authority and the consent holder.

Te Moana Road-plus 600m (TEM-NGA)

#### Sector Four Waikanae North

This sector includes chainage 12400 to 18050 and includes the following specific construction stages

- Te Moana Road-plus 600m to Ngarara Road
- Ngarara Road-Peka Peka (NGA-PP)
- Peka Peka Interchange (PP)

For more detailed Project description reference should be made to Part D, Chapters 7 and 8, Volume 2 of the the AEE that supports the Project. Further, when reading this ESCP, key reference should also be made to the Construction Methodology Report (Technical Report 4, Volume 3).

The construction methodology and ESCP for the Project is intended as a realistic and feasible methodology from which the anticipated effects on the environment of these activities can be identified. It is important that this ESCP is read in conjunction with the construction methodology with the methodology itself also providing a critical feature of the erosion and sediment control methodology.

The Project has been developed as an Alliance Project (refer to Part A, Chapter 1, Volume 2 of the AEE for further information) and hence contractor input into this ESCP has occurred from early in the consenting process. This has ensured that the ESCP provides for an achievable approach while also ensuring environmental objectives are achieved. The Project team consists of the NZ Transport Agency (NZTA), Kāpiti Coast District Council (KCDC), Fletcher Construction Limited, Higgins Contractors Limited and Beca Carter Hollings and Ferner Limited. Sub-partners of the Project team include Goodman Contractors Limited, Boffa Miskell Limited and Incite Limited.

The Project is anticipated to take 5 years to construct, and will be able to be undertaken on a number of fronts or work faces, such that many elements of the Project will be undertaken concurrently. During construction, erosion and sediment control measures will be put in place to minimise potential adverse effects by utilising measures which meet industry best practice guidelines such as reflected by Greater Wellington Regional Council's Erosion and Sediment Control Guidelines for the Wellington Region, September 2002 (Wellington Guidelines). The draft NZTA Erosion and Sediment Control Standard for State Highway Infrastructure dated August 2010 (NZTA Draft Standard) has also been considered. It is expected, as is the case for projects of this size and nature, that site and activity specific erosion and sediment control plans will be further enhanced which will follow the general principles of this ESCP. These are referred to as Construction Erosion and Sediment Control Plans (CESCPs). This will enable the Project Team and Greater Wellington Regional Council to have further input into the methodologies implemented.

The ESCP provides for an overview of the erosion and sediment management techniques and measures that will be used within the Project, provides specific examples throughout and also outlines methodologies and management techniques that will apply and will achieve the necessary environmental objectives. This ESCP also includes details on dust management techniques to be utilised within the Project.

Once the erosion and sediment controls are in place, ongoing site monitoring by the Project team and the NZTA representatives will occur to ensure that the proposed erosion and sediment control measures have been installed correctly, and are functioning effectively throughout the duration of the works.

Stormwater management during the construction phase is a separate and unique stage in the water management of the Expressway. It occurs after earthworks activities have ceased in an area, and erosion and sediment controls are no longer appropriate, but before long term operational stormwater controls are in place. Stormwater management measures are proposed for impervious construction areas and the pavement of the constructed Expressway. Reference should be made to the Construction Methodology Report (Technical Report 4, Volume 3).

There are 9 construction yards proposed along the route of the Project with the details of these provided within the Construction Methodology Report (Technical Report 4, Volume 3) and also outlined in Section 7.14 of this ESCP.

Site establishment activities will include site clearance, ground preparation, and establishing erosion and sediment control measures prior to any construction activities occurring. Upon completion of the works, it is expected that the erosion and sediment controls will be removed and any rehabilitation undertaken as necessary.

During construction, a variety of measures will be used to manage construction activities and ensure that construction is being undertaken in a way that avoids, minimises or mitigates effects on the environment. This will include specific mitigation measures, environmental monitoring and environmental auditing. To assist this process, and ensure that the Project team meets both the Designation and resource consent requirements and the NZTAs requirements, in addition to this ESCP a Construction Environmental Management Plan (CEMP, Volume 4 of the AEE) has been prepared for the Project.

The CEMP (Volume 4 of the AEE) is an overarching document which supports the applications for resource consents and designations and is intended to be used by the construction contractors to manage the environmental effects of the Project. The principles and general approach to managing the environmental effects are set out in the main body of the document. The management of specific effects (e.g. construction air quality, noise, vibration etc.) are detailed more particularly within a suite of environmental management plans (sub-plans) that form the appendices to the CEMP (Volume 4 of the AEE).

The Project team will be required to undertake all construction activities on site in accordance with the provisions of the relevant management plans as part of their contractual arrangements.

The CEMP (Volume 4 of the AEE) will be reviewed after confirmation of the resource consent and designation conditions and will be revised in accordance with these conditions. The CEMP (Volume 4 of the AEE) and the sub-plans will be updated, with the necessary approval, throughout the course of the Project to reflect material changes associated with changes to construction techniques or the natural environment.

The Project team will also be required to develop a CESCP, as a subset of the ESCP as detailed above, for each specific package of work, that is consistent and in accordance with the CEMP (Volume 4 of the AEE) and this ESCP, and submit to the Greater Wellington Regional Council for certification prior to undertaking the construction work. Importantly, the Ecological Impact Assessment (Technical Report 26, Volume 3) should also be referenced when reading this ESCP.

## 2 Design philosophy and principles

The following section outlines a generic site description and sets a context for the development of this ESCP.

The site generally has peat soils overlaying sand layers in addition to areas of sand dominant soils. Peat is essentially an accumulation of partially decayed vegetation matter that has formed when plant material is inhibited from decaying fully by the acidic conditions. Peat is soft and easily compressed and under pressure, water in the peat is forced out. From this ESCP perspective it is important to recognise that the peat has a high water table which can limit the type of the erosion and sediment controls utilised. Further the areas of sand dominant soils in many locations along the Alignment create an environment that requires specific management from an erosion and sediment control perspective.

The receiving environment values associated with the site include a range of both fresh water and coastal ecological and amenity values. It is important that erosion and sediment control options recognise these values and manage the discharge of sediment accordingly. This ESCP builds on the areas of significance as identified within the Ecological Impact Assessment (Technical Report 26, Volume 3).

Higher risk areas are identified as those locations adjacent to, or connected to, freshwater streams. These higher risk areas are protected through the minimisation of discharges and implementation of erosion and sediment control measures over and above those typically implemented. These areas focus around the existing values of the freshwater stream systems along the Project and in particular focuses on the Waikanae River and the Te Harakeke/Kawakahia Wetland. The Te Harakeke/Kawakahia wetland is the ultimate receiving environment for any discharge from the

Paetawa Drain, Ngarara Drain, Kakariki Stream and Ngarara Stream with this wetland considered to be ecologically nationally important. The Waimeha Estuary and Wharemauku Stream Estuary are also recognised as high value receiving environments. Reference should be made to the Ecological Impact Assessment (Technical Report 26, Volume 3) for specific and full details.

The Waikanae River is defined in detail within the Ecological Impact Assessment (Technical Report 26, Volume 3) and is recognised as interacting with the underlying gravel aquifer where there are large flow losses to groundwater and gains from groundwater along certain reaches.

As detailed within Section 1.0 of this ESCP more specific and enhanced erosion and sediment control plans, referred to as CESCPs, will be developed for each specific area and activity prior to construction activities commencing.

On most earthwork sites including Expressway development, sediment generally arises from the bulk earthworks phase of operations because of the area exposed by these works and the time required to undertake the works. For this Project, bulk earthworks will be undertaken and accordingly the soil types and the construction methodology are both considered of significant influence. There are also other land disturbing activities proposed by the Project that need to be taken into account when considering the potential generation and discharge of sediment. In particular, these include stream diversion and culvert placement activities. Because of the extent of these types of works required as part of this Project, and because of the immediate delivery of any sediment yield into the aquatic environment, from an environmental perspective these works could be considered to be higher risk than the works confined directly to the land with effects wider than the Project footprint which need to be considered.

By way of background, it is important to recognise that erosion is the process whereby the land surface is worn away by the action of water, wind, ice or other geological processes. The resultant displaced material is known as sediment with sediment yields being the sediment which leaves a particular control measure. Sedimentation is the deposition of this eroded material. Accelerated erosion is primarily caused by human activities and is a much more rapid process then natural erosion.

Through the erosion process, soil particles are dislodged, generally by rainfall and increased surface water flow. As rain falls, water droplets concentrate and form small flows. The combined energy of the rain droplets and the concentrated flows has the potential to dislodge soil particles. The amount of sediment generated depends on the erodibility of the soil, the amount of energy created by the intensity of the rainfall event and the site conditions, for example the slope and the slope length of the site. In general, the steeper the site and the longer the flow lengths, the more energy will be created. Any reduction of energy will reduce the erosion and sediment generation. The Project slopes are considered very "gentle" and do not represent a significant issue from an erosion perspective. The Universal Soil Loss Equation (USLE) calculations and supporting plans

within Appendix H.F and H.G of this ESCP highlight the Project slope classifications. The peat soils contain a relatively high proportion of clay and silt particles and therefore once in suspension can be take long periods to settle out. With respect to the sand soils, while they erode easily, due to larger particle size they settle within the water column relatively quickly. Therefore it is important for both of these soil types that erosion is minimised in the first instance to ensure sediment generation and yield is also minimised.

Erosion and sediment control measures are used to minimise the effects of earthworks on receiving environments. Erosion control is based on the practical prevention of sediment generation in the first instance. If erosion control is effective and sediment generation is consequently minimised, then the reliance on the sediment control process is not as significant.

Sediment control, on the other hand, refers to management of the sediment after it is generated. It is inevitable that some sediment will be generated through earthworks, even with erosion control measures in place. Sediment control is designed to capture this sediment and minimise any resultant discharge.

Rather than only relying on sediment control measures alone, a significant reduction in erosion on site will result in far less sediment being generated, required to be treated and discharged from the control measures.

The erosion and sediment control measures for the Project are designed to minimise the extent of soil erosion and any resultant sediment yield. The proposed erosion and sediment control measures have been designed in accordance with the Wellington Guidelines and have also considered the NZTA Draft Standard. These measures are detailed later within this report. It is noted that the NZTA Draft Standard provides no specific management techniques or direction with respect to peat soils and while erosion and sediment control measures are to be implemented these have been adapted for the soil types that will be encountered. The NZTA Draft Standard outlines the issues associated with wind erosion and dust management and these have been considered, and incorporated as relevant, for the management of the sand soils. The approach taken with the erosion and sediment controls is that in many circumstances, measures exceeding the Wellington Guidelines are proposed where there is a greater perceived or recognised environmental risk associated with undertaking the works.

The following erosion and sediment control principles will apply.

## **General Principles**

1. Erosion and sediment control measures will be undertaken and implemented with a hierarchy and priority order as follows:

- a. Avoidance of effects will be the first priority. Any discharge locations will be carefully selected and any streamworks will only be undertaken where they are a necessary component of the Project construction.
- b. Erosion control will be a priority in all circumstances by preventing sediment generation through a range of structural (physical measures) and non structural (methodologies and construction sequencing) means.
- c. Sediment Retention Ponds (SRPs) will be utilised, but given the nature of the Project, the soil types, the flat contour and the generally high groundwater table, other alternative devices also provide viable and effective solutions. Chemical treatment will be utilised, however, this will be on a limited basis as a risk management tool. Based on research undertaken it is confirmed that there is the ability to chemically treat sediment laden water to help achieve the necessary water quality on an "as required" basis. Chemical treatment will therefore be utilised as a risk management tool and will be based around the use of polyacrylamide contained within flocculant socks. Priority of controls will then be decanting earth bunds, super silt fences and silt fences. Various innovative products may also be used and could include measures such as filter socks.
- 2. The earthwork methodologies are based on two key activities being peat replacement and peat preload. These two activities have specific methodologies and processes which will be followed. Drawings CV CM 240 to 243 and CV CM 244 in Appendix H.C (Pre Load Drawing) and H.D (Peat Replacement Drawing), in the Management Plan Appendices, Appendix H, Volume 5 outline the details.
- 3. The erosion and sediment control methodologies and drawings provided within this ESCP are based upon methodologies and measures using the Wellington Guidelines and the NZTA Draft Standard as a minimum standard, but also incorporate some procedures and facilities that surpass these standards including items such as pumping and peat replacement methodologies. Through the implementation phase of the Project, it is recognised that there will be room for innovation and alternative means of achieving the same environmental objectives.
- 4. Preliminary design drawings are provided within this ESCP in Appendix H.I (ESCP Design Drawings). As mentioned in Section 1.0 of this ESCP, it is expected that site and activity specific erosion and sediment control plans will be developed which will follow the general principles of this ESCP and will include erosion and sediment control drawings.
- 5. Erosion and sediment control measures will be implemented in accordance with this ESCP and are based upon the appropriate approval of site specific erosion and sediment control measures referred to as CESCP's throughout the Project implementation. The principles and practices detailed within this ESCP will be reflected within the CESCPs and, as a result, will ensure that

any sediment yields, and associated effects, of the earthworks activities are negligible and are all managed within the earthworks footprint of the Project. The implementation of CESCPs will allow for future innovation, flexibility and practicality of approach to erosion and sediment control and in doing this will ensure that the Project continues to adapt appropriately to changing conditions. With the implementation of the CESCPs the construction related sediment controls must remain in place until all earthworks for that sub catchment are stabilised, and permanent stormwater facilities for the corresponding catchment must be in place and operational prior to the impervious area of that sub catchment area reaching 80%.

- 6. Greater Wellington Regional Council places emphasis on a number of principles that apply to erosion and sediment control. While not forming part of the specific principles within the ESCP they are acknowledged and are included within Appendix H.J (Greater Wellington Regional Council and NZTA ESCP Principles) of this ESCP for reference purposes. The erosion and sediment control principles from the NZTA Draft Standard are also included within this Appendix.
- 7. No specific discharge water quality standards are proposed; however, the discharge from the Project is designed to avoid conspicuous change in the colour or visual clarity of the discharge (after reasonable mixing) in the receiving environment.
- 8. All erosion and sediment control devices should be located outside the 5% AEP flood level unless no other viable alternative exists. During construction activity and where it is considered to be the only option and devices are required within this flood level, then the placement of such a device will be undertaken with consideration of minimising catchment areas and ensuring more regular maintenance activities. All stock will be excluded, through fencing, from the area of works and the erosion and sediment control measures.
- 9. Peat removed will be temporarily stockpiled as part of the peat replacement process and will be utilised within the final Project footprint or transferred to eventual peat disposal sites. The location of these sites is detailed within the Construction Methodology Report (Technical Report 4, Volume 3). Three specific sites have been identified with the erosion and sediment control aspects of these sites the subject of existing consents or agreements outside the scope of this ESCP.

#### **Erosion Control Principles**

10. Cleanwater diversion channels have not been anticipated for the Project. However, if necessary, the CESCPs may specify cleanwater diversion channels, designed to cater for the 1% AEP rainfall event. The topographic nature of the site is such that there are very few areas where specific upslope cleanwater catchments are required to be diverted away from the works area. This will, however, be subject to ongoing monitoring and checks and if required then cleanwater diversions will be installed to a 1% AEP design standard. The 1% AEP design standard exceeds that recommended by the Wellington Guidelines and provides a level of

- certainty and risk management for these diversion channels which will operate to a much larger storm event.
- 11. Progressive and rapid stabilisation of disturbed areas utilising top soil (where necessary) and seed, mulch and geotextiles will be ongoing throughout the Project. Mulch will include hay/straw and wood which will be generated on site though the removal and mulching of existing vegetation as necessary. Stabilisation will apply particularly with respect to stockpiles and batter establishment. Stabilisation is designed for both erosion control and dust minimization. Where dust generation is the predominant issue then water carts will be utilised as the initial treatment option. This in particular applies to the batter slopes which will also be subject to stabilisation. For pre load activities short term batters (less than 6 months) will have a final layer of clean granular material, sub base course or mulch (straw, hay or wood) applied over sand to ensure no wind disturbance of the surface while longer term batter slopes (greater than 6 months) will have topsoil and grass established. For final cut slopes stabilisation using topsoil and grass from the top of the slope as the cut progresses will occur.
- 12. Flumes will be utilised in accordance with the Wellington Guidelines to safely transfer runoff from the top of batters to the bottom of the batter slopes and to ensure no scour of these batters occurs. These will be designed and implemented as per Drawings CV CM 248-251 provided in Appendix H.I (ESCP Design Drawings), Management Plan Appendices, Appendix H, Volume 5.
- 13. While most site access will be from existing roads, stabilised entrance ways will be established at all ingress and egress points of the site. No vehicles will leave the site unless tyres are clean and will not contribute excessive sediment, such as deposited sediment (not dust), onto road surfaces. Wheel wash facilities will be established only if necessary.

### **Sediment Control Principles**

- 14. All Sediment Retention Ponds (SRP) to be implemented will be based a minimum 2% volume criterion applied in relationship to catchment size (i.e. 2m3 SRP volume per 100m2 of contributing catchment). This criterion is consistent with the Wellington Guidelines and the NZTA Draft Standard.
- 15. Through the flocculation testing, it was recorded that the peat soils had fine colloidal particles which remained in suspension long enough to potentially create settling issues during treatment of sediment laden runoff. Flocculants were tested with effective results noted with the use of polyacrylamide which will be dosed via a "floc sock" where sediment laden water is passed over the sock to dissolve product and the floc sock size/number is customised for the flow rates. While this flocculant is proven to be successful, other chemical treatment options and design will continue to be explored throughout the Project as different conditions and in particular soil types are encountered.

- 16. Pumping of sediment laden runoff and groundwater during construction will be required at numerous periods during excavation works. These flows will be pumped to SRP's, to grass buffer zones or to temporary sediment retention devices such as turkey nests which will assist with retaining any sediment contained within the runoff. Further pumping will also be required with associated activities such as bridge construction. This pumping activity will also ensure discharges are to treatment devices. At all times the Project team will follow the "Permit to Pump system" as outlined in Appendix H.P (Permit to Pump System) of this ESCP. This is based on a standard audit process that ensures any dewatering and/or pumping is undertaken in accordance with appropriate Fletcher Construction procedures and environmental consideration.
- 17. Where established, SRP's for the treatment of construction related sediment laden runoff will be established as independent devices. The Project also includes the installation of a number of permanent stormwater wetland features (for permanent stormwater treatment from impervious surfaces) as detailed within drawings CV SW 100 to 394, Management Plan Appendices, Appendix H, Volume 5 and in Technical Report 22, Volume 3. Where practicalities allow, such permanent devices will be installed early in the Project and will be utilised to assist with the management of runoff from the Project. Where the permanent features are utilised, consideration will be given to pond depth and configuration to ensure that the eventual conversion of these to long term stormwater features can be undertaken appropriately. No existing natural wetlands will be used for primary treatment of construction related sediment discharge.
- 18. Any decanting earth bunds established will be based on a volume of 2% of the contributing catchment area with an ideal length to width ratio of 1:3. All spillways from the decanting earth bunds will be installed to ensure that they safely pass the 1% AEP rain event with low velocity and therefore minimal scour potential. Decanting earth bunds for the pre load activities will discharge to either a watercourse or a stabilised area where no erosion will eventuate.
- 19. All SRP's will be fitted with floating decants and all decanting earth bunds will be fitted with snorkel discharge arrangements, both with a mechanism to control (or cease) outflow during pumping activities to these structures. This mechanism could take the form of a manual decant pulley system or plug. In the circumstance where decants are manually plugged, discharge will cease and only once the standard of discharge quality, as per Principle 7 above, can be achieved will discharge occur. Pumping will be such that pump volumes will only be to the same level as that able to be fully captured within the retention structure.
- 20. All super silt fences and silt fences will be based upon the design criteria within Wellington Guidelines and the NZTA Draft Standard. Super silt fence will be used in those areas of work adjacent to, or in the immediate vicinity of watercourses. As a risk management tool for super silt fences the fabric will be installed with a minimum 200mm of fabric placed upslope at the

base of the trench. In circumstances where silt fences or super silt fences are proposed next to active roads, they will be installed only after traffic barriers have been installed, to ensure safe installation and also to provide further protection of the silt fence or super silt fence material from accidental damage.

21. Dirtywater runoff diversion channels will be sized, in accordance with the NZTA Draft Standard, to cater for the 1% AEP rainfall event which will ensure that all storm events up to this design will be diverted to control measures without overtopping. This will prevent uncontrolled runoff within the site boundaries. The design for all dirtywater runoff diversion channels will be based on the largest catchment areas within the Project and accordingly will result in overdesign. Dirtywater runoff diversion channels design will be based on the tables provided within section 7.1 of this ESCP. While, for risk management purposes, these dirtywater runoff diversion channels are "oversized" as recommended by the Wellington Guidelines there remains the potential for deposition within them, and where this is noted to be an ongoing issue, excavated pits or sumps will be positioned along the channels to retain sediment bed load.

### Streamwork Principles

22. Stream works activities are considered high risk due to the potential for sediment generation and yield and will be undertaken in a manner that recognises this risk and the sensitivity of the receiving environment. At all practical times these activities, and any associated works within these environments will be undertaken in a "dry" environment. This will be based upon diversion of flows around the area of works or working directly above the stream with no formal stream diversion required. Drawings CV – CM 246 – 247 in Appendix H.E (Stream Crossing Methodology), Management Plan Appendices, Appendix H, Volume 5 show this detail. Consideration will also be given to the fish spawning and migration periods, during which time instream works will be restricted.

The NZTA has a proven track record with respect to erosion and sediment control associated with large infrastructure projects. Many of these previous projects demonstrate the effectiveness of the approach taken based on the ongoing certification of CESCPs, or the equivalent, throughout the Project.

## 3 Planning Framework

It is recognised that a range of earthworks and streamworks activities that will be undertaken as part of the Project have numerous requirements under the regional policy and planning documents. The detail of these is discussed within the AEE (Volume 2) that supports this Project. When considering these requirements, however, several key features of the Project are of importance in terms of erosion and sediment control:

- Proximity to sensitive waterbodies,
- Values of the receiving environments adjacent to, or downstream of, the Project,
- Site topography, and
- Areas of exposed soils.

These items have been considered in full in developing this ESCP and are reflected in the overall approach taken. Consents have been applied for which will authorise the necessary activities and associated discharges. Where activities are recognised as permitted activities, the conditions of these permitted activities have been taken into consideration. An example of this is vegetation removal and conditions have been assessed and methodologies incorporated to ensure the conditions can be achieved. This includes in particular the initial vegetation removal activity whereby gorse, the existing cover, will be mulched and remain on the ground as a protective cover until such a time as erosion and sediment controls are in place and earthworks commences.

In addition, the NZTA has adopted as part of its wider national Environmental Plan (NZTA EP), a series of erosion and sediment control objectives for roading projects. This part of the NZTA EP is attached as Appendix H.O of this ESCP with the key erosion and sediment management objectives outlined below:

- 1. Ensure construction and maintenance activities avoid, remedy or mitigate effects of soil erosion, sediment run-off and sediment deposition.
- Identify areas susceptible to erosion and sediment deposition and implement erosion and sediment control measures appropriate to each situation with particular emphasis on high-risk areas.
- 3. Use bio-engineering and low-impact design practices where practicable.

These objectives have been fully considered and are reflected within this ESCP.

Further planning considerations associated with the Project are outlined in Section 8.0 of this ESCP.

Greater Wellington Regional Council adopts a "best practicable option" (BPO) approach to regulate earthworks. This policy recognises that earthworks can be well controlled by undertaking best management practices on site to control sediment generation and yields. Greater Wellington Regional Council recognise that there is a degree of risk associated with accepting a BPO approach and in accepting this risk carefully consider the time of the year within which the earthworks will be undertaken. This is primarily due to the expected increased risk of effects over high rainfall periods in particular with soils containing higher percentages of clay and fine silts, or when the slopes are steeper on the site.

The highest probability of storm events occurs in the winter months and as a general rule earthworks over the period May through to August are avoided where possible. When considering this Project, and in particular the nature of the sand soils and suspectibility to wind erosion when dry, it is recomended that no winter exclusion period is necessary and, in the contrary, working some of the soils over the winter months may well result in enviornmental benefits.

The activities associated with stream diversions and culvert placement, however, are recognised as requiring periods of low stream flow to facilitate works. This low stream flow can occur at any particular time of the year, although it is more likely to occur during summer months. Therefore, prior to any streamworks, discussions will be held with Greater Wellington Regional Council to ensure the appropriateness of the time of the year and the conditions that may apply.

### 4 Assessment of risk

Estimating sediment yields for the Project has generally followed procedures within the Universal Soil Loss Equation (USLE). The primary purpose of the USLE is to provide a measure of the risk of sediment generation and yields, and to assist in identifying controls required for managing this risk to the environment from sediment discharges from earthworks sites. Further it has been used as a comparative tool to gain an appreciation of the expected increase in catchment wide sediment yields as a result of the earthworks activity. Discussions with Greater Wellington Regional Council have confirmed that USLE should be used as a risk assessment process and not necessarily as a specific sediment loading tool. The Project is lineal in nature and will involve works occurring on several fronts and will also be subject to ongoing stabilisation as works progress. It is considered that the key elements of risk for this Project are the exposure of bare land, the receiving environment locations and the value of these receiving environments.

Key recognised erosion and sediment control risks are:

- works within and adjacent to watercourses and wetlands such as culvert placement and extensions, stream diversions and bridge works;
- pumping of sediment laden water from excavations; and
- stockpiling of excess spoil material.

The Project is unique from the perspective that it is of flat contour and also is predominantly of sand and peat geology. Sand consists of large size particles and, while it erodes relatively easily it also settles very quickly in water reducing discharge quantities. These soil and contour factors are critical in concluding that the sediment generation and eventual sediment yields will be low as a result. Three key aspects of erosion and sediment control are related to risk of sediment yield

1. Sediment generating potential - this highlights the generation potential of the area in question and is based on slope, slope length, soils, rainfall and erosion control factors.

- 2. Sediment delivery this relates to the amount of eroded material that is retained on site in depressions and within the site's natural contours prior to it entering any sediment treatment devices.
- 3. Sediment yields the amount of sediment that actually leaves the site and enters the receiving environment. It is well recognised that this is the key area of interest.

The USLE allows for greater consideration to be given to the areas of higher sediment yields and for these areas to be targeted with more comprehensive control methodologies to reduce this potential. The USLE can provide for this risk assessment and specific USLE calculations have been included within this ESCP as detailed within Appendix H.G. These USLE figures highlight that, based on a range of assumptions as detailed within Appendix H.G, the pre earthworks yields from the site equates to approximately 4.2 tonnes of sediment over the Project footprint. During the earthworks phase, this is estimated to increase to a total yield of 16.64 tonnes of sediment.

When considered on a catchment wide basis, the USLE allows for a comparative analysis to be undertaken which demonstrates pre earthworks a yield of 753 tonnes and during earthworks an increase to 766 tonnes. This detail is provided within Appendix H.G and shows a sediment yield increase overall of 1.7 %. This is further analysed on a sub catchment basis with the following table showing the overall sediment yield calculation outcomes.

Sediment Yield (tonnes) Over a 2 Month Period	Project Footprint Pre Earthworks	Whole Catchment Pre Earthworks	Project Footprint During Earthworks	Whole Catchment Less Project Footprint Pre Earthworks	Whole Catchment Including Earthworks Area	% Increase – Pre Earthworks to Earthworks Whole Catchment
Whareroa	0.11	18.17	0.58	18.06	18.64	2.6
Wharemauku	0.87	38.02	4.50	37.15	41.65	9.5
Waikanae	1.16	644.72	3.96	643.57	647.53	0.4
Waimeha	0.16	2.37	0.77	2.20	2.97	25.3
Ngarara	1.90	50.56	6.83	48.66	55.49	9.8
Totals	4.21	753.84	16.64	749.63	766.28	1.7

For the purposes of the USLE, the Project has been considered in various slope classes (included in Appendix H.F, USLE Plans) and it can be stated that those areas of greater slope present a higher risk of sediment yield. During earthworks activities, these slopes will, however, be reduced

and batter slopes progressively stabilised. It is also important that these steeper areas receive a degree of focus to ensure the slope lengths are reduced and progressive stabilisation occurs on a proactive basis. Over the entire Project footprint it is assumed that each area will remain open for a maximum period of 2 months and this is considered realistic (and conservative) considering the progressive nature of the construction sequence and the need to manage dust through the provision of a stabilised surface.

The Project includes 4 sectors within which a range of earthworks activities are to occur. The predominant earthwork operations will include:

- 1. The preload and the removal and replacement with sand of peat material; and
- 2. Stockpiling and other earthwork related activities.

The erosion and sediment controls developed for works utilise a range of erosion and sediment control measures that represents the best practicable option for this sector. As detailed, progressive stabilisation will also be undertaken to ensure that areas that are completed from an earthworks perspective will not be subject to erosion. This is of particular importance when considering the establishment of batter slopes where progressive topsoil, sediment and mulching will prevent erosion and sediment generation and will also ensure dust is not generated from such areas.

The primary control measures to be utilised are based on non structural methodologies. These are outlined in Section 7.0 of this ESCP. These do, however, include the use of diversion channels, decanting earth bunds, super silt fences and sediment retention ponds in some locations. A distinctive feature of the Project from an earthworks perspective is the significant amount of sand and peat material and as a result traditional erosion and sediment control methodologies are not always practical with alternatives available. Emphasis will be placed upon the monitoring and maintenance of all controls installed and the methodologies utilised with particular attention paid to areas of higher risk prior to, during and after rain events.

While overall therefore the USLE provides a comprehensive overview of potential sediment yields, it is recognised as theoretical only and the maximum value is gained through the comparative analysis of the yields calculated. Further it is considered of value throughout the Project, as more specific detail of Project materials and location are obtained, that USLE calculations continue to be undertaken and continue to form part of the implementation risk assessment process.

USLE calculations have confirmed the following sediment yields during earthworks:

Whareroa Catchment 0.58 tonnes

Wharemauku Catchment 4.50 tonnes

Waikanae Catchment 3.97 tonnes

Waimeha Catchment

0.77 tonnes

Ngarara Catchment

6.83 tonnes

This equates to a total sediment yield of 16.64 tonnes for the total Project with an estimated exposed area of 138.8 ha over the Project duration. Pre earthwork yields are calculated as 4.20 tonnes. While the Waimeha Catchment sediment yields represent a 25% increase this is based on a 0.77 tonne sediment yield only from the Project area.

The more significant sediment yields are noted to be related to the steeper areas of the site which are clearly identified within the plans provided in Appendix H.F (USLE Plans) of this ESCP. In recognition of this increased risk that exists, comprehensive methodologies have been developed, progressive stabilisation of bare earth will be implemented and timing and duration of operations are key considerations. It is recognised that some earthworks areas will be open for only very short periods of time, for example peat excavation locations will be backfilled and stabilised with a sand layer on a daily basis. Best practice techniques have been employed during all works with particular emphasis on higher risk activities and locations.

With respect to the streamworks activities, the methodologies have taken risk into account and this is reflected in all works being undertaken in a "dry" environment wherever practicable, careful consideration of weather patterns prior to and during the works period, and also a relatively intense monitoring and audit programme of these activities. With the above in mind it is assessed that associated risk of these activities will be reduced.

For earthworks related activities chemical treatment is to be utilised as outlined within Section 7.0 of this ESCP and again this results in the associated risk of these activities greatly reduced.

## 5 Overall erosion and sediment control approach

The following section outlines the measures that will be implemented as part of the ESCP and builds on the principles outlined in Section 2.0 of this ESCP. There will be further detail and design required, which will be within the CESCP's developed, through the Project lifetime which will result in a "fine tuning" of the methodologies shown. The aim of this ESCP is to demonstrate that negligible sediment-related effects will result from construction activities with appropriate measures put in place.

Specific erosion and sediment controls

The focus on the erosion and sediment control measures is based on:

1. Viewing the proposed Project works such that all construction activities, and the full effects of these construction activities, are considered as a package.

- Minimising potential adverse effects by utilising measures which meet or exceed industry best practice guidelines (Wellington Guidelines and NZTA Draft Standard). In many circumstances due to the high water tables and soil composition, standard erosion and sediment control measures will not be suitable and innovative concepts will apply.
- 3. Implementation of an integrated approach (as outlined in Section 5.1 below) for design, implementation, maintenance and disestablishment of erosion and sediment control measures. This will ensure "ownership" of the erosion and sediment control measures and therefore better implementation and maintenance.
- 4. Undertaking pre-construction meetings for specific stages of work and having regular weekly meetings (toolbox meetings) on site with relevant personnel as part of the construction phase.
- 5. Maintaining a register of control measures and "As Built" information of key controls such as diversion bunds and sediment retention ponds to allow for quick referencing and understanding of erosion and sediment control measures. Appendix H.K of this ESCP contains a series of standard NZTA Checklists which will be adapted for this Project.
- 6. Including both structural and non-structural elements within the methodologies to be employed such as:
- Manually raised decant devices on SRPs;
- Chemical treatment utilising polyacryamide as a risk management tool;
- Proactive monitoring programme;
- Risk identification and management accordingly;
- Progressive stabilisation as works progress;
- Weather response; and
- Ensuring contracting staff are aware of the erosion and sediment controls employed and do not remove them without seeking appropriate approval.

It is expected that the specific erosion and sediment control plans will follow the principles and details outlined within this report. This enables the Project team and the consent authority to have further input into the methodologies implemented.

## 5.1 Integrated approach

The Project consists of a four lane median divided expressway through the areas of Paraparaumu and Waikanae, and includes a new bridge over the Waikanae River and a number of interchanges providing connections with local roads.

The approach taken for erosion and sediment control includes a concept whereby planning and implementation of all the erosion and sediment control methodologies and measures are

undertaken by an experienced and involved team to ensure that all relevant aspects of the Project are taken into consideration as part of these decisions. This will ensure that adequate resources, commitment and expertise are provided to erosion and sediment controls from start to finish of the Project (design through to disestablishment). This will also ensure that all key stakeholders are involved and communicated with as necessary. The team, referred to as the "Erosion and Sediment Control Team", is expected to consist of representatives from the Project team, Erosion and Sediment Control Specialist(s), other specialists as necessary such as geotechnical engineers and the Councils.

Table One below outlines the responsibilities expected for erosion and sediment control.

Organisation	Responsibilities
NZTA	■ Ensuring CESCPs are included in contract documentation as
	necessary to ensure sub contractor buy in.
	Reviews of CESCPs as required.
	Audits of Erosion and Sediment Control (E&SC) devices and
	methodologies.
	Record keeping as necessary.
Principal Civil Contractor	■ Preparation with NZTA of CESCPs.
	Implementation of CESCPs.
	■ Installation of E&SC devices.
	Inspection and Maintenance of E&SC devices.
	Stabilisation activities.
	■ Training.
	Reporting.
Consent Authorities	Certification of CESCPs.
	Certification of revised CESCPs.
	Auditing to ensure compliance with CESCPs.

Table One - Erosion and Sediment Control Responsibilities

All people working on site, or with site responsibilities, will be required to undertake a formal induction process. No one will be permitted to work on the site until they have completed the induction process. Part of this induction process will be based on environmental management including erosion and sediment control and will include familiarisation with the Wellington Guidelines and the NZTA Draft Standard.

A comprehensive environmental induction will be provided to all staff and subcontractors prior to starting work on site. The induction will include information on the ecology of the area, heritage issues including procedures in the case of unexpected finds, key environmental risks including areas of high environmental risk. Information will be provided on environmental controls such as

erosion and sediment control devices, noise and dust mitigation measures and waste management. Engineers responsible for writing work plans and job risk analysis will also be given guidance on how to assess and plan for environmental issues using the CEMP (Volume 4 of the AEE) as the key reference document.

Environmental issues will form a regular part of toolbox meetings to ensure all workers are aware of the key issues. Opportunities will also be made available for selected staff members to attend Greater Wellington Regional Council's Muddy Waters contractor education programme, Fletcher Construction Spill Response Training and other Industry Education Training programmes where they would benefit from this further training. A record shall be kept of all training including the information presented and a list of attendees.

Site staff will be made aware of the restrictions in operations when working near Designation boundaries, and areas of vegetation that are required to be protected as part of the work plan communication process.

CESCP's will be supported by an environmental toolkit based upon the "Fletcher Environmental Toolkit" as included within Appendix H.Q of this ESCP, which gives practical advice on the construction of typical site environmental controls and environmental management issues.

In addition, ongoing training opportunities will be identified throughout the course of the Project in response to issues or challenges identified. This training will take the form of an outside expert being utilised or skills already in existence within the projects resources being utilised.

Subcontractors, as a condition of their contract, will be required to actively manage environmental issues associated with the subcontract works and comply fully with the Project resource consents, all applicable statutory regulations and the overall CEMP (Volume 4 of the AEE). For significant aspects of work the Project team will require subcontractors undertaking high risk activities to provide their own Environmental Plan for review by the Environmental Manager.

Training as outlined above will be focused on:

- Understanding the resource consent conditions;
- Construction and maintenance of erosion and sediment control devices;
- Inspections; and
- Contingencies.

It is recognised that this ESCP may be administered over various contracts across the Project and it is important that the "ownership" of the ESCP and associated control measures is clear in terms of implementation and maintenance requirements. Table One above outlines the responsibilities associated with the ESCP and the associated contract documentation will include specific reference to these requirements.

## 5.2 Erosion and sediment control measures

The erosion and sediment control measures are designed to minimise the extent of soil erosion and sediment yield from the Project site. The proposed erosion and sediment control measures have been designed with the Wellington Guidelines and the NZTA Draft Standard as the minimum requirement.

It is assumed that any significant modifications to the erosion and sediment control drawings originally approved as part of any consent, may require further approval by the consent authority prior to implementation in the construction phase. This will take place where necessary through preparation of site and activity specific CESCPs and a pre-construction meeting on site with the consent authority as a precursor to installing any erosion and sediment controls prior to bulk earthworks activity. Appendix H.K contains the checklist that will form part of this pre construction process. Due to the methodologies for the erosion and sediment controls being largely similar for the specific activities is envisaged that pre construction meetings will be associated with specific activities and will generally not be required for each area of works. As an example the activity of peat replacement has a standard methodology associated with it and a pre construction meeting will be held for such an activity but will not need to be repeated unless conditions change, including a change of specific contractor involvement.

Upon completion of the installation of all approved structural erosion and sediment controls as-built certification plans will be provided.

## 5.3 Monitoring

As part of the erosion and sediment control methodology, ongoing site monitoring by the Project team will occur to ensure that the proposed erosion and sediment control measures have been installed correctly, methodologies are being followed and are functioning effectively throughout the duration of the works. Any measures requiring attention will be identified, and if necessary, relevant team members consulted to ensure continual improvement is sought. This may include undertaking further assessment of risk, including sediment yields. In the circumstance of higher risk areas being identified more stringent controls will be considered, in particular more progressive stabilisation.

Visual assessments of the receiving environment will continue to be undertaken during the works period by the Project team with particular attention during and after periods of rainfall and pumping activities. In the context of visual assessment the receiving environment is defined as the immediate receiving environment adjacent to the area of works. Any noticeable change in water clarity from that prior to the rainfall event, or upstream of the site of works, as a result of the earthworks activity will result in a review of the erosion and sediment control measures implemented and changes made as necessary.

Weather forecast monitoring will also ensure that critical works such as those associated with the stream diversion works only occur during a suitable weather window. The internet site www.metvuw.co.nz will provide one of the key tools in this regard with local weather forecasting also utilised as necessary.

### 5.3.1 Freshwater monitoring

The freshwater monitoring programme has two essential components, being "devices" monitoring and "habitat" monitoring. In addition baseline monitoring, scheduled monitoring and triggered monitoring will occur throughout the Project implementation.

Baseline surveys will define the antecedent conditions in the Project area by measuring preconstruction environmental (including ecological) variables. Scheduled monitoring will be undertaken according to a pre-determined schedule during the construction period. Triggered monitoring will occur when pre-determined thresholds are exceeded. Post-construction surveys will assess the medium term effects of the Project on the freshwater environments, and will be used to determine any need for remediation measures to counter adverse environmental effects.

Triggered monitoring for devices will involve an immediate re-check of the devices upstream of where the event occurred. If damage or malfunction of the device is observed, or the methodology for the specific works has not occurred as necessary, then it will be rectified immediately. Should the likely adverse effects have a reasonably high probability of being significant (ie. more than short-term, localised and/or minor), then ecological monitoring will be undertaken in order to determine the actual magnitude of these effects. Should significant adverse effects be detected as a result, the Project team will discuss appropriate changes to work practices and methodologies to prevent further similar events and will also consider appropriate mitigation for that particular event.

## 5.3.2 Devices monitoring

Environmental compliance for the Project during the construction period is based upon the appropriate installation, location, maintenance, and monitoring of control devices. Importantly the devices are not restricted to structures and may include work practices and methodologies. The design, installation, monitoring and maintenance of these devices are the responsibility of the Erosion and Sediment Control Team.

'Devices' monitoring comprises the monitoring of on-site construction activities, but more particularly the monitoring of on-site structures and devices designed to control the potential adverse effects of those site activities (in particular erosion and subsequent sedimentation).

The purpose of this monitoring is to ensure that all practices, control measures and devices are constructed, operated and maintained so they remain fully effective at all times. The devices monitoring will largely target erosion and sediment control activities as well as structures such as silt fences, erosion control mulching and sediment retention ponds.

This monitoring is aimed at the early detection of activities or problems that have the potential to result in a significant adverse environmental effect. Devices monitoring will be the main component of scheduled construction monitoring undertaken on-site. The devices monitoring will act as a trigger, together with the scheduled ecological monitoring, for more detailed ("trigger event") monitoring should this be required.

The frequency of the devices monitoring will vary throughout the year and will reflect areas of changing activity and risk along the Project. However, during the undertaking of activities considered higher risk such as those associated with in-stream works the monitoring of devices will be undertaken on a daily basis and more frequently during heavy rainfall. These inspections will be recorded within a weekly check-list as provided from the NZTA Draft Standard and as included within Appendix H.K of this ESCP (to be developed by the Project team) and any subsequent required actions noted. Any device problems will be recorded in a compliance report to the Councils which will comprise of a meeting with such parties and reporting of any issues identified and associated solutions. The information generated by the devices monitoring will help to determine whether any further action is necessary over and above that which is already implanted at that time.

It is essential that the monitoring of devices include inspections during storm events so that the success of the devices and controls can be reviewed and improved if appropriate.

Visual inspections of the integrity and efficiency of the erosion and sediment control devices will be the responsibility of the Erosion and Sediment Control Team. Qualitative inspections of the installation, operation and maintenance of the sediment controls will occur daily throughout the duration the devices are in place.

The visual inspections will include qualitative monitoring of the following:

- the integrity and effectiveness of all erosion control and sediment treatment devices,
- activities on site,
- general site conditions and other activities occurring within the catchment,
- general status of the immediate receiving environment.

The details of these visual (qualitative) inspections will be recorded on the check lists.

Prior to construction commencing photographs will be taken in the vicinity of the proposed discharge outlet points and any streams in the vicinity of the works. These records will show the visual state of the receiving environment at and within the vicinity of the discharge point. This photographic record will be compiled into a log book and will allow a visual comparison of before, during and at completion of the construction of the Alignment. Visual inspections of the discharge points and general stream conditions in the vicinity are part of the requirements of the devices monitoring.

Where actual problems with the integrity and/or effectiveness of the devices (ie. for both erosion & sediment control and other on-site activities) are observed these shall be rectified immediately. In addition, there will be more detailed inspections of devices, on-site practices and other catchment activities that will be undertaken in response to certain "triggers" identified over the course of the routine devices monitoring programme. The triggers for these more intensive / repeat investigations include observations such as:

- Activities observed to be happening on-site that are likely to compromise the effectiveness or integrity of that site's erosion and sediment controls;
- Bearing in mind antecedent climatic conditions, a conspicuous change of water colour at the downstream monitoring sites that is very different to the colour that is normally associated with stream conditions at the same site, and with such change in colour not evident at upstream locations above the construction zone;
- Obvious accumulation of sediment in the vicinity of the discharge points, or anywhere else within or in proximity to the active construction zones;
- Streambank collapse or obvious signs of channel erosion / instability in the immediate receiving environments;
- Visual reports / evidence of changes to downstream community structure (eg. fish kills, death or discolouration of instream plant communities, increased weed growth); and
- Spillage / accident reports by site personnel.

If the results of any devices monitoring suggest that adverse effects are likely to have occurred then "triggered" responses will be implemented. A "triggered" response is in recognition that an event associated with the Project has occurred that may result in a significant adverse effect. A triggered response follows the process below:

- ascertain that in all probability the issue is associated with the Project;
- inform and liaise with the consent authority;
- ascertain the magnitude of the adverse effects (this may involve undertaking immediate monitoring of the ecological variables);
- if the effects have been more than minor, ascertain what response is necessary;
- determine how to monitor the effectiveness of the response(s); and
- implement and monitor the response.

A continual feedback loop is included in this process until it has been verified that the implemented responses have been successful. Changes to construction site practices or to specific devices may also need to be implemented to avoid any future similar events.

#### 5.3.3 Flocculation monitoring

Chemical treatment remains as an option that may be utilised in circumstances where discharge water quality is not considered appropriate for the receiving environment or in the case of specific pumping activities. Not all sediment retention ponds or decanting earth bunds established on the site will require chemical treatment; however, these devices are likely candidates for such treatment. The application of flocculants will be carried out in accordance with best practice principles, and will be undertaken in accordance with this ESCP.

A core part of flocculation management will be monitoring, in order to check that the systems are all working as anticipated and to provide data to facilitate management of the floc socks as they are utilised and manual batch dosing. The monitoring that will be carried out is as follows:

- Discharge and receiving environment pH levels at weekly intervals and during nominated storm events. It is expected that with the use of polyacrylamide no pH influence will result; and
- Periodic checks of final discharge suspended solids concentration, particularly during storm flows.

This monitoring will be undertaken by suitably trained members of the Erosion and Sediment Control Team.

## 5.3.4 Other checks and inspections

In addition to the devices and flocculation monitoring the other on-site activities such as storage of hazardous chemicals, refuelling facilities and practices, site offices, haul roads, stock-piles, dust control, noise control, etc will also all need to be regularly checked and inspected. The intention underlying these checks is to ensure that they are being properly maintained at all times, and that they remain within the specified standards including consent conditions.

The freshwater habitat monitoring programme is intended to:

- identify and quantify any adverse effects resulting from the high risk activities, and
- identify and evaluate corrective measures which may be required in the event of adverse ecological effects arising from these activities.

These high risk activities are focused around the proposed stream works and in this regard will be monitored by use of a Before-After Control-Impact (BACI) methodology. This refers to undertaking pre-construction (ie. baseline) surveys at selected sampling sites within the location of selected streamworks, and then periodically re-surveying these same sites following the streamworks activities, and continuing for a set period after their completion and comparing the results. It also utilises fixed sampling sites stationed outside and within the likely zones of impact.

Baseline data will provide a bench-mark against which to measure the construction and operational phase data sets. The scheduled monitoring will involve routine studies of prescribed ecological

parameters. The triggered monitoring will be in response to potential adverse effects having happened, as identified by pre-determined "triggers" having occurred.

A detailed Ecological Monitoring Plan (Technical Report 26, Volume 3) provides further details of freshwater habitat monitoring to be implemented.

## 5.3.5 Monitoring response to indicators of significant effects

In the event that adverse impacts on the receiving environments are detected by the ecological monitoring programme, a possible (cause-effect) association with the Project will be investigated in the first instance. Should this prove to establish linkages between the adverse effect and on-site practices then alterations to the operational methods (including modifications to environmental control measures and methodologies) will be investigated as a first order response. Greater Wellington Regional Council will be consulted in regard to any proposed changes to the on-site practices. Further monitoring would then be used to assess the effectiveness of the alterations in operational methods to alleviate / avoid adverse effects on the environment.

Factors to be considered in the decision chain relating to the above would include:

- the assessed likely cause(s) of the effect;
- whether the effect is on-going;
- the magnitude of the event;
- the sensitivity of the receiving environment; and
- the need for, and nature of, any remedial action.

The most likely cause of a significant adverse effect would be the incorrect installation of devices or sub-optimal performance of the measures and methodologies designed to avoid or minimise adverse environmental effects. The Erosion and Sediment Control Team are responsible for ensuring adequate provision for such devices, and the routine environmental inspections are aimed at minimising incorrect installation or failure to repair any observed damage.

This ESCP outlines a number of preventative measures that will prevent an adverse effect from occurring in the first instance. In addition to the ESCP the Project team will be preparing CESCPs which will be lodged with Greater Wellington Regional Council prior to construction activities.

Contingency measures (such as the requirement for spill kits to be present in re-fuelling areas) are also detailed in the CEMP (Volume 4 of the AEE) and form part of the responsibility of the Project team.

## 5.4 **Dust**

Earthworking activities on the Project have the potential to generate dust that may be considered to be a nuisance in times of dry and windy weather particularly when working in sand spoil environments but also applicable to peat soils during dry periods. To manage the potential dust nuisance the standard procedure is to minimise, identify and acknowledge these effects. Implementing these measures and ongoing monitoring will occur at all times during construction.

Dust is the product of wind erosion, much as sediment is the product of erosion by water. Repeated tracking of soils with machinery not only breaks down the soil particles but also aerates the soils so that they become suspended as particulate material in the air. As the strength of the wind increases, the potential for dust problems increases exponentially. The rate of soil movement is proportional to the cube of the wind velocity.

Dust from problem sites can travel for kilometres and cause a range of problems to health and property. With respect to the Project, existing property locations can be immediately adjacent to the Expressway works and when downwind for the works area dust management will be critical. An example exists north of Kāpiti Road where with westerly winds as the predominant wind direction wind and sand blowing onto the properties in the east will need close monitoring.

The main practice to be used to control dust on the Project is the application of water to keep soil moisture high enough to prevent dust generation and sand blow. Water supply is detailed within the Construction Methodology Report (Technical Report 4, Volume 3).

For each area of works, consideration will be given to the following elements:

- The potential effects of dust problems if dust causes a nuisance off site.
- The soil characteristics of the site and whether the timing of operations will help or hinder dust control. This may influence undertaking works on sandy soils during wetter periods of the year.
- Considerations to the operational methodology to reduce the dust problems such as progressive stabilisation of batters and stockpile area as necessary.
- Provision for a 24 hour contact number for dealing with dust complaints that may arise from the Project (CEMP Appendix S, Volume 4).

The timing of works can be crucial for dust management and within the Project footprint if the earthworks can be carried out during the wetter winter season with minimal erosion and sediment control problems then dust control will be less of a problem.

In addition stabilised haul roads will be fully utilised and installed where construction traffic is likely to damage existing stabilised areas. These haul roads will be constructed by use of sand backfill with a progressive cover of clean granular material as works progress.

Mulch, including both the use of hay/straw mulch and wood mulch will be utilised to assist with dust management in particular with respect to stockpiles and batter establishment. Where dust generation is the predominant issue then water carts will be utilised as the initial treatment option. This in particular applies to the batter slopes which will also be subject to stabilisation. For pre load

activities short term batters (less than 6 months) will have a final layer of clean granular material applied over sand to ensure no wind disturbance of the surface while longer term batter slopes (greater than 6 months) will have topsoil and grass established. For final cut slopes, stabilisation will be through the use of topsoil and grass from the top of the slope as the cut progresses.

For further details on dust and odour management from the earthworks activities reference should be made to the Appendix G of the CEMP, Volume 4 (Construction Air Quality Management Plan).

## 6 Specific erosion and sediment control methodology

When considering this section of the ESCP, reference should be made to Appendix H.B which contains area specific erosion and sediment control plans for the Project. These plans have been drafted based on several site visits along the entire Alignment and also reflect the fact that CESCPs as outlined in Section 1 of this ESCP are to be established which will enable the Project team and Council to have further input into the methodologies implemented. The ESCP provides for an overview of the erosion and sediment management techniques and measures that will be used within the Project, provides specific examples throughout and also outlines methodologies and management techniques that will apply and will achieve the necessary environmental objectives.

It is also important to note that the Construction Methodology Report (Technical Report 4, Volume 3) provides details of staging, sequencing, overall methodology philosophy and confirms the requirements of the various activities and specific structures that will be established.

Reference should also be made to the Contaminated Soils and Groundwater Management Plan (Appendix K of the CEMP, Volume 4), which outlines the implementation and operation procedures to be followed when working within known areas of contamination. These aspects are all incorporated into the ESCP and CESCP.

Drawings CV – CM 200 – 231, Management Plan Appendices, Appendix H, Volume 5 outline the erosion and sediment control methodologies and devices that will be utilised.

## 6.1 Sector One

Sector One from chainage 1900 to 4500 includes preloading activity and a number of culvert extensions. Both preload and culvert extension methodologies will be followed.

At Poplar Avenue two separate SRPs (Sediment Retention Ponds 1, and 2) will be established for two discrete catchments associated with the new road configuration. These SRPs and associated catchment areas are detailed within Drawing Number CV – CM 201 and 202, Management Plan Appendices, Appendix H, Volume 5. In addition to the SRPs, silt fence will be established along batter boundaries where diversion channels cannot divert flows to the associated SRP. This is

expected to occur due to the flat contour within this location such that diversion channel will not be effective. Progressive stabilisation of all batters will also occur.

From chainage 2700 to 4100 the preload methodology as outlined within Section 7.4 of this ESCP will apply. This involves the establishment of topsoil bunds either side of the pre load activity and the installation of decanting earth bunds each with a maximum catchment area of 3000m2. Super silt fence is also established at chainage 3600 to protect an open channel environment which forms part of the long term stormwater management for the site.

At Raumati Road a further SRP will be established (SRP 3) to treat any runoff from discrete catchment areas as shown on Drawings CV – CM – 204, Management Plan Appendices, Appendix H, Volume 5. On the western side of the Alignment in this same location the permanent drainage swale and rock filters will also be utilised.

As noted throughout the entire Project where wetlands and flood storage facilities are to be developed they will be done so in accordance with the Technical Report 22, Volume 3 and the details within Section 7.16 of this ESCP.

Construction Yards will be established and will be managed from an erosion and sediment control perspective as per Section 7.14 of this ESCP



Plate One - Chainage 2500m Poplar Avenue Looking South Over Pre Load Area

## 6.2 Sector Two

Sector Two from chainage 4500 to 8300 includes pre load methodology up to Kāpiti Road north of which some peat replacement will occur. Both preload and peat replacement methodologies will be followed. In addition to these methodologies silt fence will be used with progressive stabilisation and a further 6 SRPs (Sediment Retention Ponds 4, 5, 6, 7, 8 and9) will be established with SRPs 5, 6, 8 and 9 all to be installed in the same location as the long term stormwater wetland facilities. In this circumstance it is expected that these long term stormwater wetland facilities will be established early in the Project to enable utilisation as outlined during construction activities. The drawings within Appendix H.B of this ESCP show these facilities and highlight the minimum volumes and design dimensions that will be required to achieve the necessary sediment management. Outlets for these devices will also be installed as per the Drawings CV – CM 248 – 251, Management Plan Appendices, Appendix H, Volume 5 which will be converted to the final stormwater management outlet device on completion of construction.

The construction related sediment controls must remain in place until all earthworks for that sub catchment are stabilised, and permanent stormwater facilities for the corresponding catchment must be in place and operational prior to the impervious area of that sub catchment area reaching 80%.

At chainage 5400, Ihakara Street is to be extended to allow access for the construction of the bridge over the Wharemauku Stream; the road construction will consist of a hard fill stabilised platform area. The Wharemauku Stream will be fully protected by super silt fence during construction. SRPs 5, 6 and 7 will discharge into the Wharemauku Stream.

From chainage 5400 to 6300 the eastern extent of the construction works will discharge into SRP number 8 while the western extent of the works will utilise the permanent drainage swale and rock filters.

From Kāpiti Road to the north the principle methodology changes to peat replacement with SRP 9 to be established as shown on Drawing Number CV – CM – 211, Management Plan Appendices, Appendix H, Volume 5. This area also involves significant works within sand environments and the peat replacement and sand methodologies involving the establishment of topsoil bunds and utilisation of pumping will occur. It is recognised that from Kāpiti Road north to Mazengarb Road that a significant dust issue could result if not managed appropriately and as a result specific management of this area is required. Works during the winter wetter period will be encouraged and in other times a programme of dust management using water carts will continue. Water source is as detailed within the Construction Methodology Report (Technical Report 4, Volume 3) with further water supply from SRP 9 as required. Further this area of works involves some large cut sand faces with progressive stabilisation of these batters as outlined in Section 5.4 of this ESCP as the batters progress.

At chainage 8000 the Mazengarb Drain will be crossed with the methodologies as outlined in Section 7.0 of this ESCP to be followed. Super silt fence will also be utilised. The rest of the sector to chainage 8300 involves pre load activity with the establishment of diversion channels and decanting earth bunds as required.



Plate Two - Approximate Chainage 4750 Location of SRP # 4



Plate Three - Looking South to Wharemauku Stream and SRP 7 Location



Plate Four - Looking north to Kāpiti Road Approximate Location of SRP 8



Plate Five - Approximate Chainage 7200 Looking South to Kāpiti Road

#### 6.3 Sector Three

Sector Three runs from chainage 8300 to 12400. From Chainage 8300 to 10650 (Waikanae River) both peat replacement and preload methodologies will be utilised including the use of topsoil bunds and decanting earth bunds. Any pumping that is necessary because of peat replacement activities will be undertaken as detailed within Section 7.11 of this ESCP, with reference also given to the "Permit to Pump" system. No SRPs are proposed within this chainage. Progressive stabilisation will continue throughout. North of Otaihanga Road a large area of sand works will utilise the methodology associated with the permanent swale drainage system and the use of rock filters spaced at 100m centres.

A portion of the existing land fill and transfer station area will be utilised as a construction yard with Drawing Number CV-SP 159 as provided in Appendix H.B, Management Plan Appendices, Appendix H, Volume 5 showing this detail including the specific erosion and sediment controls for the establishment of this yard.

Further works are also proposed associated with the Otaihanga Roundabout. These works, while isolated from the main Alignment, will comprise some lane widening, traffic island establishment and general earthworks activity. Drawing CV – CM 231, Management Plan Appendices, Appendix H, Volume 5 shows the proposed erosion and sediment controls which consist of silt fence installation on the southern and eastern extent of work with 2 small decanting earth bunds to be established on the northern extent of work. These decanting earth bunds are designed to capture any runoff from the cut batter to be established with 2 small subcatchment areas. As part of these works, progressive stabilisation of both the finished road surface and the batter slope will occur to minimise erosion.

The Waikanae River is an area that is recognised as presenting a higher risk due to the location of the works associated with the bridge establishment. This methodology is detailed within the Construction Methodology Report (Technical Report 4, Volume 3) with the erosion and sediment controls detailed within Section 7.10 of this ESCP.

From chainage 10800 to 11300 it is proposed that the permanent stormwater wetland to be established will be used during the construction period for the purposes of sediment management. This is referred to as SRP 10. Immediately north of this to chainage 11800 a further permanent stormwater wetland will be established and will be used during the construction period for the purposes of sediment management. This is referred to as SRP 11.

Works around Te Moana Road will utilise super silt fence with the Waimeha Stream to be bridged and to be fully protected with the use of super silt fences and progressive stabilisation of batter slopes as they are established. Topsoil bunds, drainage swales and rock filters will be utilised north of this area.



Plate Six - Waimeha Stream - protected with Super Silt Fence

## 6.4 Sector Four

Sector Four from chainage 12400 to 18050 includes a large proportion of working directly in sand plus additional pre load and peat replacement methodologies. These will all be undertaken in accordance with the methodologies as outlined in Section 7.5 of this ESCP. Utilisation of the permanent drainage swales and rock filters features within this sector.

A relatively large stream diversion is required north of the Ngarara Road with this to be fully established in the "dry" and only once a fully stabilised channel is established will stream flows be directed to the new channel alignment. The methodology as outlined in Section 7.7 of this ESCP details this work. Once the stream diversion is operational, as an early part of the works in this location, it will be fully protected with super silt fence as shown on Drawing Number CV – CM 222, Management Plan Appendices, Appendix H, Volume 5. Further to this a permanent stream diversion of the Kakariki Stream is also required in this location with the methodology as outlined in Section 7.7 of this ESCP to also apply. This will involve some ground improvement work which will be undertaken outside of the stream channel and the stream flow diverted to the new channel once full stabilisation has occurred to allow for bridge construction.

Wetland and offset flood storage facilities are to be established and will be undertaken in accordance with the methodology as outlined in Section 7.16 of this ESCP. Two new SRPs (SRP 12 and 13) will be developed within the sector at chainage 14000 and 14200 which will utilise the proposed permanent stormwater wetlands and will be established early in the Project.

From chainage 15400 pre load activities will occur and will be managed through the construction period as per Section 7.4 of this ESCP including the installation of decanting earth bunds.

At Peka Peka Road the pre load methodologies will be followed and will be supported with the use of silt fences. No sediment retention ponds are planned in this location at present, although it is noted that, if necessary, they could be established and room availability is not considered an issue.



Plate Seven - Approximate chainage 13300 looking south – peat replacement and sand methodologies

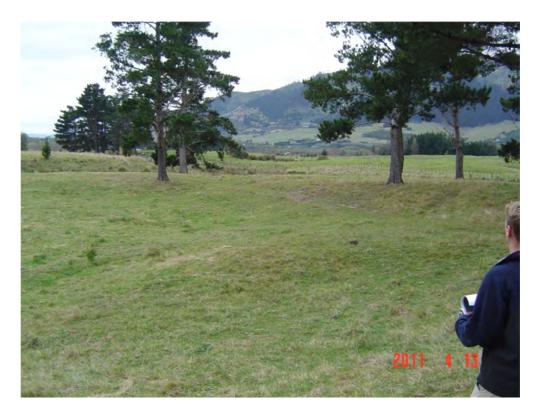


Plate Eight - Approximate chainage 15300 looking North - sand methodology



Plate Nine - Approximate chainage 16600 looking South Over Alignment

# 7 Activity details and methodologies

## 7.1 Erosion and Sediment Control Devices

As detailed, above this ESCP provides the general principles and methodology for undertaking the necessary earthworks associated with the Project construction and ensures that environmental objectives can be achieved with minimal effects from earthworks. With innovation and more detailed design as the Project progresses, development of CESCPs will be prepared and submitted for certification prior to construction.

As detailed within Section 6.0 of this ESCP the Project includes the implementation of a range of erosion and sediment control measures. With respect to the SRPs, a total of 13 SRPs will be established. These SRPs are all sized based on a volume of 2% of the catchment area, length to width ratio of 3:1, side slopes of 2:1 and a depth of 1.0m. SRP 4 has been designed at a length to width ration of 5:1 to ensure it can be accommodated within the Designation boundary. Baffles may need to be installed in this SRP to achieve design criteria.

The details of the specific erosion and sediment controls to be implemented in each of the four sectors are detailed with the Erosion and Sediment Control Plans as provided in Appendix H.B of this ESCP. These plans also show the catchment areas which apply and are related to the specific erosion and sediment control measures. The plans provided outline the control measures that are expected to be used, and the methodology to be implemented within each sector. These methodologies refer to Section 7.0 of this ESCP and centre on the following key activities:

- Peat replacement;
- Works within sand environment:
- Pre load activities:
- Works in swales / overland flow paths and placing pipes away from watercourses;
- Culvert extensions;
- Bridge construction;
- Temporary and permanent stream diversions;
- Stone Columns;
- Rip rap placement;
- Wetland and Flood Storage Facilities;
- Pumping;
- Chemical Treatment;
- Bentonite/Polymer; and
- Construction Yards.

Further to the above, it is recognised that the sizing of the various erosion and sediment control measures is critical in achieving an overall effective approach to the Project. SRPs are designed based on a 2% volume criterion as shown in Table Two below.

Sediment Retention Pond	Maximum Catchment Area (ha)	Minimum Pond Volume (m³)	Forebay Volume (m³)	Top Dimension (m)  1.0m depth – all based on  3:1 length to width ratio except SRP # 4	Number of Decants	Side Slopes	Inlet Slope
SRP # 1	2.92	584	55	46.0 by 17.0	2	2:1	3:1
SRP # 2	2.12	424	45	39.5 by 15.0	2	2:1	3:1
SRP#3	1.01	202	20	28.5 by 11.5	1	2:1	3:1
SRP # 4 – L:W = 5:1	3.35	670	70	62.0 by 14.0	3	2:1	3:1
SRP # 5 To utilise proposed perm S.Water Wetland	1.36	272	25	32.5 by 13.0	1	2:1	3:1
SRP # 6 To utilise proposed perm S.Water Wetland	1.89	378	40	37.5 by 14.5	2	2:1	3:1
SRP#7	0.84	168	15	26.5 by 10.5	1	2:1	3:1
SRP # 8 To utilise proposed perm S.Water Wetland	2.43	486	50	42.0 by 16.0	2	2:1	3:1
SRP # 9 To utilise proposed perm S.Water Wetland	2.34	468	45	41.5 by 15.5	2	2:1	3:1
SRP # 10 To utilise proposed perm S.Water Wetland	2.72	544	55	44.5 by 16.5	2	2:1	3:1
SRP # 11	4.15	830	80	54.0 by 20.0	3	2:1	3:1

To utilise proposed perm S.Water							
Wetland  SRP # 12  To utilise proposed perm S.Water Wetland	0.38	76	10	19.0 by 8.5	1	2:1	3:1
SRP # 13 To utilise proposed perm S.Water Wetland	3.92	784	80	52.5 by 19.5	3	2:1	3:1

Table Two - Sediment Retention Pond Volume and Size Analysis

Where the sediment retention pond is to form the same footprint as the permanent stormwater pond the permanent stormwater pond outlet will be established and isolated by a bund from the SRP feature. The SRP will then be established and discharge via a design outlet into the permanent stormwater outlet.

With respect to cleanwater diversion channels and dirtywater runoff diversion channels, it is recognised that within the Project there are a wide range of catchment sizes and characteristics that will require specific design for each area. Within this ESCP the approach taken for sizing diversion channels is based on provision of a conveyance system that will transfer up to the 1% AEP storm event to the treatment device. This forms part of the erosion and sediment control risk management framework for the Project. Cleanwater diversions are not anticipated as necessary for the Project; however, if required, they will be designed through the CESCPs to cater for the 1% AEP rainfall event. Table Three and Figure Two below provide an example of the sizing guidance which will be utilised within the Project.

As earthworks commence in each sector, the specific as built catchment will be determined and the diversion channel sizing calculated from this figure accordingly. Appendix H.M of this ESCP provides the full set of figures for dirtywater runoff diversion channel sizing.

Catchment Areas	100yr ARI Q (m3/s)	100yr ARI Site slope (5%) Depth (m)	100yr ARI Site slope (5%) Bund Height (m) (D+300mm)
0.50	0.1124	0.1520	0.4520
1.00	0.2248	0.1971	0.4971
1.50	0.3372	0.2295	0.5295
2.00	0.4496	0.2556	0.5556
2.50	0.5620	0.2779	0.5779
3.00	0.6744	0.2976	0.5976
3.50	0.7867	0.3153	0.6153
4.00	0.8991	0.3315	0.6315
4.50	1.0115	0.3465	0.6465
5.00	1.1239	0.3604	0.6604
5.50	1.2363	0.3736	0.6736
6.00	1.3487	0.3860	0.6860
6.50	1.4611	0.3977	0.6977
7.00	1.5735	0.4089	0.7089
7.50	1.6859	0.4196	0.7196
8.00	1.7983	0.4299	0.7299
8.50	1.9107	0.4398	0.7398
9.00	2.0231	0.4493	0.7493
9.50	2.1354	0.4585	0.7585
10.00	2.2478	0.4674	0.7674

Table Three - Dirty Water Diversion Channel Design

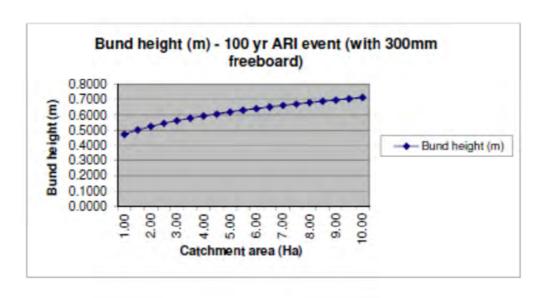


Figure Two - Dirty Water Diversion Channel Design

# 7.2 Peat Replacement

Where peat replacement is the designated approach for undertaking Alignment construction this will be undertaken in a series of steps as detailed within Drawings CV – CM 240 – 243 within Appendix H.D, Management Plan Appendices, Appendix H, Volume 5. This is summarised as follows:

1. Topsoil will be stripped from the total Alignment corridor width above. This will be utilised to form a stabilised bund which will function as a clean water diversion for water from outside of the

Alignment and will also function as a dirty water diversion for the Alignment works themselves. This will be sized as per Table 3 above. Effectively the topsoil bund also forms a clear and definitive boundary between the works area and those areas outside the works environment which will remain in their current state.

Water that collects within the works area will be either discharged via direct percolation into the soil profile and groundwater system, will be treated and discharged through a series of decanting earth bunds or will be pumped away from the Alignment to a turkeys nest and grass environment as per Drawing Number CV – CM 248 – 251, Management Plan Appendices, Appendix H, Volume 5. This pumping is temporary only and is designed to allow backfilling to occur after which groundwater levels will quickly re-establish themselves to original levels. Decanting earth bunds will be established at intervals along the corridor and will have maximum catchment areas of 3000m2 each and will be constructed to a volume that equates to 2% of the contributing catchment area.

- 2. Step 2 involves the use of a 50T excavator removing peat from the Alignment corridor and stockpiling this material between the topsoil bund previously established and the excavation. Pumping and or utilisation of decanting earth bunds will occur as necessary.
- 3. Step 3 involves the placement of sand within the excavation. This is expected to occur at the same time as the excavation and hence at any one time the open trench area will be minimised while also allowing for the required geotechnical inspection and approval of the surface conditions within the excavation prior to backfilling. This has the effect of ensuring that during works, and importantly at the end of the working day, the open trench area is minimised such that water infiltration through the peat material does not create unnecessary saturation and practical issues. At the end of each working day this sand backfill will need, as a minimum, to be to the same level as the water table.

This step will be happening at the same time as the earlier step of peat excavation. From a sediment generation perspective the works involve an excavation below the ground surface and as a result minimal runoff from the excavation itself is expected. There is, however, expected to be the requirement to undertake some pumping activities and this will occur through the use of pumping to a turkeys nest and grass environment as per Drawings CV – CM 248 – 251, Management Plan Appendices, Appendix H, Volume 5 and as detailed in Section 7.11 below.

Sand backfilled areas will then be able to be utilised as a stabilised all weather haul road providing access throughout the Alignment as works progress without unnecessary sediment generation created by tracking activities.

During this stage of the process ongoing shaping and compaction of the temporary peat stockpile will also occur utilising a 20T excavator.

4. The final step, step 4 is essentially a repeat of step 3 except that the peat removal is then focused on the central part of the Alignment. Peat will therefore be placed within dumpers and transported via the stabilised sand haul road to the temporary peat stockpile location. Sand will again be backfilled as required ensuring the minimisation of open excavation, and hence groundwater infiltration.

From an erosion and sediment control perspective the same treatment methodology will apply throughout the entire peat replacement process with all works to occur within the bunded area. From a practical construction perspective this bund may have to be removed during specific times of activity such as the transfer of adjacent sand into the peat excavation. Where this is required to occur, the works outside the bunded area will be required to be managed (from an erosion and sediment control perspective) in an isolated manner and the bund re-established on a daily basis, or prior to rain events to ensure the integrity and purpose of the bund remains.

Based on the results of a peat replacement trial undertaken on site the main conclusion was that this methodology will be successful with excavation and then immediately backfill, pushing any water ahead of the front of sand. Some risk remains that this trial was not representative of the whole site and differing conditions can be expected to result.

Removal of the peat from the stockpiles will occur once the material is considered of a suitable dryness and will be transported along the Alignment with all vehicles manoeuvring on the sand haul road only.

## 7.3 Peat Replacement Trial

Appendix H.N of this ESCP contains the results of a peat replacement trial (the trial) undertaken in May 2011.

During the trial works groundwater was located at or less than 100mm below the ground surface for most of the site throughout the test. Groundwater seepage from the peat itself was, however, relatively minor and slow and where it did occur, it was typically adjacent to tree trunks or branches located within the soil profile. Most of the water flowing into the pit was either from ponded surface water draining into the pit or from water piping up through the sand. The water pumped from the pit after it had been dug was relatively turbid. For the purposes of the trial, erosion and sediment control methodologies consisted of pumping to a grass environment some 100m away from the nearest watercourse. No turkey nest or detention device was utilised at the pump discharge. However, during pumping activity, it is noted that the pump intake was subject to blockage and intake of sticks; to avoid this occurring a 100mm layer of hay and ballast material was utilised with the pump intake located within this layer. This in itself provided a filtering media where larger debris and particles were not sucked into the pump intake. This avoids physical blockages and damage but also avoids unnecessary sediment transfer to the pump outlet. This is discussed as part of the pumping methodologies within Section 7.11 of this ESCP.

There was no overland flow of pumped water into the drains beside the trial site with most water ponding within the paddock and entering the subsurface water over time. The peat stockpile itself was also noted to release water over time and with the surface ponding due to the wet conditions raised the surface water level behind the stockpile. This ponding issue has resulted in the need to further consider cross drainage, or physical gaps, through the stockpile locations and will be installed at approximately 50m intervals where the stockpile does not allow natural drainage. For drainage, PVC 200mm pipes will be utilised in this manner.

Of importance to note is that during the trial the drain upstream of the trial site appeared to have low water quality as it was discoloured and had an organic oily skin in stagnant areas, similar to that observed leaking from the peat stockpile.

The trial has further concluded that:

- There is no need for any drainage as part of the excavation itself. Peat can be excavated and backfilled with sand back to ground levels at which time the Alignment itself can be constructed which will include permanent drainage as necessary.
- Stockpiles will be established adjacent to the peat excavation along the entire Alignment where this methodology is to occur. The stockpiles will be temporary only and will be removed to permanent locations.
- Temporary drainage for the position of the stockpiles from the excavation may be required. Stockpiles will not be placed in, or immediately adjacent to, watercourses and ideally they will be placed where they do not interfere with natural surface drainage. If the positioning of the stockpiles are such that it does interfere with the natural surface drainage solid PVC pipes can be installed at a minimum 150mm diameter (to prevent blockage) at calculated intervals such that the drainage can continue in its natural form.

## 7.4 Pre Load

Sections of the proposed Alignment will be subject to pre load activities to assist with ground settlement and ensure that future settlement is minimised. This activity essentially involves the placement of sand or granular material over the position of the Alignment. This material will be trucked into the site utilising a fully stabilised access way to ensure no unnecessary erosion of this area occurs. The stabilised access way also provides a "buffer" between the works area and the existing road from which this material will enter the site and thus will prevent material being transported onto the existing road network. Drawing Number CV – CM – 244, Management Plan Appendices, Appendix H, Volume 5 shows the conceptual pre load activity.

Prior to placement of the pre load material the site will be prepared as follows:

1. Topsoil will be stripped from the location of the Alignment outside of the preload footprint. The pre load footprint itself will remain in its natural state. This area to be stripped will have the

topsoil removed and compacted in the form of a bund on either side of the Alignment location. This will act as a dirty water diversion channel and as such will be constructed to the design criteria.

It is noted that during pre load activities the permanent drainage swales will also be established on site. While these swales will form part of the permanent drainage, during the construction phase of the works they will be used as part of the sediment management techniques. Filter rocks can be established within the swale to assist with trapping sediment and preventing sediment discharge. In sand environments rock filters will be placed at 100 metre intervals due to the larger soil particle size and ease of settlement. It is not expected that significant amounts of sediment will actually reach the swale environment and, therefore, while maintenance is important, this is not expected as a major requirement.

- 2. Decanting earth bunds will also be established at intervals along the preload corridor. These will have maximum catchment areas of 3000m2 each and will be constructed to a volume that equates to 2% of the contributing catchment area. It is expected that based on a maximum of 3000m2 per decanting earth bund that the volume of these structures will be 60m3. The pre load corridor length per decanting earth bund will alter throughout the Project although it will typically be established at 60m intervals with diversion channels established across the corridor to limit the catchment area to 3000m2. All decanting earth bunds will be established with floating decants.
- 3. The preload material will be placed directly onto a geotextile blanket and once various sections are at the desired preload levels the preload area will be fully stabilised. This will serve two purposes associated with minimisation of erosion and hence sediment yields and also minimisation of any dust generation from the preload deposit.

Erosion and sediment controls are expected to remain in place throughout the entire pre load period and can act as the specific control measures, with associated maintenance, once the preload is completed and road formation commences.

# 7.5 Working in Sand

Sand soils present a unique situation whereby they have a very high infiltration rate and while they can be subject to scour and erosion issues the sand particles are of such a size that they settle very quickly within depressions and/or detention devices. These soils are, however, subject to significant wind blow erosion particularly when they are subject to drying and in windy conditions.

Soils dominated by sands are generally non-cohesive and are more susceptible to erosion than silts and clays. However, sands settle out easily and can be controlled using simple management practices on site. For the proposed Alignment there are many locations where sand soils will be the dominant material within which works are occurring. This material is very difficult to form water tight

and compact diversion channels and detention facilities and as a result these types of devices are not proposed in such areas.

The primary device to be used will include the use of formed diversion bunds which will act as an infiltration device and in combination with the high infiltration rates of the sand soils themselves will act as an appropriate control device. The bunds will also have a series of rock filters installed within them which assist with slowing water flow and hence minimising erosion and also capturing any movement of sand downstream. While it is unexpected, in circumstances where peat and/or other soil layers are encountered within the sand soil profile, then the devices will be amended and decanting earth bunds and formal runoff diversion channels can be created.

#### 7.6 Culverts

Culvert installation, both temporary construction and permanent, is required in a number of locations with the key purpose of the culvert installations to allow for road construction, with the culverts providing for a dry environment over which the construction activity can then occur.

As with the stream diversion methodologies detailed below in Section 7.7, it is also important that the culvert activities are undertaken early in the construction program to ensure that the surrounding earthworks can be completed around these areas.

Fish migration and spawning is considered an important issue, and at all times during the fish migration period, fish migration will be able to continue in the normal manner with culvert construction creating no expected issues. This includes the methodology of physically transferring fish from upstream or downstream which shall be undertaken in accordance with the CESCP and any existing approved Council protocols. Appendix M of the CEMP, Volume 4 (Ecological Management Plan) outlines the detailed methodologies associated with fish migration and management.

Where culvert installation or extension is required within a stream channel this can be undertaken by two main methodologies, pumping around the area of works or establishment of a temporary diversion around the culvert footprint. For the methodology associated with a full stream diversion reference should be made to Section 7.7 below.

Prior to works commencing the specific methodology will need to be determined and will be detailed within the CESCP for the location. This determination, including specific culvert sizing, will be undertaken with endorsement of Greater Wellington Regional Council and will be based upon stream flows and upstream catchment areas, timing of works and the expected duration of works.

The typical methodology, for permanent flowing stream systems, for the culvert installation works allows for the entire stream works associated with the culvert installation to be undertaken in dry conditions, isolated from the existing stream flows.

- 1. A pump will be installed approximately 5m upstream of the extent of an upstream temporary bund. This pump will pump upstream flows around the work area to discharge back into the watercourse downstream of the culvert works. Sand bags or similar will be used to impound flows for this pump. The inlet of the pump will be supported above the base of the stream and will contain a fish grill such that no fish can enter the pump intake structure.
- 2. Where there is no practical ability to install a diversion channel as detailed below, pumping will remain as the primary methodology for stream diversion during the culvert works with the pump to have capacity for low flows only during which works will occur. This decision to pump as opposed to the installation of a diversion channel will be through the Project team and will form part of the CESCP's.
- 3. Where there is the ability to install a temporary diversion channel this methodology will be implemented as in Drawings CV CM 246 and 247 (Appendix H.E., Management Plan Appendices, Appendix H, Volume 5) and as detailed in Section 7.7 below.
- 4. With these controls in place, any fish observed in any of the pools within the work area will be removed by hand netting and released downstream of the work area. Any fish or eels discovered during excavation will also be captured and released downstream.
- 5. The initial excavation will remove the vegetation from the work area followed by the excavation of unsuitable material. This excavated material will be disposed of elsewhere on site within the catchment of other erosion and sediment controls.
- 6. Once all unsuitable material has been removed, the culvert area will be backfilled with structural material to an appropriate depth for culvert installation. The culvert will be installed with associated wingwalls, retaining walls and backfill as necessary. Rock rip-rap erosion control will also be installed at the inlet and outlet of the culvert. Care will be taken during the placement of this rip rap material so that a low flow channel for permanent fish passage purposes remains and will be maintained for the life of the culvert.
- 7. The associated activity over the culvert will occur (filling etc) with other erosion and sediment controls in place such as silt fences and super silt fences. When the works have been completed any disturbed area will be fully stabilised.
- 8. With the necessary ecological signoff stream flows can then be diverted through the new culvert structure.
- 9. Where the culvert works are associated with a culvert extension, at the outlet end of the existing culvert a plywood bulkhead with a 150mm diameter nova coil cut into and fixed into the bulkhead 100mm above the invert of the culvert will be installed. The bulkhead will be sealed to the base and sides of the culvert. A supplementary pump will be utilised if necessary to ensure a dry working environment. However, it is noted that a single 150mm diameter nova coil will pass

approximately 12 litres per second (full). With a head of 400mm (the height of the bulk head) a 150mm diameter nova coil will pass approximately 25 litres per second. The nova coils will be a sufficient length to allow low flows to discharge beyond the works area discharging below the lower bund feature. Figure Three below demonstrates this methodology.

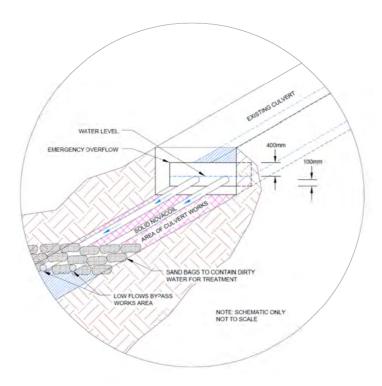


Figure Three – Schematic of Cleanwater Bypass

## For all culvert works:

- Prior to any works commencing with the culvert installation, a suitable weather window will be confirmed, the Greater Wellington Regional Council's Compliance Officers will be advised, and any concerns or further clarification at the time, will be addressed immediately and prior to any works commencing on site.
- Culverts are expected to be installed in sections with that particular section fully completed and stabilised within the day works programme.
- Any water within the works area will be pumped to a decanting earth bund or equivalent device which will be located away from, and discharge away from the stream environment.
- On completion of the culvert extension, all plant and resources will be demobilised and the site will be permanently stabilised to as per Greater Wellington Regional Counsil's requirements. Should any rock armouring be required to be placed at the outlet of the culvert for stabilisation of the streambed and banks, this can be accommodated as required.

In the event of high rainfall during the course of construction, or prior to leaving the site for more than a 24 hour period, the Project team will ensure the following:

- Any lose material that could enter a watercourse is to be removed.
- Any downstream sand bag barriers will be checked and, if required removed for heavy discharge events.
- All existing and additional sediment control measures will be inspected and secured and maintained where required should a significant rainfall event be imminent.
- The streambed in the location of the culvert will be fully stabilised to ensure no flows overtopping the upstream cofferdams create scour issues. It is expected that this will be achieved through geotextile with the geotextile appropriately trenched in at the head and toe of the area.

Extended working hours will be considered if it is believed significant benefit with regard to programme and environment impact is either required or possible.

# 7.7 Temporary or Permanent Stream Diversions

Stream diversions are required for either the establishments of a dry environment within the original stream channel to facilitate works or for the establishment of a new channel Alignment. The proposed methodology for stream diversion allows for the stream diversion to be constructed in a dry environment isolated from the existing stream flows. The methodology to be employed is shown within Drawings CV – CM 246 – 247 within Appendix H.E, Management Plan Appendices, Appendix H. Volume 5 and is as follows:

- 1. Excavation of the diversion channel will occur, to design drawings, leaving a clay plug at each end so that the stream does not breach the diversion.
- 2. Stabilisation of the diversion channel will occur to ensure it does not become a source of sediment and this will be undertaken utilising geotextile and rip rap material. Technical consultation with Greater Wellington Regional Council will occur to ensure that the realignment is fully stabilised and can accept stream flows. Ecological sign off will also be necessary for identified high value streams.
- 3. Any water within the works area will be pumped to a decanting earth bund. Pumped volumes will be minor and the decanting earth bund will have the decant manually raised during this process to allow for settlement of sediment and chemical treatment if necessary.
- 4. Once the diversion channel is stabilised (refer to 2 above) the downstream plug will be removed to allow stream flows to flow up the diversion channel, keeping some water within the channel to reduce scour problems when the upstream plug is also removed. The upstream plug can also then be removed allowing stream flows through the diversion channel.

- 5. A non erodible dam will be immediately placed in the upstream end of the original channel. This dam will include formation of a sand bag barrier with an impermeable lining to avoid seepage.Clay will then be placed up to this barrier to allow the necessary filling or activity to occur.
- 6. A non erodible downstream dam will be immediately placed to prevent backflow into the construction area. Fish recovery from the original channel will then occur and the channel drained by pumping to a decanting earth bund where treatment of the ponded water can occur prior to discharge to the receiving environment.
- 7. The original channel can then be backfilled forming part of the Expressway construction or the specific activity, such as culvert installation, undertaken.
- 8. While it is considered unlikely to be required, if necessary cleanwater diversion bunds will then be installed above the area of work to ensure that no offsite cleanwater enters the site of the realignment during the works period.
- 9. Material excavated from the diversion itself will be placed in stockpiles away from the stream diversion and outside of the identified flood plain area. While works will not commence until a fine weather window is available, geotextile will be available on site to cover exposed areas as required during the works if flood conditions result in stream flows entering the newly-formed channel pre stabilisation. The works will be staged such that if flood conditions result the area can be fully stabilised in a few hours to ensure no adverse effects. Any sediment deposited within the newly formed channel will then be pumped and removed to a decanting earth bund.
- 10. Once the works within the original channel has been completed, other appropriate controls, such as silt fences, will be installed below the area of works.

It is likely that there will be some rainfall events encountered during the course of construction. In the event of forecast rain, or before leaving the site for more than 24 hours the following will occur:

- Any loose material that could enter a watercourse is to be removed.
- Where possible, all exposed areas will be covered with geotextile to ensure no flows overtopping the existing stream banks create scour issues. It is expected that this will be achieved through geotextile with the geotextile appropriately trenched in at the head and toe of the area.
- All existing and additional erosion and sediment control measures will be inspected and secured and maintained where required.
- Additional mulch and geotextile / polythene will be kept on site at all times.
- Extended working hours will be considered if it is believed significant benefit with regard to programme and environment impact is either required or possible.

# 7.8 Bridges

Bridge construction will typically involve piling operations and reinforced concrete column and crosshead construction. Bridge beams will be cast off-site in the precast concrete construction yard and then transported to site and placed in position with the top slab poured in situ to a depth of 180 to 200mm thick. Barrier, settlement slabs and wing walls are also all poured in situ. In addition in some cases construction of the bridge will involve structures with sheet piling on either side of the stream system and placement of a concrete slab over the stream without diverting the stream.

Sixteen bridges will be established as part of the Project with 7 of these crossing watercourses, namely the Waikanae River, Wharemauku Stream, Waimeha Stream, Kakariki Stream and the Paetawa Drain. Specific erosion and sediment control measures will be applied to each of these 7 bridge sites with the Waikanae River bridge, as detailed within section 7.10 of this ESCP, providing an example of the nature of these works. All other bridges associated with roads will utilise the erosion and sediment controls as shown for the main Alignment works within Drawings CV – CM 200 – 231 within Appendix H.B (ESCP Drawings), Management Plan Appendices, Appendix H, Volume 5.

#### 7.8.1 Stone Column Installation

As part of the bridge establishment process there is the requirement to undertake ground improvement of the surrounding soils. This can be achieved by numerous engineering methodologies with the preferred methodology involving reinforcing the soils with densely compacted granular columns through the process of vibro - replacement. A vibrator is used to penetrate and displace the soil and to compact the clean stone in stages to form a dense column, as shown in Figure Four. Jetting water will be utilised to assist the penetration of the vibro head. The surrounding soil confines the granular columns and allows the columns to develop a higher bearing pressure relative to the surrounding ground. Overall the stone columns and surrounding soil form an integrated system with low compressibility and improved bearing capacity suitable for bridge placement.

# Vibroreplacement Process

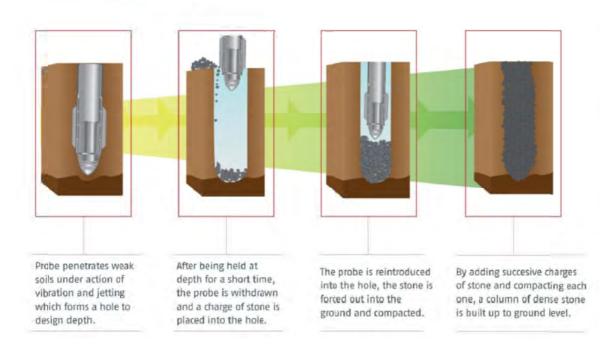


Figure Four - Vibroreplacement Process

It is proposed that the stone columns will be installed at the bridge abutments, will be of a 600mm diameter size and will be placed at 1.5m centres in a triangular grid. The stone columns will be located over an area of approximately 3000m2 at each bridge abutment.

The process for installation of the stone columns is as above and from an erosion and sediment control perspective these utilise a significant amount of water as part of the process. Approximately 150 to 200 m3 per day per operation will be utilised.

Drawing CV – CM - 245 (Appendix H.H, Stone Column Drawing), Management Plan Appendices, Appendix H, Volume 5 outlines the methodology for management of the water flow from the stone column works. Essentially the works area will be graded such that all runoff from the stone column installation and surface flows will be directed to an in-ground sump. Any stream edge of the works area will be protected with a super silt fence designed as per Drawings CV – CM 248 – 251, Management Plan Appendices, Appendix H, Volume 5. From the sump a construction pump will transfer the flows into a 70m3 container with an effective 63.5 m3 capacity. This will dewater into Container # 2 which will eventually dewater away from the works area or be recycled back to the stone column works area and supplement water supply. The level of the containers will be set up such that the first container will either be raised the second container lowered to allow the natural flows without the need for further pumping between container systems.

One baffle per container will be installed to assist with sediment settlement with the spacing of these baffles such that they will also enable cleaning with an excavator bucket as required without damaging the baffle system. It is envisaged that such maintenance will be focused within the first container system.

The addition of flocculant into the container system remains as an option and will be implemented as necessary. If required the water within the containers can be "held" by plugging the final outlet and allowing further settlement and potential for batch dosing with flocculant or utilisation at the discharge point.

For each area of stone column installation, the container system as outlined will be installed as a first priority and only after this is fully operational will the stone column installation itself commence. Availability of room to install such a system is critical. However, it has been assessed that a total area of 30m by 3m will be required for the treatment system and all of the sites assessed either can provide sufficient area under current contours or sites can be developed as part of the overall earthworks programme.

# 7.8.2 Bridge Pile Construction

All bridge pile construction, including the use of sheetpiles, will be undertaken outside of the stream channel (defined as the normal flow width of the stream) to which the bridge applies. Some of these works, however, will be within flood plain areas and as a result will be subject to inundation during periods of high stream flows.

The key erosion and sediment control methodology associated with the works is the use of non structural practices, and of particular importance is the use the following techniques:

- Weather forecasting will be undertaken using, for example, www.metvuw.co.nz which will provide an indication when high rain events are predicted and as such stream flows are also expected to be higher. For works adjacent to the Waikanae River, river level monitoring will also occur whereby Greater Wellington river level recordings will be monitored and as such will act as an indicator of high stream levels.
- Prior to predicted periods of high stream flows, all high environmental risk activities, such as the use of wet concrete, will cease within the flood plain area.
- While some temporary storage of fuels or storage of hazardous substances will be within the flood plain area they will be removed prior to and during flood events and all refuelling for activities in these locations will be via mobile units only.
- Prior to predicted periods of high stream flows, where practicable, all machinery, including mobile pumps will be moved to outside of the flood plain area.
- Any dewatering will be undertaken with particular care to ensure pH and water quality issues do not arise.

- Structural erosion and sediment controls will include the following measures:
- Utilisation of a fully stabilised surface, with compacted clean granular material or similar, over the entire working footprint adjacent to the stream system. This will ensure that any machinery working within this location does not generate sediment and during periods of high flow over these areas sediment is not generated or removed from the site.
- Any stockpiles of material, such as drill spoil material, will be removed from the site on sealed truck units. While it is envisaged that no stockpiles of spoil material will be located within the floodplain area, if this is required they will be temporary and short term only.
- Below any drilling or earthworks activities a super silt fence will be established in a horseshoe configuration which will capture any runoff from this activity. This will typically be located around the perimeter of the works and will ensure that the works area is fully isolated from the stream system itself. The super silt fence is designed for the capture and treatment of sediment only and is not designed for concrete contamination. As an alternative, or a backup to the super silt fence, filter socks may be appropriate and can be pegged to the ground surface below the works area. These will be bark or mulch filled filter socks which will assist with filtering sediment and also reducing the pH of concrete discharge if this results.

For concrete works in this location reference should be made to section 7.8.3 of this ESCP however the environmental controls are centred on the full removal of any slurry from the site. Housekeeping practices are critical in ensuring that concrete slurry is minimised. These practices include:

- Ensuring concrete spills are minimised;
- Cleaning up of any concrete spills that result; and
- Having a dedicated concrete wash area for items such as concrete tools and barrows.

For any concrete slurry generated this will be removed from the site with sucker trucks or will be discharged through a bark filled Filter Sock, removed the stream environment such that discharge can be checked for pH levels.

#### 7.8.3 Concrete Work

During construction of the bridges, it is proposed to minimise the amount of in-situ concrete that will be required. Pre-cast beams will be utilised as necessary. Cement contaminated water will require treatment before discharge, and this will either be conducted on site using treatment tanks and the water pH tested before discharge, or the water removed from site and treated elsewhere through the use of sucker trucks. Concrete placement will be carefully controlled to ensure minimal loss to the environment using pumps and skips. Concrete truck wash and pumps will occur on site with a dedicated concrete wash facility.

## 7.8.4 Bentonite/Polymer

A mobile bentonite or polymer plant is required for permanent pile construction on the bridges and the option remains where polymer may be used as an alternative during the drilling of piles. The material is a dense liquid used to support the sides of the excavation, preventing the sand and gravels collapsing into the excavation. The bentonite or polymer is displaced by the concrete for the pile by tremie pouring the concrete with the displaced bentonite or polymer captured and recycled by passing through a series of screens and filters to remove foreign material.

With the use of bentonite, dry bentonite clay will be stored within a roofed area, mixed in a formal mixer and then transferred to the storage tanks as a bentonite slurry. From these bentonite tanks the slurry is pumped to the pile as required. After each pile construction the area surrounding the pile will also be cleaned to ensure material is not unnecessarily transferred via vehicles or foot traffic around the construction area. As mentioned above any bentonite (or polymer) slurry is passed through a desanding device with the "clean" product then pumped to the storage tanks for further use. Any sand or unsuitable material collected as a result of the desanding process is removed offsite to a cleanfill facility.

Important aspects of the use of bentonite or polymer are as follows:

- bentonite is a naturally occurring clay;
- the bentonite system is based on a fully recycled system with no planned discharge from the operation; and
- The bentonite/polymer mixing and pumping system is based on a mobile plant which will be fully bunded when in position. This will capture any unexpected flows or spills from the operation and allow for full clean up to ensure no discharge from the site.

Further to the above a risk management approach will occur with the use of bentonite whereby hose couplings will be carefully checked and sandbags will be available as a contingency should temporary containment be necessary for any small spills of material

Overall the bentonite / polymer plant is considered an activity that is easily managed and that will create no effects on the receiving environment.



Plate Ten - Mobile Polymer Mixing and Pumping Unit

# 7.9 Pumping

Based on the results of the trial the water pumped from the peat excavation after it had been dug was relatively turbid. For the purposes of the trial, erosion and sediment control methodologies consisted of pumping to a grass environment some 100 metres away from the nearest watercourse. No turkey nest or detention device was utilised at the pump discharge. During pumping activity, however, it is noted that the pump intake was subject to blockage and intake of sticks and to avoid this a 100mm layer of hay and ballast material was utilised with the pump intake located within this layer. This in itself provided a filtering media where larger debris and particles were not sucked into the pump intake. This avoids physical blockages and damage but also avoids unnecessary sediment transfer to the pump outlet.

For pumping methodologies from excavations the pump intake will sit on 100mm layer of hay and ballast material to provide a filtering media where larger debris and particles are not sucked into the pump intake. This acts as a pre treatment system and also avoids direct damage to the internal workings of the pump.

The pump discharge will be, where possible, to grass environments well away from any watercourse which will be fenced from stock along the Alignment of the Designation. The trial undertaken demonstrated that a pump discharge 150m distance from the watercourse was adequate to ensure no discharge occurred. This will be the desired circumstance and will continue to be monitored during the pumping activity.

Where a grass buffer zone is unavailable and /or the stream system is closer than desirable all pumping will be to a turkeys nest as shown within Drawing Numbers CV – CM 248 – 251, Management Plan Appendices, Appendix H, Volume 5. This will discharge though a series of floc socks which will consist of Polyacrylamide within a filter sock. These are placed in a horseshoe configuration to ensure that flows over the sock are maximised and provides for full contact with the flocculant hence maximum possible sediment deposition.

In addition to the pumping from peat excavations other pumping activities will be required associated with dewatering and specific activities. These pumping activities will also be subject to specific management and will be discharged through treatment devices. This includes treatment container systems, turkey nests and buffer zones.

At all times the "Permit to Pump" system will be followed as per Appendix H.P of this ESCP. This provides for a "check and balance" that the appropriate management is being undertaken.

### 7.10 Waikanae River Works

The works in and around the Waikanae River are considered higher risk and from this perspective specific environmental management aspects of the activity have been detailed within this ESCP. These same environmental considerations will also apply to the other bridge locations over stream systems. Reference should be made to Drawings CV – CM – 500 to 508 within Appendix H.R (Waikanae River Environmental Plans), Management Plan Appendices, Appendix H, Volume 5 which detail 8 specific stages that will occur associated with the Waikanae River works. These are as detailed below with various steps outlined within each stage.

## 7.10.1 Stage One Site Set Up

- Step 1 involves ensuring the site is safe for pedestrians within the area and involves closing of the existing walkway. Alternative access provisions have been provided for as detailed within the Traffic Management Plan (Appendix O of the CEMP, Volume 4). No specific environmental controls are required during this activity.
- 2. Step 2 is critical in ensuring that the future works associated with the Waikanae River can occur without impacting on the Muaupoko Stream environment. This involves diverting the stream to a temporary alignment as shown on Drawing CV CM 501, Management Plan Appendices, Appendix H, Volume 5. Prior to these works commencing a super silt fence will be placed below the temporary diversion position to ensure that any sediment runoff that is created will be treated

through such a device prior to discharge into the Waikanae River. Section 7.7 of this ESCP outlines the stream diversion procedure that will be followed which essentially involves excavation of the new channel in a "dry" environment, full stabilisation of the new Alignment with geotextile and rock protection and then formally opening up the new diversion for stream flow.

During the construction process any water that collects within the diversion channel will be considered as dirty water and will be pumped to either a container treatment device that will be utilised for future stone column works or pumped to the long term wetland location at chainage 10250 which will provide adequate storage and treatment opportunities.

As part of this second step a super silt fence will be established along the Waikanae River edge which will remain in place during the backfilling and removal of the original stream alignment. Section 7.7 of the ESCP outlines this process whereby fish recovery, pumping and backfilling can occur. Once the original channel is backfilled the super silt fence will be extended along the Waikanae River bank for the full extent of works and return up the Muaupoko Stream channel to the Designation boundary.

Access for the works to be undertaken will be from the Project Alignment to the south.

- 3. Step 3 involves undercutting of an area of approximately 1000 m2 with this material to be placed outside of the identified flood plain area. This undercut will then be backfilled with clean granular material which has the purpose of long term flood protection. Environmental management will be provided for with the use of a clean granular material only and the placement of the super silt fence.
- 4. Step 4 involves the installation of a concrete retaining wall to protect the adjacent property. These works are outside of the identified flood plain area and will be managed by independent environmental controls likely to consist of topsoil bunds and decant systems. Any concrete waste will be removed from the site.

## 7.10.2 Stage Two Ground Improvement

1. Step 1 involves the excavation of the area subject to ground improvement such that this can then have stone column installation commence. Any material extracted, which is likely to be sand based, will be stored away from the flood plain area. During the excavation works the super silt fence installed along the Waikanae River boundary will remain as the primary environmental control. It is noted, however, that due to the sand nature of the soils in this environment that the runoff expected as a result of the works will be minor.

Stone column installation in this area can commence on completion of the excavation with this activity fully detailed within Section 7.8.1 of this ESCP.

2. Step 2 involves the regrading of the ground adjacent to the ground improvement location which is designed to provide for a refuge area and laydown area during the works. This is located outside of the flood plain and will be a location whereby prior to and during flood events machinery and hazardous material that can be practically moved can be relocated to this area. The area will be covered with a clean granular fill and will also have a decanting earth bund which provides a dual purpose treatment. During the excavation of the refuge area the decanting earth bund will provide a treatment device for the excavation itself while after the excavation works in this location the decanting earth bund will provide a facility to pump sediment laden runoff for treatment. The decanting earth bund will have a capacity of 150 m3 and with the nature of the sand soils in this location may need to be lined with an impervious lining to ensure water does not infiltrate back into the works site. Discharge will be to the Muaupoko Stream.

The super silt fence will be extended to the refuge area with the refuge area itself protected with a diversion channel on the eastern and northern boundaries.

3. Step 3 involves the undertaking of piling works where either polymer of bentonite will be utilised. The super silt fence in this location remains as the primary control measure; however, as detailed within Section 7.8.4 of this ESCP, independent controls for the bentonite / polymer plant will also be established.

# 7.10.3 Stage Three Sheet Piles

- 1. Step 1 involves the installation of sheet piles using vibration or jetting to enable the construction of the pile cap in this location. Dewatering of the area may be necessary during these works with this to occur to the decanting earth bund. The treatment containers also installed for the stone columns will provide a further back up for treatment during the dewatering process.
- Step 2 also involves the completion of the piling works for the southern abutment. The super silt
  fence in this location remains as the primary control measure; however, as detailed within
  Section 7.8.4 of this ESCP, independent controls for the bentonite / polymer plant will also be
  established.

## 7.10.4 Stage Four Columns

1. Step 1 and 2 involves the construction of columns and also the cross heads at the southern embankment. During these works the super silt fence and the decanting earth bund remain in place as the primary control measures with the Muaupoko Stream fully protected from the works area. Clean granular fill will also be utilised to ensure that the platforms from which the works are to be undertaken remain clean.

## 7.10.5 Stage Five Re-profiling

- Step 1 involves the construction of cross heads and then the MSE abutment wall as shown on Drawing Number CV - CM 505, Management Plan Appendices, Appendix H, Volume 5.
   Discharge from these activities is expected to be minor; however, if it does occur then this will be pumped to the decanting earth bund. During works that involves concrete activities any discharge will be checked for pH adjusted accordingly.
- 2. Step 2 involves the reprofiling of the river bank and the establishment of the new Muaupoko Stream channel. To achieve this, the super silt fence on the Waikanae River bank will be removed and relocated to below the ground improvement location. The Muaupoko Stream will remain protected by the existing super silt fence.

The Waikanae River will be diverted by establishment of a geotextile blanket filled with rock from the river channel. This will ensure that no foreign material is introduced into the river system but will also ensure that the diversion will be established from clean material and will not be subject to scour or significant sediment discharge. Works will occur during low flow periods, however, the diversion is designed to divert all the flows away from the area of the proposed works. Some water is expected to collect within the works location from both leakage through the geotextile blanket over time and also through ground infiltration; this water will be pumped as necessary to the decanting earth bund for treatment and safe discharge. Where re profiling of the main Waikanae River bank is required this will also occur as above utilising a geotextile blanket filled with rock diversion which will allow works to occur in the dry with any dirty water that results within the diversion to be pumped to the decanting earth bund for treatment and safe discharge.

The works include the establishment of the necessary rip rap material and the new Muaupoko Stream profile. These will be undertaken using clean rock and the new channel will be fully stabilised prior to allow any flows into this environment. Once the works are completed the Muaupoko Stream will be diverted, the Waikanae River diversion removed and the super silt fence re-established on the new river bank.

### 7.10.6 Stage Six Deck Placement

1. Steps 1 and 2 involve the construction of the settlement slab and the placement of the deck units at the southern location. Deck concrete pours will be undertaken to compete this part of the process. Concrete discharge is expected to be minimal but as with other stages the decanting earth bund remains in position and provides a easily accessible location for pumping contaminated water for treatment (or removal) as necessary.

## 7.10.7 Stage Seven Northern Embankment

1. Step 1 involves the opening of the footpath on the southern side of the river. At the same time the footpath on the northern side will be closed as described in the Construction Methodology

Report (Technical Report 4, Volume 3) and Construction Traffic Management Plan (Appendix O of the CEMP, Volume 4).

2. Step 3 to Step 6 is a repeat of the same process as followed on the southern side of the river. The refuge area location as shown on Drawing CV - CM 507, Management Plan Appendices, Appendix H, Volume 5 will be established and as with the southern location will have a decanting earth bund established for the same purpose. In addition the permanent stormwater wetland facility at chainage 10850 will be available as a backup facility in the circumstance that an additional treatment device is required.

River bank reprofiling is again part of this process and will follow the same procedure as Stage 5 on the southern embankment.

# 7.10.8 Stage Eight Deck Placement

- 1. Steps 1 and 2 involve the use of cranes to place the deck units over the river. A topping slab is to be completed and the final road pavement established.
- 2. Once the full bridge deck is completed and the site is considered to be fully stabilised then environmental controls can be removed from both the southern and northern locations. The super silt fence will remain in place for a period of time to ensure that any associated Alignment works have this extra level of environmental protection in place.

During all the works within the Waikanae River the issue of fish migration and spawning periods is acknowledged. At no time will the river flows be fully stopped and fish passage will remain throughout. The key environmental consideration is that associated with minimisation of discharge of contaminants and the controls measures as detailed above are designed to achieve this. During the fish spawning and migration periods particular care will be taken and ongoing monitoring will occur to ensure no effects result.

# 7.11 Works in Swales/Overland Flow Paths and Placement of Pipes away from Watercourses

Part of the Project earthworks activities will include the placement of pipe networks for stormwater management and other utility services. Where these are to be placed within, under or over watercourses the methodologies referred to above should be referenced. Where they are to be placed away from watercourses, the methodologies to be employed are as below. These works are typically lineal in nature and require removal of spoil and placement of pipe hardfill bedding and backfill.

The first step is to identify the specific location of the works and the nature of the environment within which it is to be undertaken. In particular, from an environmental perspective, note will be made of any specific stream systems or overland flow paths through which the works will occur.

For all works outside of the stream systems

- Provide cesspit protection for all adjacent cesspits as per Drawing Numbers CV CM 248 251,
   Management Plan Appendices, Appendix H, Volume 5. Ensure this practice does not result in the full blockage of cesspits and result in localised flooding.
- If the works are adjacent to watercourses these will be protected by placement of either Filter Socks or Silt Fence between the works and the stream environment. These will be maintained to ensure capacity and functionality remains and can be moved with the works as they progress.
- Undertake the works with excavation, placement of pipes and backfilling as necessary and ensure that completed areas are fully stabilised at the completion of the day's work. This stabilisation will be achieved through the use of hay mulch, hardfill or temporary placement of geotextile.
- Stockpiles of any spoil material will be avoided by removal of this material offsite, however, where necessary they will be stockpiled in a compacted manner and will be protected from erosion and dust generation by the placement of geotextile over the stockpile. Any stockpile of hardfill material will be placed such that it is not subject to scour from surface runoff and is also protected during periods of rain with Filter Socks.

If works are to be undertaken within a swale or overland flow path care will be applied such that these can continue to operate as designed during the works themselves. Temporary coffer dams may be used within swales, both upstream and downstream during periods of flow, with connected solid novacoil pipes taking any swale water around the works area on a temporary basis. On completion of such works the coffer dams would be removed and a stabilised surface will remain.

Within overland flow paths the key erosion and sediment control methodology revolves around ensuring material is not stockpiled within such flow paths and the flow path is stabilised on completion of works and during works when rain is forecast.

## 7.12 Chemical Treatment

Two peat soil samples were collected from the Alignment which were considered to represent the peat material expected to be encountered during the earthworks phase of the operation. These samples were collected during geotechnical investigations. These were tested by Envirolab Geotest Limited for soil particle size and were also subject to bench tests with numerous flocculants by Orica Chemnet Limited. The purpose of this sampling was to determine if water quality could be improved with the use of flocculants or if unassisted settlement was considered satisfactory in terms of erosion and sediment control.

Soil sample TP203 (J487) particle size analysis is detailed below. This soil represents organic silt with some clay and some fine to medium sand. Fibrous organic material was present in the soil sample.

Coarse & Inte	rmediate Fraction	Fine Fraction		
Sieve Size	% Passing	Sieve Size	% Passing	
75.0mm	100	2.00mm	100	
63.0mm	100	1.18mm	100	
53.0mm	100	600µm	99	
37.5mm	100	425µm	98	
26.5mm	100	300µm	97	
19.0mm	100	212µm	96	
13.2mm	100	150µm	95	
9.50mm	100	90µm	92	
6.70mm	100	63µm	91	
4.75mm	100	<63µm	91	

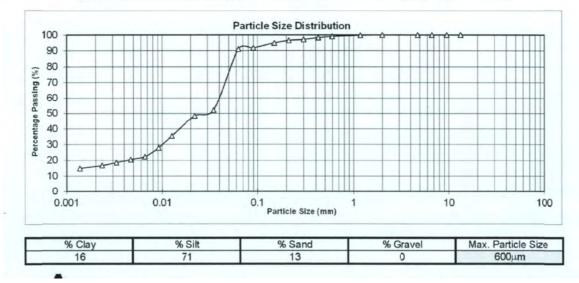


Figure Four – Particle Size Analysis TP203

Soil sample TP205 (J489) particle size analysis is detailed below. This soil represents an organic silt with some clay and some fine to medium sand. Fibrous organic material was also present in the soil sample with this sample containing more fibrous rootlets and spongy branches.

Coarse & Inte	rmediate Fraction	Fine Fraction		
Sieve Size	% Passing	Sieve Size	% Passing	
75.0mm	100	2.00mm	100	
63.0mm	100	1.18mm	100	
53.0mm	100	600μm	99	
37.5mm	100	425µm	97	
26.5mm	100	300µm	96	
19.0mm	100	212μm	94	
13.2mm	100	150µm	91	
9.50mm	100	90µm	86	
6.70mm	100	63µm	85	
4.75mm	100	<63µm	85	

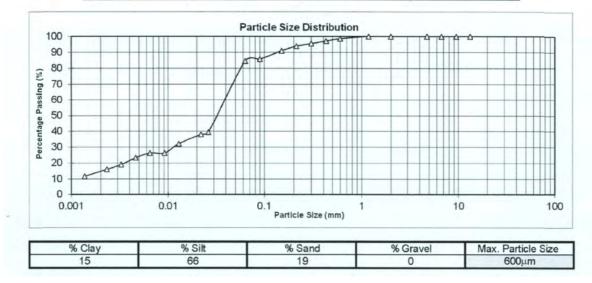


Figure Five - Particle Size Analysis TP205

Flocculation testing was undertaken by Orica Chemnet Limited and through the flocculation testing it was recorded that both of the samples provided had fine colloidal particles which remained in suspension long enough to potentially create settling issues during treatment of sediment laden runoff. The pH of the samples tested were considered very low at 4.09 and 4.01.

It is recommended that the Project does not use an aluminium based coagulant (such as Poly Aluminium Chloride or Aluminium sulphate) for the soil types due to the relatively low starting point pH and relatively high dose rates required followed by post treatment pH correction, or pre treatment pH adjustment and then difficult subsequent treatment.

Other flocculants were tested with the samples with effective results noted with the use of polyacrylamide. B610 (Polyacrylamide) performed well on this sample (~6 to 12ppm) with relatively low settled water and no effect on pH. B610 can be dosed via a "floc sock" where sediment laden water is passed over the sock to dissolve product and the floc sock size/number is customised for the flow rates. If sufficient mixing energy can be engineered into the dosing regime the polyacrylamide option is considered the preferred option, and this erosion and sediment control plan reflects this methodology. Appendix H.L (Chemical Treatment Plans) of this ESCP provides the full bench test report and the associated material safety data sheet for polyacrylamide.

Unassisted settling data showing the turbidity readings for the soil samples is as follows:

Time	Sample J487	Sample J489
Start	>1000	>1000
1 hour	>1000	486
3 hours	>1000	482
5 hours	926	451
15 hours	683	386
24 hours (1 day)	615	298
48 hours (2 days)	498	230
72 hours (3days)	384	158
96 hours (4days)	343	128
192 hours (8days)	323	122

Table Four - Soil Settling Bench Tests

The results above shows sample J487 had the highest risk in terms of settled water turbidity vs time with sample J489 also showing a high risk in terms of settled water turbidity vs time.

# Sample J487

L3RC ppm	рН	NTU at 10 min	610 ppm	рН	NTU at 10 min
0	4.09	>1000	0	4.09	>1000
5	4.08	>1000	3	4.09	>1000
10	4.07	987	6	4.09	486
20	4.05	709	9	4.09	43.7
30	4.01	516	12	4.09	39.2
40	3.98	4.57	15	4.09	69.5
50	3.97	2.42	18	4.09	129
60	3.96	2.67			
70	3.96	2.71			

Sample J489

L3RC ppm	рН	NTU at 10 min	610 ppm	рН	NTU at 10 min
0	4.01	>1000	0	4.01	>1000
5	4	>1000	3	4.01	512
10	4	846	6	4.01	99.6
20	3.98	493	9	4.01	22.3
30	3.97	86.1	12	4.01	14.6
40	3.96	8.79	15	4.01	87.4
50	3.96	1.66	18	4.01	216
60	3.94	5.69			
70	3.92	29.7			

Table Five - Soil Flocculant Bench Tests

These results clearly demonstrate the effectiveness of chemical treatment with Polyacrylamide demonstrating that at relatively low dosage rates turbidity levels can generally be significantly reduced.

#### 7.13 Construction Yards

Establishing the construction yards will typically involve stripping of topsoil, contouring and placement of hardfill dependent upon the use of the yard area. Construction yards will be required to have adequate erosion and sediment control and due to the temporary nature of the exposed area, will be based upon super silt fences and during construction followed by a progressive cover of hard fill material. This hard fill will consist of clean granular metal compacted with a track roller.

A full set of drawings for the construction yards is contained within Construction, Construction Office and Yard Plans, Volume 5.

## 7.14 Rip Rap Placement

Rip rap will be placed below culvert outlets to avoid erosion of these areas and to ensure that undercutting of the culvert headwall does not result. The placement of this rip rap material is such that it will be undertaken at the same time as the culvert placement itself and therefore can be undertaken during a period when flows are fully diverted around the work area. This will also apply to any concrete works that may occur associated with the rip rap placement to ensure stability of the rip rap material. Where such concrete works are to occur they will be undertaken in a dry environment and the concrete fully cured and swept thoroughly prior to allowing water to pass over the finished surface.

Where rip rap material is to be placed to serve a function such as stream or river bank erosion protection, such as that proposed below the bridge over the Waikanae River, then again the works

will be undertaken such that the rip rap will be placed in a dry environment. From an erosion and sediment control perspective the sequence of works will be as follows:

- Operate all machinery from behind a super silt fence which is in place along the stream bank edge:
- Install sandbags within the stream system to isolate the area within which the rip rap works will occur. On the inside edge of the sandbags place a mulch filled filter sock to ensure that any sediment generated during the works is captured and or filter prior to discharge;
- Excavate the stream bank profile to the final contours and place the necessary geotextile and rip rap bedding on the excavated surface;
- Ensure the rip rap material is clean in nature and does not contain finer material and carefully place within the stream bank position as necessary;
- Remove any sediment that has accumulated within the sandbags and filter sock coffer dam and
  if necessary remove any ponded contaminated water via pump away from the stream system;
  and
- Remove the sandbags and filter sock coffer dam and allow the stream to flow back to normal flow conditions.

# 7.15 Wetland and Offset Storage Facilities

Wetland and offsetting storage facilities are to be constructed along the Expressway Alignment as detailed in Technical Report 22, Volume 3 and Drawings CV-SW-100 – 394, Management Plan Appendices, Appendix H, Volume 5. While these are relatively large footprints, they do not, however, involve significant volumes of earthworks. The areas form an important part of the Project, and, from an erosion and sediment control perspective, they will need to be constructed in an isolated manner. The works will involve the use of an excavator and motorscrapers removing the peat material from the location and then final contouring to be undertaken. No ground improvement works are expected through this operation.

Prior to these works commencing the perimeter of the excavation area will be marked with a topsoil or peat bund such that it is clear where the works boundary exists to prevent machinery moving outside of and disturbing unnecessary areas. Further the bund will be formed such that it can act as an impoundment area if necessary with decanting devices installed. Groundwater levels are expected to be high within these locations and as a result during excavation some pumping may be necessary. This will be achieved through the undertaking of the excavation on a cell by cell basis whereby the area will be worked within one cell and any water that requires pumping and/or disposal can be done so through an adjacent cell. It is expected that chemical treatment will not be necessary; however, if this is required it can be applied as per Section 7.12 of this ESCP.

For the development of the offsite wetlands reference should be made to Appendix M of the CEMP, Volume 4 (Ecological Management Plan) which outlines the specific works required. For each of these areas a CESCP will be developed and certified by GW prior to works commencing.

# 8 Planning Considerations

Section 3.0 of this ESCP provides an overview of the planning framework associated with the earthworks activity and the Project. This section that follows details the specific statutory provision of relevance to earthworks and places this ESCP in the context of these provisions.

### Resource Management Act (RMA)

Section 104(1) of the RMA requires regard to be had to specific factors, subject to Part 2 of the RMA ("Purposes and Principles"). The purpose of the RMA is to promote the sustainable management of natural and physical resources. Sustainable management means the use, development and protection of natural and physical resources in a way, or at a rate, which enables people and communities to provide for their social, economic, and cultural wellbeing and for their health and safety while: sustaining the potential of natural and physical resources (excluding minerals) to meet the reasonably foreseeable needs of future generations; and safeguarding the life-supporting capacity of air, water, soil, and ecosystems; avoiding, remedying or mitigating any adverse effects of activities on the environment.

With reference to Table Seven below, sections 105 and 107 requires regard to be had to additional matters associated with the discharge of contaminants. This ESCP outlines a comprehensive programme of implementation of erosion and sediment control measures which will be the subject of detailed design, implementation and ongoing monitoring to ensure effectiveness. All of these aspects confirm that the effects of any sediment yields associated with the construction activity will be negligible.

#### Overall Assessment of Earthworks and Streamworks Activities

Earthworks Assessment Criteria	Description
Erosion and Sediment Control and Environmental Management	Environmental control measures will be fully implemented as part of the Project implementation. These will be implemented in accordance with this ESCP and the CESCPs which will require future Council certification on an as-required basis.

Water Quality	All discharges will be treated to a minimum standard associated with Wellington Guidelines. This standard is exceeded in many circumstances and includes chemical treatment, comprehensive methodologies and stabilisation techniques.
Aesthetics and odour	After reasonable mixing, any sediment discharged will not give rise to:  Conspicuous oil or grease films, scums or foams, or floatable or suspended materials; Any conspicuous change in the colour or visual clarity; and/or Any emission of objectionable odour.  Environmental controls are comprehensive and reflect the best practical option approach while also adopting standards and monitoring of discharges.  With treatment and after mixing no conspicuous change to the receiving waters is expected. Similarly, no emission of objectionable odour is expected.
	objectionable educitie expected.

Table Seven - Earthworks Assessment

## 9 Conclusions

A range of earthworks and streamworks activities (including bridges) that will be undertaken as part of the Project have numerous requirements under regional policy and planning documents. Several key items are of importance in terms of erosion and sediment control:

- Proximity to sensitive stream systems,
- Values of the receiving environments adjacent to, or downstream of, the Project, and
- Areas of exposed soils.

These items have been considered in full in developing this ESCP and are reflected in the overall approach taken.

The NZTA has adopted as part of its wider national Environmental Management Plan (NZTA EMP), a series of erosion and sediment control objectives for roading projects. This part of the NZTA EMP is attached as Appendix O of this ESCP and is also detailed within Section 3 of this ESCP. These objectives have been fully considered and are reflected within this ESCP.

The following key points are noted for the erosion and sediment control methodologies for the Project.

- The statutory framework and policy guidance from Greater Wellington Regional Council and the NZTA require the Project team to be aware of, and ensure, implementation of appropriate erosion and sediment controls including construction and maintenance of these devices.
- A range of erosion and sediment control measures are proposed to be employed on the Project. These will be implemented and maintained and will at all times achieve as a minimum the requirements of the Wellington Guidelines.
- The erosion and sediment control methodology relies on a future erosion and sediment control plan (referred to as a CESCP) to be submitted at a later date, pre any earthworks activity, to allow for flexibility, Project team input and also input from various other bodies such as Greater Wellington Regional Council.
- Chemical treatment will be implemented on the site as a risk management tool and will be done so in accordance with the Chemical Treatment Plan provided with this report.

With these measures in place it is considered that overall, any adverse effects on the receiving environment will be no more than minor.

#### 10 References

Auckland Regional Council (March 1999). Erosion & Sediment Control Guidelines for Land Disturbing Activities in the Auckland Region, Technical Publication No. 90.

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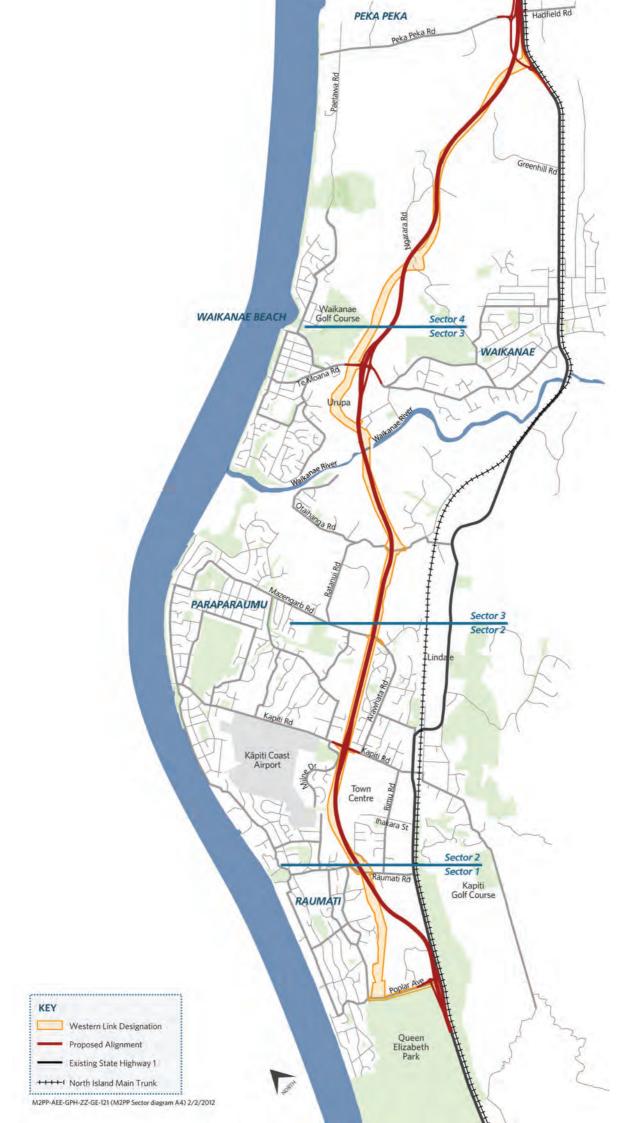
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Park, M. Ecological Management Plan, Appendix M of the CEMP, Volume 4 of the MacKays to Peka Peka Expressway AEE.

Minchington, J. Construction Traffic Management Plan: Appendix O of the CEMP, Volume 4 of the MacKays to Peka Peka Expressway Project AEE.

Smith, G. Contaminated Soils and Groundwater Management Plan: Appendix K of the CEMP, Volume 4 of the MacKays to Peka Peka Expressway Project AEE.

Appendix H.A Sector Diagram



Appendix H.B ESCP Drawings: Refer to Drawings CV-CM-200 - CV-CM-231 and CV-CM-234, Management Plan Appendices, Appendix H, Volume 5

Appendix H.C Pre Load Drawing: Refer to Drawing CV-CM-244, Management Plan Appendices, Appendix H, Volume 5

#### Appendix H.D

Peat Replacement Drawing: Refer to Drawings CV-CM-240 - CV-CM-243, Management Plan Appendices, Appendix H Volume 5

Appendix H.E Stream Crossing Methodology: Refer to Drawings CV-CM-246 -CV-CM-247, Management Plan Appendices, Appendix H, Volume 5 Appendix H.F USLE Plans: Refer to Drawings CV-CM-260 - CV-CM-270 and CV-CM-272 - 282, Management Plan Appendices, Appendix H, Volume 5

Appendix H.G USLE Calculations

# **USLE Calculation M2PP Pre Earthworks - Main Project Footprint**

Whareroa Wharemauku Waikanae Waimeha Ngarara Catchment 1
Catchment 2
Catchment 3
Catchment 4
Catchment 4
Catchment 5

R factor based on NIWA HIRDS Data

K Factor based on soil samples and soils /gravels to be utilised - grass cover LS Factor based on different slopes with a uniform 100m slope length - this is the worst case scenarion with the installation of contour drains reducing this value

C and P Factors based on a pastoral surface

Duration - for purposes of risk assessment has been based on 2 months total for each stage to provide comparison with earthworks scenario Sediment Delilivery Ratio - based on a high infiltration rate and irregular surface capturing flow and sediment - 0.25 assumed figure Efficiency - based on 0% as no control measures in place with existing situation

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r A			71 0.132	71 0.132	71 0.132		71 0.5016	71 0.5016	71 0.5016	71 0.5016		71 0.132	71 0.132		71 0.132			71 0.1188	71 0.1188	71 0.1188		71 0.1188	71 0.1188	71 0.1188	71 0.1188			71 0.1188	71 0.1188	71 0.1188			71 0.1188	71 0.1188
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sdr		0.25	0.25	0.25	0.25		0.25	0.25	0.25	0.25		0.25	0.25	0.25	0.25		0.25	0.25	0.25	0.25		0.25	0.25	0.25	0.25		0.25	0.25	0.25	0.25		0.25	0.25	0.25
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Yield		0.017264191	0.017727942	0.018781497	0.0199522		0.005045395	0.002769498	0.007877099	0.021102777		0.011473169	0.008482328	0.053746385	0.151642262		0.001367837	0.0025218	0.015144147	0.090508167		0.006664444	0.000345695	0.003721867	0.00775143		0.000863443	6.86958E-05	0.001073676	0.013213344		9.37866E-05	7.31278E-05	0.002022141
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											31.6671		
0.314		0.7341	0.9991	2.4762	1.5929	1.0872	0.9978	2.5794	0.7578	3.3284	0.454	3.7091	0.9225
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0.000292558	0.000332399	0.003796993	0.017772422	5 27258E_05	0	0.000607268	0.00539707		0.000894238	0.001616567	0.005884869		0.000274127	0.000204979	0.006260499		0.000316821	4.21039E-05	0.001164453		0.003507197	0.003515672	0.01 /0/5511		9.14536E-05	1.108E-06	0.012963942		0.001849368	0.009008858	0.019872391	10000	0.001344585	0.008194298	0.021818839	0.000851078	0.001948966	0.01618339	0.041829787	0.000401898	0.001628016	0.020644344	0.035824175	0.008548211	0.006778722	0.02451681
0	0	0	0	c	0	0	0		0	0 0	o c		0	0	0 0	>	0	0	0 0		0	0 (	0 0		0 0	0 0	00		0 0	0	0	d	o c	0	0	0	0	0 0	0	0	0	0 (	0	0	0	0
0.25	0.25	0.25	0.25	0.05	0.25	0.25	0.25		0.25	0.25	0.25	0.45	0.25	0.25	0.25		0.25	0.25	0.25		0.25	0.25	0.25		0.25	0.25	0.25		0.25	0.25	0.25	C	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25
0.16	0.16	0.16	0.16	0 18	0.16	0.16	0.16		0.16	0.16	0.16	2	0.16	0.16	0.16		0.16	0.16	0.16		0.16	0.16	0.16		0.16	0.16	0.16		0.16	0.16	0.16	0	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
-	_	-	-	+	-	-	1		<del>.</del> .			-	-	-		-	-	-			-					- ,					1	,		-	-	-	-		-	-	-	<del>.</del> .	-	-	-	-
0.02	0.02	0.02	0.02	000	0.02	0.02	0.02		0.02	0.02	0.02	20.0	0.02	0.02	0.02		0.02	0.02	0.02		0.02	0.02	0.02		0.02	0.02	0.02		0.02	0.02	0.02		0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
0.3457401	1.6420015	4.6388912	7.3920692	0.3457401	1.6420015	4.6388912	7.3920692		0.3457401	1.6420015	7.3920692	1.005002	0.3457401	1.6420015	4.6388912		0.3457401	1.6420015	7.3920692		0.3457401	1.6420015	7.3920692		0.3457401	1.6420015	7.3920692		0.3457401	4.6388912	7.3920692	1000	1 6420015	4.6388912	7.3920692	0.3457401	1.6420015	4.6388912	7.3920692	0.3457401	1.6420015	4.6388912	7.3920692	0.3457401	1.6420015	4.6388912
0.1188	0.1188	0.1188	0.1188	0 1188	0.1188	0.1188	0.1188		0.1188	0.1188	0.1188		0.1188	0.1188	0.1188		0.1188	0.1188	0.1188		0.1188	0.1188	0.1188		0.1188	0.1188	0.1188		0.1188	0.1188	0.1188		0.5016	0.5016	0.5016	0.1188	0.1188	0.1188	0.1188	0.5016	0.5016	0.5016	0.5016	0.5016	0.5016	0.5016
7	7	7	71	7		71	71		7	F 7			77	7	<u> </u>		71	۲ i	<		7	F i	< F		F 1	<b>5</b> 7	7 7		<u> </u>		71	i	7 7	7	71	7.	71	F 7	5	71	71	7	7.1	7	7	71
0.1254	0.03	0.1213	0.3563	96600	0	0.0194	0.1082		0.3833	0.1459	0.188	1000	0.1175	0.0185	0.2		0.1358	0.0038	0.0372		1.5033	0.3173	0.5455		0.0392	0.0001	0.2599		0.7927	0.2878	0.3984	1007	0.069	0.062	0.1036	0.3648	0.1759	0.517	0.8386	0.0408	0.0348	0.1562	0.1701	0.8678	0.1449	0.1855
Area 3 Slope 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Area 4	Slope 5-10%	Slope 10-20%	Slope >20%	Area 5	Slope 0-5%	Slope 5-10%	Slone >20%	Area 6	Slope 0-5%	Slope 5-10%	Slope 10-20%	Area 7	Slope 0-5%	Slope 5-10%	Slope >20%	Area 8	Slope 0-5%	Slope 5-10%	Slope 10-20%	Area 9	Slope 0-5%	Slope 5-10%	Slope >20%	Area 10	Slope 0-5%	Slope 10-20%	Slope >20%	Area 11	Slone 5-10%	Slope 10-20%	Slope >20%	Area 12 Slope 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Slope 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Slope 0-5%	Slope 5-10%	Slope 10-20%

State   Colored   Colore		i c	0000	ì		1000				L	•	000000000			
Separation		Slope 0-3%	0.9062	7 7	0 1188	1 6420015	0.02		0.16	0.25	0 0	0.002300603			
State of the control of the contro		Slone 10-20%	0.3967		0 1188	4 6388912	000		0.16	0.25	· c	0.0124177			
State of the control of the contro		Slope >20%	2.3455		0.1188	7.3920692	0.02		0.16	0.25	0	0.116994713		3.8119	
Stage 5-19,		Area 16													
State 10 ft		Slope 0-5%	0.5971	7	0.5016	0.3457401	0.02	-	0.16	0.25	0	0.005881697			
State   Colore   Co		Slope 5-10%	0.1606	71	0.5016	1.6420015	0.02	-	0.16	0.25	0	0.0075132			
Single - 5.07%   Colore   Color   Co		Slope 10-20%	0.1583	7	0.5016	4 6388912	0.02	-	0.16	0.25	C	0.020921893			
Stage   5 Per 1968   1 Per 19		Slone >20%	0 0991	7	0.5016	7 3920692	000	-	0.16	0.25		0.02087111		1 0151	
Steps - Color   Steps - Colo		Area 17					1				,				
Supple 5-75   Control of the contr		Olege P	11000	7	0	0 0 4 1 4 0 4		•	7		c	100001			
Steps 10-25%   O. 10.000-00-00-00-00-00-00-00-00-00-00-00-0		310pe 0-3%	0.0000	- i	0.1100	0.5457401	0.02		00	0.23	<b>&gt;</b> (	0.001399271			
State   20%   Control		Slope 5-10%	0.0629	7	0.1188	1.6420015	0.02	-	0.16	0.25	0	0.00069693			
Special Color		Slope 10-20%	0.1984	7	0.1188	4.6388912	0.02	-	0.16	0.25	0	0.006210415			
Stage 6-56,   Control of the contr		Slone >20%	0.3729	7	0 1188	7 3920692	000	-	0.16	0.25	C	0.018600438		1 3197	
State   Control   Contro		0,027,000	22.00	-		2000200.	20:0	-	2	0.10	>	000000000000000000000000000000000000000		5	
Shippe 69%		Area 18													
State 5-19%   Colore 10-10%   Colore 10-10%		Slobe 0-5%	0.4202	7	0.1188	0.3457401	0.02	-	0.16	0.25	0	0.000980326			
Shippe 10-25%   O.1016   O.1016   O.1016   O.25   O.		Slope 5-10%	0.2141	7	0.1188	1.6420015	0.02	-	0.16	0.25	0	0.00237222			
Stope 1-20%   Other Colone		Oct 20 000/	! 6	. 7	0 0			. ,		) i		11000000			
Supple 20%   Control 10   Control 20%   Co		210pe 10-20%	0.182	<b>-</b> i	0.1188	4.6388912	0.02		0.10	0.25	<b>&gt;</b>	0.005697054			
Area 14   Area 14   Area 15   Area		Slope >20%	0.053	7	0.1188	7.3920692	0.02	-	0.16	0.25	0	0.002643666		0.8693	
Skep 6-19,		Area 19													
State   Control of the control of		, ou o	0	7	0	0 0 0 4 5 7 4 0 4		•	0	100	c	70000000			
Shope 10-287, 0.1468   71 0.0016 4.658812 0.02   1 0.16 0.25   0 0.01966613   1.22/2   1.22		%c-n adole	0.9161	-	0.3016	0.0457401	0.02	-	00	0.20	>	0.00302300			
Shope 1-02%   Otto		Slope 5-10%	0.0531	7	0.5016	1.6420015	0.02	-	0.16	0.25	0	0.002484128			
State Control		Slope 10-20%	0.1488	71	0.5016	4.6388912	0.02	-	0.16	0.25	0	0.019666315			
March 17   17   17   17   17   17   17   17		Slone 200/2	0 1062	7	0.5016	7 3920692	000	-	18	0.05		0.022366416		1 2242	
Stope 5-10%   Oxfore 71   Oxfore 81   Oxfore 72   Oxfore 92   Ox	1	0/05/ adoin	0.1002	-	0.00.0	1.002002	20.0	-	2.0	0.4.0		0.055000		7277	
Stope 6-70%         0.00002540131         0.0000254013 <th></th> <td>Area 20</td> <td></td>		Area 20													
Steps 5-10%, 0.0207, 11 0.1188   1642016   0.02   1 0.16   0.25   0 0.0000289518   0.15   0.15   0.25   0 0.0000289518   0.15   0.15   0.25   0 0.0000289518   0.15   0.15   0.25   0 0.0000289518   0.15   0.15   0.15   0.25   0 0.0000289518   0.15   0.1		Slobe 0-5%	0.1055	7	0.1188	0.3457401	0.02	-	0.16	0.25	0	0.000246131			
Stope 10-20%		Slone 5-10%	0.000	7	0 1188	1 6420015	000	-	0.16	0.25	c	0.000229355			
Single 10-20%   Outside 17		200 C	0.000	: i		0.0000	1 0		2 6	9 0		0.0000000000000000000000000000000000000			
Stope 10-27%   Control of the cont		Slope 10-20%	0.0083	_	0.1188	4.6388912	0.02	_	0.16	0.25	0	0.000259811			
Name of the color of the colo		Slope >20%	0.004	7	0.1188	7.3920692	0.02	-	0.16	0.25	0	0.000199522		0.1385	
Stope 0-5%   Control 10-20%   Control		Area 21													
Stope -0.7%   Concept -0.7%		/01/0	77	ï	0	7071		,				10000000			
Stope 5-10%   Course 5		%c-n adole	0.2341	. i	0.3016	0.5457401	0.02	_	00	0.25	>	0.002002997			
Shope 10-20%   Control of the cont		Slope 5-10%	0.0598	7	0.5016	1.6420015	0.02	-	0.16	0.25	0	0.002797568			
Supple Services		Slope 10-20%	0.054	7	0.5016	4.6388912	0.02	-	0.16	0.25	0	0.007136969			
Shope 0-5%   1.188   71   0.1188   0.3457401   0.02   1   0.16   0.25   0   0.002771603   0.00946875   0.1880   7.1   0.1188   1.420015   0.02   1   0.16   0.25   0   0.00184788   0.000946875   0.1883   7.1   0.1188   4.538812   0.02   1   0.16   0.25   0   0.001846875   0.000949698   0.00094998   0.000949698   0.000949998   0.000949998   0.000949999   0.000949999   0.0009499999   0.0009499999999999999999999999999999999		Slope >20%	0.0325	7	0.5016	7.3920692	0.02	-	0.16	0.25	0	0.006844713	1.15899688	0.4004	25.5268
Stope 0-5%   1:188   71   0.1188   0.2457401   0.02   1   0.116   0.25   0   0.002771603   0.02771603   0.02771603   0.02771603   0.02864585   0.02864685   0.02864585   0.0	4	Area 1													
Stope 0-20%   1-186		Aca -	7	ì	0		0	,		L					
Slope 5-10%   O.108   A.108   A.108		Slope 0-5%	1.188	7	0.1188	0.345/401	0.02	_	0.16	0.25	0	0.002//1603			
Slope 10-20%   0.3024   71   0.1168   4.6389812   0.02   1   0.16   0.25   0   0.009468875   0.29446   0.29468   0		Slope 5-10%	0.1683	7	0.1188	1.6420015	0.02	-	0.16	0.25	0	0.001864758			
Slope 5-20%   1.2859   71   0.1188   7.3920692   0.02   1   0.16   0.25   0   0.064141335   2.9446   2.9486		Slope 10-20%	0.3024	71	0.1188	4.6388912	0.02	-	0.16	0.25	0	0.009465875			
Slope 6-5%   2.5951   71   0.5016   0.3457401   0.02   1   0.16   0.25   0   0.00562875     Slope 6-5%   0.0028   71   0.5016   0.3457401   0.02   1   0.16   0.25   0   0.005628261     Slope 6-5%   0.0028   71   0.5016   0.3457401   0.02   1   0.16   0.25   0   0.001149945     Slope 6-5%   0.0028   71   0.5016   7.3320692   0.02   1   0.16   0.25   0   0.001149945     Slope 6-5%   0.0028   71   0.5016   7.3320692   0.02   1   0.16   0.25   0   0.00149945     Slope 6-5%   0.2511   71   0.1188   0.3457401   0.02   1   0.16   0.25   0   0.003059028     Slope 6-5%   0.2511   71   0.1188   0.3457401   0.02   1   0.16   0.25   0   0.003059028     Slope 5-10%   0.2511   71   0.1188   1.4420015   0.02   1   0.16   0.25   0   0.003059028     Slope 6-5%   0.0035   71   0.1188   0.3457401   0.02   1   0.16   0.25   0   0.003059028     Slope 6-5%   0.1147   71   0.5016   0.3457401   0.02   1   0.16   0.25   0   0.003059028     Slope 6-5%   0.0035   71   0.5016   0.4457401   0.02   1   0.16   0.25   0   0.00404477     Slope 6-5%   0.0035   71   0.5016   0.4452015   0.02   1   0.16   0.25   0   0.00404477     Slope 6-5%   0.0035   71   0.5016   0.4452015   0.02   1   0.16   0.25   0   0.00404477     Slope 6-5%   0.0035   71   0.5016   0.4452015   0.02   1   0.16   0.25   0   0.00404477     Slope 7-20%   0.1188   1.4420015   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.1188   1.4420015   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.1188   1.4420015   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.1188   1.4420015   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.1188   1.4420015   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.1188   1.4420015   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.1188   0.3457401   0.02   1   0.16   0.25   0   0.00404477     Slope 5-20%   0.1188   0.3457401   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.1188   0.3457401   0.02   1   0.16   0.25   0   0.00404477     Slope 5-10%   0.0345401   0.02   1		Slopo - 20%	0000	7	0 4 4 0 0	7 2020602	000		9 0	300		0.064141996		20000	
Stope 5-10%   Course of the		Siope >20%	EC02. I	- /	0.1100	7.3920092	0.02	-	0.10	0.23	0	0.004141333		2.3440	
Slope 0-5% 2.5951 71 0.5016 0.3457401 0.02 1 0.016 0.25 0 0.0025662875		Area 2													
Slope 5-10%   0.1266   71   0.5016   1.6420015   0.02   1   0.16   0.25   0   0.005892861   0.00143845   0.0087   71   0.5016   4.538912   0.02   1   0.16   0.25   0   0.00143845   0.00889898   0.00889898   0.00889898   0.00889898   0.00889898   0.008898988   0.00889898   0.00889898   0.00889898   0.00889898   0.0889998   0.0889998   0.088		Slobe 0-5%	2.5951	7	0.5016	0.3457401	0.02	-	0.16	0.25	0	0.025562875			
Signe 10-20%   Concest		Slone 5-10%	0.1266	71	0.5016	1.6420015	0.02	-	0.16	0.25	C	0.00592261			
Slope 520%   1,311   7,1   0,3016   4,538912   0.02   1   0,116   0.25   0   0,000589898   2,7332   2,7332   2,000		Oct 20 000/	0 0 0 0	7	0.00	0.0000	0 0	- •	5 6	9 6		00011110011			
Slope > 20%   0.0028		Siope 10-20%	0.008/	_	0.2016	4.0388912	0.02	-	00	0.20	>	0.00 1 148843			
Altea 3         Altea 4         Altea 3         Altea 3         Altea 4         Altea 4 <t< td=""><th></th><td>Slope &gt;20%</td><td>0.0028</td><td>71</td><td>0.5016</td><td>7.3920692</td><td>0.02</td><td>1</td><td>0.16</td><td>0.25</td><td>0</td><td>0.000589698</td><td></td><td>2.7332</td><td></td></t<>		Slope >20%	0.0028	71	0.5016	7.3920692	0.02	1	0.16	0.25	0	0.000589698		2.7332	
Slope 0-5%         1.3112         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.003059028           Slope 5-10%         0.2511         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.002782179         2.6754           Slope 1-20%         0.4336         71         0.1188         4.6388912         0.02         1         0.16         0.25         0         0.013572762         2.6754           Slope 1-20%         0.6796         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.00338938         0.164776367         2.6754           Slope 0-5%         1.2918         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.00338938         0.164776367         2.6754           Slope 1-20%         0.0114         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         0.004064707         0.16476367         2.6754           Slope 1-20%         0.0138         0.02         1         0.16         0.25         0         0.004064		Area 3													
Slope 5-10%   Control of the contr		Slone 0-5%	1.3112	7	0 1188	0.3457401	000	-	0.16	0.25	c	0.003059028			
Slope 10-20%   0.4336   71   0.1188   4.688812   0.02   1   0.16   0.25   0   0.013572762   0.164776367   2.6754     Slope 5-20%   0.6795   71   0.1188   7.3920892   0.02   1   0.16   0.25   0   0.013572762   0.164776367   2.6754     Slope 5-20%   0.6795   71   0.1188   7.3920892   0.02   1   0.16   0.25   0   0.013724797   0.16476367   0.25   0   0.003105903     Slope 5-10%   0.1144   71   0.5016   4.6388912   0.02   1   0.16   0.25   0   0.003105903   1.446     Slope 10-20%   0.0193   71   0.5016   4.6388912   0.02   1   0.16   0.25   0   0.004064707     Slope 10-20%   0.1188   1.642015   0.02   1   0.16   0.25   0   0.004064707   1.446     Slope 10-20%   0.1188   1.642015   0.02   1   0.16   0.25   0   0.00122436   1.446     Slope 10-20%   0.1188   7.3920892   0.02   1   0.16   0.25   0   0.003105903   1.446     Slope 10-20%   0.1188   7.3920892   0.02   1   0.16   0.25   0   0.003105903   1.446     Slope 5-20%   0.1188   7.3920892   0.02   1   0.16   0.25   0   0.003105903   1.446     Slope 5-20%   0.1188   7.3920892   0.02   1   0.16   0.25   0   0.003105903   1.446     Slope 5-20%   0.0314   71   0.1188   7.3920892   0.02   1   0.16   0.25   0   0.00310591   1.446   1.448   1.4484   1.4444		Close F 408/	1 + 1 10 0			1 640004				) i c	, ,	07000000			
Slope 10-20%   0.4336		%01-c adole	1162.0	- i	0.1100	1.0420013	0.02		00	0.23	<b>&gt;</b> (	0.002/021/9			
Slope >20%   0.6795   71   0.1188   7.3920692   0.02   1   0.16   0.25   0   0.00338938   0.164776367   2.6754		Slope 10-20%	0.4336	7	0.1188	4.6388912	0.02	_	0.16	0.25	0	0.0135/2/62			
Area 4         Stope 0-5%         1.2918         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.012724797           Stope 0-5%         0.1144         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         0.003105903           Stope 5-10%         0.0135         71         0.5016         4.6388912         0.02         1         0.16         0.25         0         0.003105903           Stope 5-10%         0.0193         71         0.5016         4.6388912         0.02         1         0.16         0.25         0         0.004064707           Area 5         Stope 0-5%         2.2292         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.004064707         1.446           Stope 0-5%         0.01105         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.004064707         1.446           Stope 10-20%         1.11824         71         0.1188         7.3920692         1         0.16         0.25         0         0.001224336         1.446           <		Slope >20%	0.6795	7	0.1188	7.3920692	0.02	-	0.16	0.25	0	0.0338938	0.164776367	2.6754	8.3532
Slope 0-5% 1.2918 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.012724797 Slope 5-10% 0.1114 71 0.5016 1.6420015 0.02 1 0.16 0.25 0 0.005211522 Slope 10-20% 0.0235 71 0.5016 4.6388912 0.02 1 0.16 0.25 0 0.003105903 Slope >20% 0.0193 71 0.5016 7.3920692 0.02 1 0.16 0.25 0 0.004064707  Area 5 Slope 5-10% 0.1118 1.6420015 0.02 1 0.16 0.25 0 0.004064707 Slope 5-10% 0.1105 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.001224336 Slope 5-20% 0.0314 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.0257453213  Area 6 Slope 0-5% 0.0314 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.005309304	5	Area 4													
0.0235 71 0.5016 0.2343491 0.02 1 0.16 0.25 0 0.002145737 0.0193 71 0.5016 4.6388912 0.02 1 0.16 0.25 0 0.003105903 0.0193 71 0.5016 7.3920692 0.02 1 0.16 0.25 0 0.003105903 0.0193 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.00220721 0.1105 71 0.1188 4.6388912 0.02 1 0.16 0.25 0 0.001224336 0.1184 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.03712071 0.1167 71 0.1188 0.3457401 0.02 1 0.16 0.25 0 0.03712071	,	Clono O Eo/	1 2010	7	0 5016	0.2457404	600	•	97	30.0	c	707707010			
0.0235 71 0.5016 1.6420015 0.02 1 0.16 0.25 0 0.003105903 0.0235 77 0.5016 4.6388912 0.02 1 0.16 0.25 0 0.003105903 0.0193 71 0.5016 4.6388912 0.02 1 0.16 0.25 0 0.004064707 0.0198 7.3920692 0.02 1 0.16 0.25 0 0.004064707 0.1188 0.3457401 0.02 1 0.16 0.25 0 0.005200721 0.1188 4.6388912 0.02 1 0.16 0.25 0 0.037012071 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.037012071 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.037012071 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.0037013071 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.0037013071		Signature 0.5%	0165.1	- i	0.301.0	1047040.0	20.0	- ,	00	0.60	> 0	0.012/2/200			
0.0235         71         0.5016         4.6388912         0.02         1         0.16         0.25         0         0.003105903           0.0193         71         0.5016         7.3920692         0.02         1         0.16         0.25         0         0.004064707           2.2292         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.005200721           0.1162         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.001224336           1.1824         71         0.1188         4.6388912         0.02         1         0.16         0.25         0         0.037012071           5.1614         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.257453213           0.0314         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.0039394		%01-c adols	0.1114	-	0.5016	1.6420015	0.02	-	0.16	0.25	>	726112600.0			
0.0193         71         0.5016         7.3920692         0.02         1         0.16         0.25         0         0.004064707           2.2292         71         0.1188         1.642015         0.02         1         0.16         0.25         0         0.005200721           0.1105         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.001224336           5.1614         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.03712071           5.1614         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.257453213           0.031         7         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.027453213		Slope 10-20%	0.0235	7	0.5016	4.6388912	0.02	-	0.16	0.25	0	0.003105903			
2.2292         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.005200721           0.1105         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.001224336           1.1824         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.037453213           5.1614         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.257453213           0.0314         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.000309304		Slope >20%	0.0193	7	0.5016	7.3920692	0.02	-	0.16	0.25	0	0.004064707		1.446	
2.2292         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.005200721           0.1105         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.001224336           1.1824         71         0.1188         4.6388912         0.02         1         0.16         0.25         0         0.037012071           5.1614         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.257453213           0.0314         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.00309304		Area 5													
0.1105 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.001224336 1.1824 71 0.1188 4.6388912 0.02 1 0.16 0.25 0 0.037012071 0.188 7.3920692 0.02 1 0.16 0.25 0 0.257453213 0.0314 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.00309304		Slope 0-5%	22292	7	0.1188	0.3457401	0.02	-	0.16	0.25	C	0.005200721			
0.0314 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.003093904 0.02 0 0.003093904 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.		Slone 5-10%	0 1105	7	0 1188	1 6420015	000		16	0.05		0.001224336			
5.1614 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.00309304 0.00 0.00309304		Close 10 008/	7007			4 6000040				) i c	, ,	0000100000			
0.0314 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.00309304		Siope 10-20%	1.1024	- i	0.1100	4.6300912	0.02	- ,	0.10	0.23	<b>&gt;</b> (	0.03/0120/1		1000	
0.0314 71 0.5016 0.3457401 0.02 1 0.16 0.25 0		olope ><070	5.1014	-	0.1100	7.3920092	0.02	-	0.10	0.25	0	0.257453215		0.000.0	
0.0314 71 0.5016 0.3457401 0.02 1 0.16 0.25 0		Area 6		i						1					
		Slope 0-5%	0.0314	7	0.5016	0.3457401	0.02	-	0.16	0.25	0	0.000309304			

		0.3281					0.4885				1	1.1723				11 7819	200				1.8165					0.7798				0 7450	0.7439				1.4323				0.1188				1 2242	1.2242				1.1161				14 1519	- -		
0,000,000	0.02159594	0.021355505		0.001205694	0.0008888859	0.008551146	0.059475291		0.003827881	0.000987102	0.024344994	0.121814832	0.006457974	4/6/640000	0.000000347	0.07.923.11064	1020110002.0	0.01165504	0.017908176	0,024688626	0.013415638		0.000710398	0.001578895	0.006617348	0.006055493		0.004663198	0.004650138	0.012754028	0.016132462	0.001515049	0.001512415	0.014255157	0.009527175	70000	0.000213723	0.002286473	0.001326821		0.00795817	0.005239592	0.02237572	0.020431003	0.00155471	0.001694126	0.006880289	0.003840798		0.025902119	0.014064906	0.036398542	0.000.0	0.054084822	0.021697523
c	0 0	0		0	0	0	0	•	<b>&gt;</b> (	0	0 (	Э	c	> <	<b>&gt;</b>	o c		c	o c	0	0		0	0	0	0		0	0	0 0	0	C	0	0	0	c	0 0	0	0		0	0 (	<b>o</b> c	>	0	0	0	0		0	0 (	0 0	5	0	0
1000	0.25	0.25		0.25	0.25	0.25	0.25	i d	0.20	0.25	0.25	0.25	30.0	2.0	0.20	0.50	0.50	0.05	0.25	0.25	0.25		0.25	0.25	0.25	0.25		0.25	0.25	0.25	0.25	0.25	0.25	0.25	0.25	0	0.25	0.25	0.25		0.25	0.25	0.25	0.63	0.25	0.25	0.25	0.25		0.25	0.25	0.25	01:0	0.25	0.25
	0.16	0.16		0.16	0.16	0.16	0.16		0.10	0.16	0.16	0.16	16	0.0	0.16	0.10	0	0.16	0.16	0.16	0.16		0.16	0.16	0.16	0.16		0.16	0.16	0.16	0.10	0.16	0.16	0.16	0.16	0	0.16	0.16	0.16		0.16	0.16	0.16	00	0.16	0.16	0.16	0.16		0.16	0.16	0.16	5	0.16	0.16
,		- 1		-	-	-	1			-		-		- ,			-	-		-	-		-	-	-	-		-	-		-	-		-	-	,		-	-		-			-	-	-	-	-		<del>.</del> .	<b>-</b> .		-	-	-
	0.02	0.02		0.02	0.02	0.02	0.02	0	0.02	0.02	0.02	0.02	000	20.0	20.0	20.0	20.0	000	0.02	0.02	0.02		0.02	0.02	0.02	0.02		0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0	0.02	0.02	0.02		0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02		0.02	0.02	0.02	10.0	0.02	0.02
4 0 40004	4.6388912	7.3920692		0.3457401	1.6420015	4.6388912	7.3920692		0.345/401	1.6420015	4.6388912	7.3920692	0.9457404	1043040	1.6420013	7.3920692	1.0320032	0 3457401	1 6420015	4.6388912	7.3920692		0.3457401	1.6420015	4.6388912	7.3920692		0.3457401	1.6420015	4.6388912	7.3920092	0.3457401	1.6420015	4.6388912	7.3920692	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 6420015	4.6388912	7.3920692		0.3457401	1.6420015	4.6388912	7.3920092	0.3457401	1.6420015	4.6388912	7.3920692		0.3457401	1.6420015	4.6388912	1.0040001	0.3457401	1.6420015
0 10 10	0.5016	0.5016		0.5016	0.5016	0.5016	0.5016	i d	0.5016	0.5016	0.5016	0.5016	0 1100	0.1100	0.1100	0.1100	0	0.5016	0.5016	0.5016	0.5016		0.1188	0.1188	0.1188	0.1188		0.5016	0.5016	0.5016	0.3016	0.1188	0.1188	0.1188	0.1188	0	0.5016	0.5016	0.5016		0.5016	0.5016	0.5016	0.3010	0.1188	0.1188	0.1188	0.1188		0.1188	0.1188	0.1188		0.5016	0.5016
1.		71		7	7	7	71	i	- i	7	F i	1/	7	7 7	7 7	7 7		7		7	7		7	7	77	7		7	F 1	F 7	-	7.7	: .	71	71	7		7			7	F i	< 7	-	7	7	7	71		F 1	Γi	F F	1	71	71
0,000	0.0319	0.1014		0.1224	0.019	0.0647	0.2824		0.3880	0.0211	0.1842	0.5784	2 7681	2007.7	0.0022	5.5318	0.00	1 1832	0.3828	0.1868	0.0637		0.3045	0.1425	0.2114	0.1214		0.4734	0.0994	0.0965	0.0700	0.6494	0.1365	0.4554	0.191	0	0.0219	0.0173	0.0063		0.8079	0.112	0.1693	0.133	0.6664	0.1529	0.2198	0.077		11.1025	1.2694	1.1628	1.0.0	5.4906	0.4638
00/1	Slope 10-20%	Slope >20%	Area 7	Slope 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Area 8	Siope 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Slope 0-5%	Slope 0-3 /8	Slope 3-10%	Slope 20%	010pe 720 70	Slope 0-5%	Slone 5-10%	Slope 10-20%	Slope >20%	Area 11	Slope 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Area 12	Slope 0-5%	Slope 5-10%	Slope 10-20%	Siope >20%	Slone 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Area 14	Slope 5-10%	Slope 10-20%	Slope >20%	Area 15	Slope 0-5%	Slope 5-10%	Slope 10-20%	Area 16	Slope 0-5%	Slope 5-10%	Slope 10-20%	Slope >20%	Area 17	Slope 0-5%	Slope 5-10%	Slope 10-20%	Area 18	Slope 0-5%	Slope 5-10%

Slope 10-20%	0.4787	71	0.5016	4.6388912	0.02	-	0.16	0.25	0	0.063267909			
Slope >20%	0.5298	71	0.5016	7.3920692	0.02	1	0.16	0.25	0	0.111579353		6.9629	
Area 19													
Slope 0-5%	6.3419	71	0.5016	0.3457401	0.02	-	0.16	0.25	0	0.062470501			
Slope 5-10%	0.3299	71	0.5016	1.6420015	0.02	-	0.16	0.25	0	0.015433404			
 Slope 10-20%	0.2865	71	0.5016	4.6388912	0.02	-	0.16	0.25	0	0.037865586			
Slope >20%	0.0648	71	0.5016	7.3920692	0.02	-	0.16	0.25	0	0.013647305		7.0231	
Area 20													
Slope 0-5%	0.6919	71	0.1188	0.3457401	0.02	-	0.16	0.25	0	0.001614202			
Slope 5-10%	0.235	71	0.1188	1.6420015	0.02	-	0.16	0.25	0	0.002603791			
Slope 10-20%	0.0904	71	0.1188	4.6388912	0.02	-	0.16	0.25	0	0.002829746			
Slope >20%	0.0234	71	0.1188	7.3920692	0.02	-	0.16	0.25	0	0.001167204		1.0407	
Area 21													
Slope 0-5%	1.6663	71	0.5016	0.3457401	0.02	-	0.16	0.25	0	0.016413787			
Slope 5-10%	0.5562	71	0.5016	1.6420015	0.02	-	0.16	0.25	0	0.026020186			
Slope 10-20%	0.6075	71	0.5016	4.6388912	0.02	-	0.16	0.25	0	0.080290902			
Slope >20%	0.3773	71	0.5016	7.3920692	0.02	-	0.16	0.25	0	0.079461853	1.900227962	3.2073	63.5198

TOTAL 4.20693 tonnes

138.7981 Total Area (ha)

K Factor	VeD	ŧ	Sand		Nomograph	Correction Earthor	Ashie	Metric Convert
nple 1	Clay	311t	34IIU 71	13	Value	Peat (4% Organic)	Aaine	K Factor
Sample 2		15	99	19		Sand/Gravels (0% Organic)		
Average	7	15.5	68.5	16	0.52	-0.14	0.38	0.5016
Sand Soils								
nple 1		1	9	93				
nple 2		2	∞	06				
Average		1.5	7	91.5	0.15	-0.06	0.00	0.1188
Gravels		10	20	70	0.2	-0.1	0.1	0.132

Assumes a full grass cover over alignment in existing state

Sitename: M2PP Paraparaumu Coordinate system: NZMG Northing: 6030188 Easting: 2679016

Sitename: M2PP PekaPeka Coordinate system: NZMG

Northing: 6038488 Easting: 2685968

Rainfall depths (mm)

Rainfall depths (mm)

ARI (y) 1.58 72h 99.4 105.6 127 143.6 161.5 172.7 181.2 187.9 193.7 203 48h 90.9 96.5 116.1 131.2 147.6 157.9 165.6 171.8 173 173 175 185.6 78 82.8 99.6 112.6 135.4 142 147.4 151.8 159.2 **12h** 56.3 60 73.1 83.2 94.3 101.3 110.9 114.5 120.4 40.6 53.6 61.5 70.3 75.8 80.3 91 91 24.2 24.2 26.1 32.8 38.1 44.1 47.9 50.8 53.2 55.2 58.5 61.2 60m 17.5 18.9 28.2 28.2 32.8 35.8 35.8 35.8 40 41.6 44.2 46.4 30m 12.2 13.2 16.8 19.7 23 25.1 26.7 28 29.1 30.9 32.4 20m 9.9 10.7 13.7 16 18.6 20.4 21.6 22.7 23.6 25.1 26.3 7.5 9.6 9.6 11.2 13.1 14.2 15.1 15.9 16.5 17.6 18.4 0.5 0.1 0.05 0.03 0.025 0.025 0.017 0.012 ARI (y) 1.58 2 5 10 20 20 30 40 40 50 60 80

72h 98 104.1 125.4 141.9 159.8 159.8 171 179.4 186.2 201.3 208.9

88 93.5 112.6 127.4 143.4 153.5 161.1 167.2 172.3 180.7

24h
73.2
77.7
93.7
106
119.3
127.7
134
139
143.3
150.3

12h 54 57.6 70.1 79.8 90.4 97.1 102.1 106.2 109.6 115.2

39.9 52.4 60.1 60.1 68.4 77.8 77.8 81.1 83.8 83.8

24.7 24.7 26.5 33.1 38.3 44.1 47.8 50.6 52.8 54.8 54.8 56.5

60m 18.3 19.7 24.8 28.8 33.4 36.3 36.3 40.3 41.9 44.4

13 14.1 17.7 20.6 23.9 26 27.6 27.6 28.8 29.9 31.8

20m 10.7 11.6 14.5 16.9 19.6 21.3 22.6 23.7 24.6 27.3

10a 7.7 8.3 10.4 12.1 14 15.3 16.2 16.9 17.6 18.7

aep 0.633 0.5 0.2 0.1 0.05 0.025 0.025 0.017 0.017

2 10 10 20 20 30 40 40 50 60 80

Extreme rainfall assessment with climate change

Projected temperature change: 2.0 ° C

72h 106.4 113.2 139.2 160.5 184.1 199.3 209.6 218 224.7 235.5 244.3 48h 97.8 103.8 127.7 147.2 168.6 182.5 191.8 199.3 205.3 223.3 24h 84.7 89.9 110.4 126.8 144.8 157.1 171 171 176.1 184.7 **12h** 61.7 65.8 81.6 108.1 117.5 123.7 128.6 132.8 139.7 44.9 60.1 69.9 80.7 87.9 92.8 96.7 100.1 27.2 27.2 29.3 37.2 43.6 50.8 55.6 58.9 61.7 64 60m 19.8 21.4 27.4 32.4 37.9 41.5 44.2 46.4 66.4 68.3 51.3 14 15.1 19.3 22.7 26.6 29.1 31 32.5 33.8 35.8 20m 11.4 12.3 15.8 18.5 21.6 23.7 25.1 26.3 27.4 29.1 30.5 8.1 8.7 11.1 13 15.1 16.5 17.5 18.4 19.1 20.4 21.3 aep
0.633
0.5
0.5
0.1
0.05
0.05
0.033
0.025
0.025
0.017
0.012

5 10 20 30 40 50 60 80

ARI (y) 1.58

Extreme rainfall assessment with climate change

Projected temperature change: 2.0  $^{\circ}$  C

72h 104.9 111.4 137.4 158.6 182.2 197.3 207.6 216 222.7 233.5 242.3 48h 94.7 100.6 1123.9 142.9 163.8 177.4 186.6 194 199.9 209.6 217.5 24h
79.5
84.4
103.8
119.4
136.5
148.1
155.4
161.2
166.2
174.3 12h 59.2 63.1 78.2 90.2 103.6 112.6 118.4 123.2 127.1 133.6 58.8 68.3 78.5 85.6 90.2 94.1 97.2 27.8 27.8 29.8 37.5 43.8 50.8 55.4 58.7 61.2 63.6 67.3 60m 20.8 22.3 28.3 33.1 38.5 42.1 44.7 46.7 46.7 48.6 53.9 30m 14.9 16.1 20.3 23.7 27.6 30.2 32.3 33.4 34.7 36.9 38.5 20m 12.3 13.4 16.7 19.5 22.7 24.7 26.2 27.5 27.5 28.5 30.3 31.7 8.9 9.6 12.1 14 16.2 17.7 18.8 19.6 20.4 21.7 22.6 aep 0.633 0.5 0.2 0.1 0.05 0.025 0.025 0.017 5 10 20 30 40 40 50 60 80

Rainfall Erosion Index (J/ha) - Based on NIWA HIRDS Data

R = 0.00828p2.2\*1.7

48.1 p = 6 hour duration 2 year storm

R Factor

0.2 for slopes < 1%	0.3 for slopes 1 to 3%	0.4 for slopes 3.5 to 4.5%	0.5 for slopes > 5%
ш			

Slope (Av/Mid Slope)	Area	S2	S2+10000		L (m)	Weight L	m	rs
Area 1								
2.5	9.9	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	1.44	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	75.0	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	98'0	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 2								
2.5	0.5122	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0592	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	9650.0	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1002	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 1								
2.5	4.426	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	689'0	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	1.5453	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	2.7361	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 2								
2.5	8985.0	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.2276	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.4838	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	1.8145	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 3								
2.5	2.8566	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0312	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1189	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1554	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 4								
2.5	1026.0	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0062	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0343	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.2649	400	10400	101.9803903	100	30.48	0.5	7.392069161

2 20 2								
2.5	0.0402	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	9900'0	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0646	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.2026	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 6								
2.5	0.1491	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.323	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1127	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1493	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 7								
2.5	0.2967	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0719	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.2426	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.3879	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 8								
2.5	1.119	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.3714	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.5687	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.4171	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 9								
2.5	0.6771	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1415	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.3093	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.465	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 10								
2.5	0.7131	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0585	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1527	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1629	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 11								
2.5	0.5134	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0728	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.2617	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1499	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 12								
2.5	0.8128	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.346	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.3469	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	1.0737	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 13								
L		100	100001	7170700 007	001	0, 00	0 0	

7.5	0.1825	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0805	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.0959	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 14								
2.5	0.2864	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0959	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.3364	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	2.6097	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 15								
2.5	0.3664	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.012	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.0756	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 1								
2.5	1.6884	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.3154	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.5939	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	1.1114	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 2								
2.5	0.2064	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	9090'0	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1931	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.4624	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 3								
2.5	0.1254	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.03	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1213	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.3563	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 4								
2.5	0.0226	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0194	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1082	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 5								
2.5	0.3833	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1459	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.188	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.2384	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 6								
2.5	0.1175	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0185	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
U T	60	225	10225	101.1187421	100	30.48	0.5	1 638801 <i>001</i>

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Area 7								
2.5	0.1358	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0038	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0372	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.145	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 8								
2.5	1.5033	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.3173	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.5455	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.598	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 9								
2.5	0.0392	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0001	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	8960'0	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.2599	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 10								
2.5	0.7927	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0943	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.2878	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.3984	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 11			10000	100	100	30.48	0.5	
2.5	0.1365	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	6900'0	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.062	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1036	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 12								
2.5	0.3648	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1759	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.517	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.8386	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 13								
2.5	0.0408	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0348	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1562	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1701	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 14								
2.5	0.8678	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1449	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1855	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.4904	400	10400	101.9803903	100	30.48	0.5	7.392069161

2.5	0.9862	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0835	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.3967	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	2.3455	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 16								
2.5	0.5971	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1606	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1583	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.0991	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 17								
2.5	0.6855	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0629	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1984	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.3729	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 18								
2.5	0.4202	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.2141	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.182	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.053	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 19								
2.5	0.9161	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0531	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1488	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1062	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 20								
2.5	0.1055	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0207	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0083	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.004	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 21								
2.5	0.2541	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0598	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.054	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.0325	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 1								
2.5	1.188	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1683	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.3024	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	1.2859	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 2								
2.5	2.5951	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
1	00000	20 32	10056.25	100 2808556	100	01 00	П	4 0.40004 500

	/0000	277	10225	101.1187421	001	30.48	0.5	4.638891224
20	0.0028	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 3								
2.5	1.3112	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.2511	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.4336	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.6795	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 4								
2.5	1.2918	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1114	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0235	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.0193	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 5								
2.5	2.2292	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1105	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	1.1824	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	5.1614	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 6								
2.5	0.0314	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0319	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1634	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1014	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 7								
2.5	0.1224	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.019	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0647	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.2824	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 8								
2.5	0.3886	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0211	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1842	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.5784	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 9								
2.5	2.7681	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.8022	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	2.5318	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	2.6798	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 10								
2.5	1.1832	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.3828	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1868	225	10225	101.1187421	100	30.48	0.5	4.638891224
	10000	700	10400	101 000000	700	07 00	L	7000000

2.5	0.3045	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1425	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.2114	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1214	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 12								
2.5	0.4734	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0994	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0965	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.0766	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 13								
2.5	0.6494	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1365	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.4554	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.191	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 14								
2.5	0.0219	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0733	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0173	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.0063	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 15								
2.5	0.8079	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.112	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1693	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.135	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 16								
2.5	0.6664	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.1529	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.2198	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.077	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 17								
2.5	11.1025	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	1.2694	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	1.1628	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.6172	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 18								
2.5	5.4906	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.4638	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.4787	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.5298	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 19								
L	0.770	L	LO 0000	1 L 1 C 1 C C C C T				

0.3299	56.25 10056.25	100.2808556	100	30.48	0.5	1.642001523
225	10225	101.1187421	100	30.48	0.5	4.638891224
400	10400	101.9803903	100	30.48	0.5	7.392069161
6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
225	10225	101.1187421	100	30.48	0.5	4.638891224
400	10400	101.9803903	100	30.48	0.5	7.392069161
6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
225	10225	101.1187421	100	30.48	0.5	4.638891224
400	10400	101.9803903	100	30.48	0.5	7.392069161

## **USLE Calculation M2PP During Earthworks - Project Footprint**

1600 1380 14200 120 1690 **Total Catchment Area (ha)** Whareroa Wharemauku Waikanae Waimeha Ngarara Catchment 1 Catchment 2 Catchment 3 Catchment 4

Assumptions

R factor based on NIWA HIRDS data

K Factor based on soil samples and soils /gravels to be utilised

LS Factor based on different slopes with a uniform 100m slope length - this is the worst case scenarion with the installation of contour drains reducing this value

C and P Factors based on a bare site which has a rough and irregular surface

Duration - for purposes of risk assessment has been based on 2 months total for each stage however staging and progressive stabilisation will occur. Sediment Delilivery Ratio - based on a high infilitration rate and irregular surface capturing flow and sediment - 0.25 assumed figure Efficiency - based on 95% due to control measures exceeding guidelines and chemical treatment - all measures considered of equal efficiency

Area 1 Slope 0-5% 6.66 71 Slope 5-10% 1.44 71 Slope 5-20% 0.54 71 Slope 5-20% 0.54 71 Area 2 Slope 0-5% 0.5122 71 Slope 5-10% 0.0592 71 Slope 5-10% 0.0596 77 Slope 10-20% 1.5456 77	0.396 0.396 0.396 0.396 0.5016 0.5016	0.3457401	,	р	time	sdr	sed eff.	Yield	Overall Footprint Yield Area		Project Footprint Area	Pro Rata Total Catchment Area	Slope % Total Catchment	Less Project Footprint	Catchment Area
0.5122 71 0.0592 71 0.0592 71 0.0096 71 0.1002 71 1.543 71		2	-	6:0	0.16	0.25	0.95	0.116533288				1095.034528	0.74	1088.374528	
0.54 71 0.36 71 0.5122 71 0.0592 71 0.0596 71 0.1002 71 4.426 71 0.689 71 1.5453 71		1.6420015	-	6.0	0.16	0.25	0.95	0.119663606				236.7642223	0.16	235.3242223	
0.55 71 0.5122 71 0.0592 71 0.0596 71 0.1002 71 4.426 71 0.689 71 1.5453 71		4.6388912	-	6.0	0.16	0.25	0.95	0.126775108				88.78658336	90.0	88.24658336	
0.5122 71 0.0592 71 0.0596 71 0.1002 71 4.426 71 0.689 71 1.5453 71		7.3920692	1	6.0	0.16	0.25	0.95	0.13467735		6		59.19105557	0.04	58.83105557	1479.776389
0.5122 71 0.0592 71 0.0596 71 0.1002 71 4.426 71 1.5453 71															
0.0592 71 0.0096 71 0.1002 71 4.426 71 0.689 71 1.5453 71		0.3457401	-	6.0	0.16	0.25	0.95	0.011352139				84.21571851	0.700492341	83.70351851	
0.0596 0.1002 4.426 0.689 1.5453		1.6420015	-	6.0	0.16	0.25	0.95	0.006231372				9.73364025	0.080962801	9.67444025	
0.1002 4.426 0.689 1.5453		4.6388912	-	6.0	0.16	0.25	0.95	0.017723473				9.799408089	0.081509847	9.739808089	
4.426 0.689 1.5453	0.5016	7.3920692	1	0.9	0.16	0.25	0.95	0.047481248	0.580437584	0.7312	9.7312	16.4748438	0.137035011	16.3746438	120.2236107
4.426 0.689 1.5453															
0.689	0.396	0.3457401	-	6.0	0.16	0.25	0.95	0.077443894				192.9147369	0.471121708	188.4887369	
1.5453	0.396	1.6420015	-	6.0	0.16	0.25	0.95	0.057255712				30.03123673	0.073340004	29.34223673	
2 7361	0.396	4.6388912	-	6.0	0.16	0.25	0.95	0.3627881				67.35452847	0.16448811	65.80922847	
1007.3	0.396	7.3920692	-	6.0	0.16	0.25	0.95	1.02358527		9.3964		119.2575716	0.291241777	116.5214716	409.4796176
Area 2															
Slope 0-5% 0.5863 71	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.007181145				25.54998721	0.188387636	24.96368721	
Slope 5-10% 0.2276 71	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.013239448				9.918432695	0.073131547	9.690832695	
0.4838 71	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.079506774				21.08320623	0.155452734	20.59940623	
	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.475167878		3.1122		79.07291795	0.583028083	77.25841795	135.6245441
Area 3															
	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.034988332				124.4859176	0.90338699	121.6293176	
0.0312 71		1.6420015	-	6.0	0.16	0.25	0.95	0.001814898				1.359644552	0.009866861	1.328444552	
6 0.1189 71	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.0195398				5.181465938	0.037601594	5.062565938	
Slope >20% 0.1554 71	0.2772	7.3920692	-	0.9	0.16	0.25	0.95	0.040695006		3.1621		6.772075751	0.049144556	6.616675751	137.7991038
Area 4															
	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.004533075				16.12834772	0.547890452	15.75824772	
Slope 5-10% 0.0062 71	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.000360653				0.270185776	0.009178386	0.263985776	
Slope 10-20% 0.0343 71	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.005636797				1.49473744	0.050777202	1.46043744	
Slope >20% 0.2649 71	0.2772	7.3920692	-	0.9	0.16	0.25	0.95	0.069370058		0.6755		11.54390519	0.39215396	11.27900519	29.43717612
71	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.000492379				1.751849712	0.128025478	1.711649712	
0.0066 71		1.6420015	-	6.0	0.16	0.25	0.95	0.000383921				0.287617117	0.021019108	0.281017117	
7	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.010616241				2.815161477	0.205732484	2.750561477	
Slope >20% 0.2026 71	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.053055394		0.314		8.828973919	0.64522293	8.626373919	13.68360222
0.1491 71		0.3457401	-	6.0	0.16	0.25	0.95	0.001826213				6.497532139	0.203105844	6.348432139	
Slope 5-10% 0.323 71	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.018788848				14.07580738	0.439994551	13.75280738	
0.1127 71	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.018520904				4.911280161	0.153521319	4.798580161	

ō					0				0011000		Č	00017000	000010000	0001700100	07100000
Slope >20%	0.1493	71/2/0 1/2	7.72 7.3920692	1032	0.9	0.16	0.25	0.95	0.039097583	0.7341	0.0	6.506247809	0.203378288	6.35694/809 31.99086/49	1.99066749
Slone 0-5%	0.2967	27720 17	772 0.3457401	1 1	60			5 0 95	0 003634054		12.5	92969675	0.296967271	12,63299675	
Slope 5-10%	0.0719			1015	6.0				0.004182409		. m	33283439	0.071964768	3.061383439	
Slope 10-20%	0.2426	71 0.2772	772 4.6388912	1912 1	0.0	0.16	6 0.25		0.039868424		10.	10.57210796	0.242818537	10.32950796	
Slope >20%	0.3879			1692	0.9			5 0.95	0.101580391	0.9991	16.9	16.90404237	0.388249424	16.51614237	43.53913052
Area 8															
Slope 0-5%	1.119			7401 1	0.0	0.16			0.013705784		48.	48.76417481	0.451902108	47.64517481	
Slope 5-10%	0.3714			1 100	0.0		6 0.25	5 0.95	0.021604267		16.	16.18499957	0.14998/885	15.81359957	
Slope >20%	0.5687	71.20 17	772 7.3920692	1 218	6.0				0.093459079	2,4762	. 47	24.78300823 18.17653022	0.168443583		107.9087128
Area 9				-		5						110000			
Slope 0-5%	0.6771		772 0.3457401	1 104	6.0				0.008293286		29.	29.50690148	0.425073765	28.82980148	
Slope 5-10%	0.1415			1 100	6.0				0.008231028		6.10	6.166336671	0.088831691	6.024836671	
Slope 10-20%	0.3093	71 0.2772		3912 1	0.0	0.16	6 0.25	5 0.95	0.050829775	0004	13.	13.47878397	0.194174148	13.16948397	SO 41EOFESE
Slope >20%	0.465		7.3920692	1 2690	0.9				1//0//1	828C.1	20.3	26393323	0.291920397		69.41595536
Slope 0-5%	0.7131	71 0.9779	772 0 3457401	401	0		0.05	70 05	0.008734222		31.0	31 07572212	0 655905077	30.36969219	
Slope 5-10%	0.0585	71 0.2772		1015 1	6.0	0.16			0.003402934		2.5	2.549333535	0.053807947	2.490833535	
Slope 10-20%	0.1527			1912 1	0.0				0.025094428		9.9	6.654414203	0.140452539	6.501714203	
Slope >20%	0.1629			1 1 1	0.9		6 0.25		0.042659051	1.0872	7.09	.098913383	0.149834437		47.37838324
Area 11											•				
Slope 0-5%	0.5134			7401	0.0				0.011378735		22.	22.37312542	0.51453197	21.85972542	
Slope 5-10%	0.0728	71 0.5016	)16   1.6420015	1015	D. C		6 U.25	0.95 7	0.0078227		1.5	3.172503955	0.072960513	3.0997.03955	
Slope >20%	0.1499			1692 1	6.0	0.16			0.071032326	0.9978	19	6.53239482	0.150230507		43.48247866
Area 12															
Slope 0-5%	0.8128			1 104	6.0				0.009955372		35.	35.42048372	0.315112042	34.60768372	
Slope 5-10%	0.346			1 1	0.0				0.020126754		15.0	15.07810946	0.134139722	14.73210946	
Slope 10-20%	0.3469	71 0.2772		3912 1	6.0	0.16	6 0.25 6 0.25	5 0.95	0.057008888	V 5797	15.	15.11732997	0.134488641	14.77042997	110 4050027
Slope >20%	1.0737		7.3920092	7697	0.9				0.2811/203/	2.3/34	40	0.7900733	0.410233333		12.4039907
Slope 0-5%	0.3989	71 0.5016	0.3457401	1 1 1	0.9	0.16	6 0.25	5 0.95	0.008841015		17.3	17.38340423	0.526392188	16.98450423	
Slope 5-10%	0.1825			1 1015	0.0				0.019209887		7.9	7.953049064	0.240828715	7.770549064	
Slope 10-20%	0.0805	71 0.5016		1 1	6.0		6 0.25	5 0.95	0.023938584		3.5(	3.508057258	0.106228556	3.427557258	
Slope >20%	0.0959	71 0.5016	7.3920692	1 1	6.0	0.16	6 0.25	5 0.95	0.045443629	0.7578	4.1	4.179163864	0.126550541	4.083263864	33.02367441
Area 14	7000		770		C				1001010		Č	4000004	0.00004705	40440074	
Slope 6-10%	0.2864			1 1 1 1 1 1 1 1 1 1	9.0			CS 0.95	0.003507897		12.4	12.48083974	0.08604/35	12.19443974	
Slope 10-20%	0.3364	71 0.2772		1 1 1	6.0	0.16	6 0.25		0.055283338		14.0	14.65975729	0.101069583	14.32335729	
Slope >20%	2.6097			1 1	0.0				0.683408989	3.3284	113	113.7264227	0.784070424		145.0461836
Area 15															
Slope 0-5%	0.3664	71 0.5016	0.345/401	401 1	0.0 0.0			.5 0.95 .5 0.95	0.008120702		15.3	15.96710782	0.807048458	15.600/0/82	
Slope 10-20%	0.012			912 1	6.0	0.16	0.25		0.003568485		0.5	22940212	0.026431718	0.510940212	
Slope >20%	0.0756			1 1	0.9				0.035824175	<b>4.5010508</b> 0.454	31.6671 3.29	3.294523338	0.166519824		19.78457137
Area 1	,			,								7110070	1017001170		
Slope 0-5% Slope 5-10%	0.3154	71 0.5016	0.345/401	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6.0	0.16		5 0.95	0.037420834		938	939.2199571 175.4501152	0.085034105	175.1347152	
Slope 10-20%	0.5939			3912 1	6.0				0.176610246		330	330.3735682	0.160119706		
Slope >20%	1.1114		7.3920692	1 1	0.0	0.1	6 0.25	5 0.95	0.526653283	3.7091	618	618.2474889	0.299641422	617.1360889	2063.291129
Area 2 Slope 0-5%	0.2064	27720	779 0 3457401	101	0	0.16	200	ה ה ה	0.000508037		117	114 8158014	0.993739837	114 6094014	
Slope 5-10%	0.0606	71 0.2772		1015	0.0				0.00352509		33.	33.71045333	0.065691057	33.64985333	
Slope 10-20%	0.1931			3912 1	6.0	0.16			0.031733688		107	107.4173026	0.209322493		
Slope >20%	0.4624	71 0.2772	772 7.3920692	1 1	6.0		6 0.25	5 0.95	0.121089902	0.9225	25	257.222997	0.501246612	256.760597	513.1665544
Area 3 Slope 0-5%	0 1254	71 0 9772	772 0.3457401	1 101	o c		6 0 25	5 0 95	0.00153593		69	69 75727471	0 198104265	69 63187471	
Slope 5-10%	0.03			1015 1	0.0				0.001745094		16.0	68834323	0.047393365	16.65834323	
Slope 10-20%	0.1213	71 0.2772	4	3912 1	0.9	0.16			0.019934212		67.4	67.47653447	0.191627172		
Slope >20%	0.3563	71 0.2772	772 7.3920692	1 2692	0.0		6 0.25	5 0.95	0.093305216	0.633	26L	98.2018898	0.562875197	197.8455898	352.1240422
Slope 0-5%	0.0226	71 0.2772	772 0.3457401	1 101	0.9			5 0.95	0.00027681		12.1	12.57188523	0.150466045	12.54928523	
Slope 5-10%	0			1 100	6.0	0.16			0			0	0	0	
Slope 10-20%	0.0194	71 0.2772	772 4.6388912	3912 1	0.0		6 0.25	5 0.95	0.003188159	0.1500	10.7	10.79179529	0.129161119	10.77239529	82 55207178
Area 5	100			100		5						2100			
Slope 0-5%	0.3833			7401 1	0.0				0.004694752		213	213.2213987	0.401109251	212.8380987	
Slope 5-10%	0.1459	71 0.2772	772 4.6388912	1 1 1 1 1 1 1	6.0 6.0	0.16	6 0.25 6 0.25	.5 0.95 .5 0.95	0.008486975		104	81.1609/592	0.1526/8945	81.01507592	
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Area 6	0.6304		0.5772	7.3320036	-	6.0	0.0	0.53	0.93	10.0024-20.0	0.000.0	102.0107003	0.1014642.0	132.37 00000	16006 10.10
Slone 0-5%	0 1175	7	0.2772	0.3457401		60	0.16	0.25	0.95	0.001439169		65.36267766	0 142182962	65 24517766	
Slope 5-10%	0.0185	7.	0.2772	1.6420015		6.0	0.16	0.25	0.95	0.001076141		10.29114499	0.022386254	10.27264499	
Slope 10-20%	0.2	F 7	0.2772	4.6388912	- ,	6.0	0.16	0.25	0.95	0.032867621		111.2556215	0.242013553		0
Slope >20%	0.4904	5	0.2772	7.3920692		6.0	0.16	0.25	0.95	0.128422335	0.8264	2/2./98/84	0.593417231	2/2.308384 45	459.7082282
Slope 0-5%	0.1358	7	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.001663311		75.54256703	0.422001243	75.40676703	
Slope 5-10% Slope 10-20%	0.0038	<u> </u>	0.2772	1.6420015		6.0	0.16	0.25	0.95	0.000221045		2.113856809	0.011808577	2.110056809	
Slope >20%	0.145	71	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.037971531	0.3218	80.66032562	0.450590429	٠.	179.0102951
Area 8 Slope 0-5%	1.5033	7	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.018412784		836.2528793	0.507169124	834.7495793	
Slope 5-10%	0.3173	71	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.01845728		176.5070436	0.10704767	176.1897436	
Slope 10-20% Slope >20%	0.598	<u> </u>	0.2772	4.6388912		6.0	0.16	0.25	0.95	0.089646435	2.9641	303.4497078 332.6543084	0.184035626	332,0563084 16	1648.863939
Area 9			2.17.0	1000000			2	Circ	9						
Slope 0-5%	0.0392	F i	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.000480131		21.80610182	0.098989899	21.76690182	
Slope 5-10%	0.0001	F 1	0.2772	1.6420015		6.0	0.16	0.25	0.95	5.81698E-06		0.055627811	0.000252525	0.055527811	
Slope >20%	0.2599		0.2772	7.3920692		e:0 6:0	0.16	0.25	0.95	0.068060695	0.396	144.5766802	0.656313131		220.2861307
Area 10		i							-				1		
Slope 0-5%	0.7927	F F	0.2772	0.3457401		6.0	0.16	0.25	0.95	0.009709183		440.961656	0.503877447	440.168956	
Slope 10-20%	0.2878	7.7	0.2772	4.6388912		6.0	0.16	0.25	0.95	0.047296506		160.0968394	0.182939232		
Slope >20%	0.3984	71	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.104330054	1.5732	221.6211981	0.2532418	221.2227981 87	875.1367191
Area 11 Slope 0-5%	0.1365	7	0.5016	0.3457401	-	6.0	0.16	0.25	0.95	0.003025316		75.9319617	0.441747573	75.7954617	
Slope 5-10%	6900.0	71	0.5016	1.6420015	-	6.0	0.16	0.25	0.95	0.000726292		3.838318943	0.022330097	3.831418943	
Slope 10-20%	0.062	۲ <i>۲</i>	0.5016	4.6388912		6.0	0.16	0.25	0.95	0.01843717 0.049092388	608:0	34.48924268 57.63041196	0.200647249	34.42724268 57.52681196 17	171.8899353
Area 12															
Slope 0-5%	0.3648	F 7	0.2772	0.3457401	- ,	6.0	0.16	0.25	0.95	0.004468159		202.9302537	0.192374624	202.5654537	
Slope 5-10%	0.1759	< F	0.2772	1.6420015		n.o	0.16	0.25	0.95	0.010232069		97.84931915	0.092/59584	97.67341915	
Slope >20%	0.8386	71	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.219606383	1.8963	466.4948211	0.442229605		1054.870176
Area 13	8000	7	2,03,0	0.3457404	•	0	910	30.0	20 0	70,0000000		22 69614679	0.10151779	22 65534670	
Slope 5-10%	0.0348		0.5016	1.6420015		6.0 6.0	0.16	0.25	0.95	0.003663036		19.35847815	0.086588704	19.32367815	
Slope 10-20%	0.1562	7.7	0.5016	4.6388912		6.0	0.16	0.25	0.95	0.046449773	0,404	86.89064042	0.388653894		223 5681715
Area 14				1000100	-	2	2	24:0	200			1	1		
Slope 0-5%	0.8678	7.7	0.5016	0.3457401		6.0	0.16	0.25	0.95	0.019233475		482.7381419	0.513916854	481.8703419	
Slope 10-20%	0.1855		0.5016	4.6388912		6.0	0.16	0.25	0.95	0.055162823		103.189589	0.109854317	103.004089	
Slope >20%	0.4904	71	0.5016	7.3920692	-	6.0	0.16	0.25	0.95	0.232383273	1.6886	272.798784	0.290418098		939.3312127
Area 15 Slope 0-5%	0.9862	7	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.012079218		548.6014698	0.258716126	547.6152698	
Slope 5-10%	0.0835	7	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.004857179		46.44922199	0.021905087	46.36572199	
Slope 10-20%	0.3967	۲ <i>۲</i>	0.2772	4.6388912		6.0	0.16	0.25	0.95	0.065192925	6. 6.	220.6755253 1304 750302	0.104068837	220.2788253 1302 404802 21	2120 476519
Area 16							5								
Slope 0-5%	0.5971	<u> </u>	0.5016	0.3457401		6.0	0.16	0.25	0.95	0.013233819		332.1536581	0.58821791	331.5565581	
Slope 10-20%	0.1583	7 7	0.5016	4.6388912		6.0	0.16	0.25	0.95	0.047074258		88.05882445	0.155945227	87.90052445	
Slope >20%	0.0991	71	0.5016	7.3920692	-	0.9	0.16	0.25	0.95	0.046959997	1.0151	55.12716047	0.09762585	55.02806047 56	564.6779071
Area 17 Slope 0-5%	0.6855	7	0.0779	0.3457401	-	60	0 16	70.0	0.95	0.008396171		381 3286428	0.519436236	380 6431428	
Slope 5-10%	0.0629	7	0.2772	1.6420015		6.0	0.16	0.25	0.95	0.003658881		34.98989298	0.047662348	34.92699298	
Slope 10-20%	0.1984	F 7	0.2772	4.6388912		6.0	0.16	0.25	0.95	0.03260468	1 2107	110.3655766	0.150337198	110.1671766	73/ 1202188
Area 18	0.0123		0.5772	7.5350035		6.0	5	0.43	0.90	0.03700200	20.0.	+00100+: 102	0.20204213		04.1202100
Slope 0-5%	0.4202	Fi	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.005146712		233.7480609	0.48337743	233.3278609	
Slope 5-10% Slope 10-20%	0.2141	< F	0.2772	1.6420015		6.0	0.16	0.25	0.95	0.012454156		119.0991429	0.209363856	118.8850429	
Slope >20%	0.053	71	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.013879249	0.8693	29.48273971	0.060968595		483.572559
Area 19 Slope 0-5%	0.9161	7	0.5016	0.3457401	-	6.0	0.16	0.25	0.95	0.020303972		509.6063745	0.748325437	508.6902745	
Slope 5-10%	0.0531		0.5016	1.6420015	-	6.0	0.16	0.25	0.95	0.005589288		29.53836752	0.043375265	29.48526752	
Slope 10-20%	0.1488	7	0.5016	4.6388912	-	6.0	0.16	0.25	0.95	0.044249208		82.77418243	0.121548/6/	82.62538243	

	Slope >20%	0.1062	71	0.5016	7.3920692	-	6.0	0.16	0.25	0.95	0.050324436		1.2242		59.07673504	0.086750531	58.97053504 680.9956595	0.9956595
	Area 20																	
	Slope 0-5%	0.1055	Fi		0.3457401	- ,	0.0	0.16	0.25	0.95	0.00129219				58.68734036	0.761732852	58.58184036	
	Slope 5-10%	0.0207	< F	0.2772	1.6420015		6.0 6.0	0.16	0.25	0.95	0.001204115				4 617108294	0.149458484	11.49425683 4.608808294	
	Slope >20%	0.004			7.3920692	-	0.0	0.16	0.25	0.95	0.00104749		0.1385		2.225112431	0.028880866		77.04451792
	Area 21		i													1000	0.0000	
	Slope 0-5%	0.2541	7 7	5016	0.345/401	- •	D 0	0.16	0.25 0.25 0.25	0.95	0.005631742				141.3502672	0.634615385	141.0961672	
	Slope 5-10%	0.0396	7 7		1.6420015	- •	n o	0.10	0.20	0.90	0.00628452/				33.26343064	0.149330049	33.20303004	
	Slope >20%	0.0325		5016	7.3920692		e 6.0	0.16	0.25	0.95	0.015400604	3.968943853	0.4004	25.5268	18.0790385	0.081168831		222.7337543
4	Area 1																	
	Slope 0-5%	1.188	7	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.014550913				17.06651343	0.403450384	15.87851343	
	Slope 5-10%	0.1683	7		1.6420015	-	6.0	0.16	0.25	0.95	0.009789979				2.41775607	0.057155471	2.24945607	
	Slope 10-20%	0.3024	7		4.6388912	-	0.0	0.16	0.25	0.95	0.049695842				4.344203419	0.102696461		
	Slope >20%	1.2859	7.1	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.336742008		2.9446		18.47292056	0.436697684	17.18702056 42	42.30139348
	Area 2		ř		70,11	,	(				0070711000				***************************************	74.04.00	* *************************************	
	Slope U-5%	2.5951			0.345/401	- ,	6.0	0.16	0.2.0 0.2.0	C.9.0	0.05/516468				37.28056314	0.9494/3145	34.68546314	
	Slope 5-10%	0.1266	7 7		1.6420015	- ,	9.0	0.16	0 K	C.6.0	0.013325872				1.818/04209	0.046319333	1.692104209	
	Slope 10-20%	0.008/		0.5016	4.6388912 7.3920692		n. o	0.16	0.25	0.90	0.002587 [5]		0 7330		0.124982043	0.003183082	0.116262043	39 2644735
	Area 3	01000			1000				31.0	200			100		000			
	Slope 0-5%	1.3112	71		0.3457401	-	6.0	0.16	0.25	0.95	0.016059897				18.83637408	0.490094939	17.52517408	
	Slone 5-10%	0.2511	7	0.2772	1 6420015		600	0.16	0.25	0.95	0.014606439				3 607240339	0.093855124	3.356140339	
	Slone 10-20%	0.4336			4 6388912		0.0	0.10	0.05	0.00	0.071257001				6 228990088	0.16206923	5 795390088	
	Slope >20%	0.6795	: -		7.3920692		6.0	0.16	0.25	0.95	0.177942449	0.765400842	2.6754	8.3532	9.761528516	0.253980713		38.43413303
2	Area 4																	
	Slope 0-5%	1.2918	71	0.5016	0.3457401	-	6.0	0.16	0.25	0.95	0.028630794				34.3694722	0.893360996	33.0776722	
	Slope 5-10%	0.1114	7		1.6420015	-	6.0	0.16	0.25	0.95	0.011725925				2.963894723	0.077040111	2.852494723	
	Slope 10-20%	0.0235	71	0.5016	4.6388912	-	6.0	0.16	0.25	0.95	0.006988282				0.625238115	0.016251729	0.601738115	
	Slope >20%	0.0193	71		7.3920692	1	6.0	0.16	0.25	0.95	0.00914559		1.446		0.51349343	0.013347165	0.49419343 38	38.47209846
	Area 5																	
	Slobe 0-5%	2.2292	7		0.3457401	-	6.0	0.16	0.25	0.95	0.027303784				59.3098215	0.256716762	57.0806215	
	Slope 5-10%	0.1105	7		1.6420015	-	6.0	0.16	0.25	0.95	0.006427764				2.939949433	0.012725284	2.829449433	
	Slope 10-20%	1.1824	7	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.194313373				31.45878923	0.136166292		
	Slope >20%	5.1614	71		7.3920692	-	6.0	0.16	0.25	0.95	1.351629366		8.6835		137.3235747	0.594391662	132.1621747 23	231.0321349
	Area 6		i												1	1		
	Slope 0-5%	0.0314	F 1		0.3457401	-	6.0	0.16	0.25	0.95	0.000695934				0.835424545	0.09570253	0.804024545	
	Slope 5-10%	0.0319	ς i		1.6420015	- ,	6.0	0.16	0.25	0.95	0.003357783				0.848/2/483	0.097226455	0.81682/483	
	Slope 10-20%	0.1634	< 7	0.5016	4.6388912	- •	n c	0.16	0.70	0.90	0.048590864		19000		4.34/400338	0.498018897	4.184000338 2.50642595	0 70000017
	30 pe >20 %	10.0	-		7800766.7	-	6.0	00	0.20	0.93	0.040043000		0.3201		2.037 03333	0.303035110		23300317
	Slone 0-5%	0 1224	77	0.5016	0.3457401		0	0.16	0.25	0.95	0.002712811				3 256559372	0.250562948	3 134159372	
	Slone 5-10%	0.019			1.6420015		6.0	0.16	0.25	0.95	0.001999933				0.505511667	0.038894575	0.486511667	
	Slope 10-20%	0.0647			4.6388912		6.0	0.16	0.25	0.95	0.019240079				1.721400256	0.132446264	1.656700256	
	Slope >20%	0.2824	7		7.3920692	-	6.0	0.16	0.25	0.95	0.133819405		0.4885		7.513499728	0.578096213		12.99697102
	Area 8																	
	Slope 0-5%	0.3886	71		0.3457401	-	6.0	0.16	0.25	0.95	0.008612732				10.33904389	0.331485115	9.950443889	
	Slope 5-10%	0.0211	7		1.6420015	-	6.0	0.16	0.25	0.95	0.002220979				0.561384009	0.017998806	0.540284009	
	Slope 10-20%	0.1842	۲ i		4.6388912	-	6.0	0.16	0.25	0.95	0.054776237		1		4.900802584	0.157127015		
	%02< adole	0.5784	-	0.5016	7.3920692	-	6.0	0.16	0.25	0.90	0.274083371		1.1723		10.388833838	0.493389084	14.61045959 31	31.19000967
	Slone 0-5%	2 7681	7	0.0779	0.3457401		0.0	910	0.05	0.05	0.033904363				73 64772874	0.234945128	70 87962874	
	Slope 5-10%	0.8022			1.6420015		6.0	0.16	0.25	0.95	0.046663821				21.34323471	0.06808749	20.54103471	
	Slope 10-20%	2.5318	71		4.6388912	-	6.0	0.16	0.25	0.95	0.416071209				67.36075995	0.21488894	64.82895995	
	Slope >20%	5.6798	71	0.2772	7.3920692	1	6.0	0.16	0.25	0.95	1.487384134		11.7819		151.1160614	0.482078442	145.4362614 31	313.4677848
	Area 10																	
	Slope 0-5%	1.1832	7		0.3457401	-	6.0	0.16	0.25	0.95	0.026223839				31.48007393	0.65136251	30.29687393	
	Slope 5-10%	0.3828	7		1.6420015	-	6.0	0.16	0.25	0.95	0.040293395				10.1847298	0.21073493	9.801929801	
	Slope 10-20%	0.1868	5 7	0.5016	4.6388912	- ,	6.0	0.16	0.25	0.95	0.055549409		0.00		4.969977865	0.102835122		20067507
	Sighe >20%	0.0037	-	0.301.0	7.3920092		6.0	0.10	0.20	0.90	0.0001000.0		0010.1		1.0947.9437.9	0.033007437	1.051094579 40	40.02937.397
	Slope 0-5%	0.3045	71	0.2772	0.3457401		6.0	0.16	0.25	0.95	0.00372959				8.101489614	0.39048474	7.796989614	
	Slope 5-10%	0.1425	7		1.6420015	-	6.0	0.16	0.25	0.95	0.008289198				3.791337504	0.182739164	3.648837504	
	Slope 10-20%	0.2114	71		4.6388912	-	6.0	0.16	0.25	0.95	0.034741075				5.624482445	0.271095153	5.413082445	
	Slope >20%	0.1214	71	0.2772	7.3920692	٦	6.0	0.16	0.25	0.95	0.031791337		0.7798		3.229953495	0.155680944	3.108553495 20	20.74726306
	Area 12	7017	i		20,000	,	C	9	L		1000000				0000000	0.0040000	00000	
	Slope 0-5%	0.4734	< F		0.345/401		n o	0.16	0.25	0.95	0.010492195				12.5952228 2 644624196	0.634669527	12.12182228	
	Slone 10-20%	0.0965		0.5016	4 6388912		n o	0.16	0.25	0.95	0.028696563				2.567467152	0.129373911	2.470967152	
Ī					-		3	,	)	2	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,							

Slope >20%	0.0766	71	0.5016	7.3920692	1	0.0	0.16	0.25	0.95	0.03629804	0.7459	2.038010195	0.102694731	1.961410195 19.84532382	19.84532382
Area 13															
Slone 0-5%	0.6494	71	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.007954009		17.27785667	0.453396635	16.62845667	
700000000000000000000000000000000000000	1007	1	0 0 0 0	10000	,		0.70			0.0000000000000000000000000000000000000		0.0001700004	70000000	40000004	
%01-c adols	0.1365	7	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.007940179		3.631702241		3.495202241	
Slope 10-20%	0.4554	7	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.074839572		12.11631649		11.66091649	
Slope >20%	0.191	7	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.050017671	1.4323	5.08172255	0.133351951	4.89072255	38.10759795
Area 14															
Slope 0-5%	0.0219	7	0.5016	0.3457401		6.0	0.16	0.25	0.95	0.00048538		0.582668711	0.184343434	0.560768711	
Clone F 108/	0.0700	7	91010	1 6400046	,		9	100	100	0.007746600		1 0500100	0.617009967	1 0760100	
Siope 3-10%	0.0733	- i	0.3010	1.0420013		0.0	00	0.20	0.90	0.007		90120001.		0016070.1	
Slope 10-20%	0.0173	7	0.5016	4.6388912	-	6.0	0.16	0.25	0.95	0.005144565		0.460281676		0.442981676	
Slope >20%	0.0063	7	0.5016	7.3920692	-	6.0	0.16	0.25	0.95	0.002985348	0.1188	0.167617027	0.053030303	0.161317027	3.160778214
Area 15															
Slope 0-5%	0.8079	71	0.5016	0.3457401		6.0	0.16	0.25	0.95	0.017905882		21.49488821	0.659941186	20.68698821	
Slone 5-10%	0 112	7	0.5016	1 6420015		0	0.16	0.25	0 95	0.011789081		2 979858249	0.091488319	2 867858249	
Slope 10-20%	0 1602	7	0.5016	4 6388010		0.0	9 0	30.0	0.05	0.050345369		4 504375014		4 335075014	
Slope 1020/2	0.100	7.7	0.00	7 2020602		9 0	9 9	2.0		0.000043003	1 2242	4:304014		2 456703425	22 5700140
Siope >20 %	0.1.00		0.00.0	7.3320032	-	6.0	0.10	0.20	0.90	14/1/6590.0	2422.1	3.391793423	0.110270033	0.4007.90460	02.37.03143
Area 16															
Slope 0-5%	0.6664	7	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.008162229		17.73015658	0.597079115	17.06375658	
Slope 5-10%	0.1529	7	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.008894164		4.068038627	0.136994893	3.915138627	
Slope 10-20%	0.2198	71	0.2772	4.6388912		6.0	0.16	0.25	0.95	0,036121515		5.847971814		5.628171814	
Slope >20%	0.077	7	0.2772	7 3920692		00	0.16	0.25	0 95	0 020164192	1 1161	2 048652546		1 971652546	29 69481957
SIODE /20/8	10.0		0.5112	2000200.1		0.0	5	0.50	0.00	20101020		2:04020040	100000000	0+0300170.1	00000
Area 17															
Slope 0-5%	11.1025	7	0.2772	0.3457401	-	6.0	0.16	0.25	0.95	0.135986124		295.3917519		284.2892519	
Slope 5-10%	1.2694	7	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.073840755		33.77350055	_	32.50410055	
Slope 10-20%	1.1628	7	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.191092346		30.93731403	0.082165646	29.77451403	
Slope >20%	0.6172	7	0.2772	7.3920692	-	6.0	0.16	0.25	0.95	0.161627784	14.1519	16.42114742	0.043612518	15.80394742	376.5237139
Area 18															
Slone 0.5%	5 4906	7	0.5016	0.3457401	٠	0	0.16	0.05	0.05	0.121690849		146 0822295	0.788550748	140 5916295	
Sleep 5 408/	0.400	. 7	0.00	10400040	. ,	o 6	5 6	2.0	0.00	0.048840407		40.0000000	0.000000140	11 97600596	
200be 3-10%	0.4030	- i	0.3016	1.0420015	- ,	0.0	0.70	0.20	0.90	0.040019427		12.33900300		0.0000000000000000000000000000000000000	
Siope 10-20%	0.4787	ς ;	0.5016	4.6388912		6.0	0.16	0.25	0.95	0.142352795		12.73623343		12.25/53343	
Slope >20%	0.5298	71	0.5016	7.3920692	-	6.0	0.16	0.25	0.95	0.251053544	6.9629	14.09579375	0.076088986	13.56599375	185.2540625
Area 19															
Slope 0-5%	6.3419	7	0.5016	0.3457401	-	6.0	0.16	0.25	0.95	0.140558626		168.7318128	0.903005795	162.3899128	
Slope 5-10%	0.3299	7	0.5016	1.6420015	-	6.0	0.16	0.25	0.95	0.03472516		8.777278896	0.046973559	8.447378896	
Slope 10-20%	0.2865	7	0.5016	4.6388912	-	6.0	0.16	0.25	0.95	0.085197568		7.622583824	0.040793951	7.336083824	
Slope >20%	0.0648	7	0.5016	7.3920692	-	6.0	0.16	0.25	0.95	0.030706436	7.0231	1.724060844	0.009226695	1.659260844	186.8557363
Area 20															
Slope 0-5%	0.6919	71	0.2772	0.3457401	-	0.9	0.16	0.25	0.95	0.00847456		18.40860645	0.664840972	17.71670645	
Slope 5-10%	0.235	7	0.2772	1.6420015	-	6.0	0.16	0.25	0.95	0.013669905		6.252381147	0.225809551	6.017381147	
Slope 10-20%	0.0904	7	0.2772	4.6388912	-	6.0	0.16	0.25	0.95	0.014856164		2.405171301	0.08686461	2.314771301	
Slope >20%	0.0234	71	0.2772	7.3920692		6.0	0.16	0.25	0.95	0.006127819	1.0407	0.622577527	0.022484866	0.599177527	27.68873643
Area 21															
Slone 0-5%	1 6663	7	0.5016	0.3457401	•	0	0.16	0.05	0.05	0.036931091		44 33337309	0.519533564	42 66707322	
Siope 0-3/8	0000-	7.7	0.00	0.00004	- ,	o 0	5 6	2.0	0.90	0.000001021		14.30337.322	0.013333334	14 24100901	
200 9-10%	2000.0	- i	0.3016	1.0420015	- ,	0.0	0.70	0.20	0.90	0.000040419		14.7.9019991	0.17.04.10095	14.24190091	
Slope 10-20%	0.6075	ς ;	0.5016	4.6388912		6.0	0.16	0.25	0.95	0.180654529				15.5555/041	
Slope >20%	0.3773	7	0.5016	7.3920692	-	6.0	0.16	0.25	0.95	0.17878917	<b>6.825237487</b> 3.2073 63.5198	98 10.03839748	0.117637889	9.661097476	85.33303002

138.7981 Total Area (ha)

Peat	Clay	Silt	Sand	
Sample 1	16	71	. 13	
Sample 2	15	99	19	
Average	15.5	68.5	16	
Sand Soils				
Sample 1	1	9	. 93	
Sample 2	2	∞	90	
Average	1.5	7	91.5	
Gravels	10	20	70	

Metric Convert K Factor	0.5016	0.2772
Value	0.38	0.21
Correction Factor Peat (4% Organic) Sand/Gravels (0% Organic)	-0.14	0.06
Nomograph Value	0.52	0.15

Sitename: M2PP Paraparaumu Coordinate system: NZMG Easting: 2679016 Northing: 6030188

Rainfall depths (mm)

 ARI(y)
 aep
 10m
 30m
 60m
 2h
 6h
 12h
 4h
 4h
 72h

 1.58
 0.633
 7
 9.9
 12.2
 17.5
 2.4
 40.6
 56.3
 78
 99.4
 78h

 2
 0.5
 7.5
 10.7
 13.2
 18.9
 26.1
 43.6
 60.3
 82.8
 96.5
 105.6

 10
 0.1
 11.2
 16.8
 24
 32.8
 53.6
 73.1
 99.6
 116.1
 127

 20
 0.05
 1.6
 13.7
 16.8
 24
 32.8
 53.6
 73.1
 99.6
 116.1
 127

 20
 0.05
 1.1
 1.6
 1.9
 28.2
 38.1
 60.5
 112.6
 147.6
 161.5

 20
 0.03
 1.4
 2.0
 28.2
 38.1
 60.3
 147.6
 147.6
 161.5

 20
 0.03
 1.4
 2.0
 38.2
 44.1
 70.3
 39.4
 10.9

Extreme rainfall assessment with climate change

Projected temperature change: 2.0 ° C Rainfall depths (mm)

72h 106.4 113 139.2 160.5 184.1 199.3 209.6 218 224.7 235.5 244.3 48h 97.8 103.8 127.7 147.2 168.6 182.5 191.8 199.3 205.3 223.3 24h
84.7
89.9
110.4
126.8
144.8
157.1
164.7
171
176.1
184.7 12h 61.7 65.8 81.6 108.1 117.5 123.7 128.6 132.8 139.7 145.2 94 44.9 60.1 69.9 80.7 87.9 92.8 96.7 100.1 100.1 **9** Duration 27.2 27.2 29.3 37.2 43.6 50.8 55.6 58.9 61.7 64.7 60m 19.8 21.4 27.4 37.9 44.5 46.4 46.4 48.3 51.3 53.8 14 15.1 19.3 22.7 26.6 29.1 31 32.5 33.8 35.8 20a 11.4 12.3 15.8 18.5 21.6 23.7 25.1 26.3 27.4 27.4 29.1 30.5 8.1 8.7 11.1 13 15.1 16.5 17.5 18.4 19.1 20.4 21.3 0.5 0.1 0.05 0.03 0.025 0.02 0.017 5 10 20 30 40 50 60 80 ARI (y) 1.58

Rainfall Erosion Index (J/ha) - Based on NIWA HIRDS Data

R = 0.00828p2.2\*1.7

48.1 p = 6 hour duration 2 year storm

R Factor 71

Sitename: M2PP PekaPeka Coordinate system: NZMG Easting: 2685968 Northing: 6038488

		24h
		12h
	tion	eh
	Duration	2h
		60m
		30m
		20m
Ê		10m
lepths (m		aeb
Rainfall depths (mm		ARI (y)

	72h	86	104.1	125.4	141.9	159.8	171	179.4	186.2	192	201.3	208.9
	48h	88	93.5	112.6	127.4	143.4	153.5	161.1	167.2	172.3	180.7	187.5
	24h	73.2	7.7.7	93.7	106	119.3	127.7	134	139	143.3	150.3	156
					79.8							
_	ę,	39.9	42.7	52.4	60.1	68.4	73.8	77.8	81.1	83.8	88.3	95
Duratio	7h	24.7	26.5	33.1	38.3	44.1	47.8	9.09	52.8	54.8	28	60.5
	60m	18.3	19.7	24.8	28.8	33.4	36.3	38.5	40.3	41.9	44.4	46.5
	30m	13	14.1	17.7	50.6	23.9	56	27.6	28.8	29.9	31.8	33.2
	20m	10.7	11.6	14.5	16.9	19.6	21.3	22.6	23.7	24.6	26.1	27.3
	10m	7.7	8.3	10.4	12.1	14	15.3	16.2	16.9	17.6	18.7	19.5
	æ				0.1							
	ARI (y)	1.58	2	2	10	20	30	40	20	09	80	100

Extreme rainfall assessment with climate change

Projected temperature change: 2.0 ° C Rainfall depths (mm)

						- Dara	5				
ARI (y)		10m	20m	30m	e0m	Zh	<b>9</b>	12h	24h	48h	72h
1.58		8.9		14.9	20.8	27.8	44.1	59.2	79.5	94.7	104.9
2		9.6		16.1	22.3	29.8	47.2	63.1	84.4	100.6	111.4
5		12.1		20.3	28.3	37.5	58.8	78.2	103.8	123.9	137.4
10	0.1	14	19.5	23.7	33.1	43.8	68.3	90.2	119.4	142.9	158.6
20		16.2		27.6	38.5	20.8	78.5	103.6	136.5	163.8	182.2
30		17.7		30.2	42.1	55.4	85.6	112.6	148.1	177.4	197.3
40		18.8		32	44.7	58.7	90.2	118.4	155.4	186.6	207.6
20		19.6		33.4	46.7	61.2	94.1	123.2	161.2	194	216
09		20.4		34.7	48.6	9.89	97.2	127.1	166.2	199.9	222.7
80		21.7		36.9	51.5	67.3	102.4	133.6	174.3	209.6	233.5
100		22.6		38.5	53.9	70.2	106.7	139	181	217.5	242.3

m 0.2 for slopes < 1%</li>
0.3 for slopes 1 to 3%
0.4 for slopes 3.5 to 4.5%
0.5 for slopes > 5%

Siope (AV/Mid Siope)	Area	20	0000110			- meion	***	3
Area 1								
2.5	9.9	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	1.44	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.54	225	10225	101 1187421	100	30.48	0.5	4 638891224
20	0.36	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 2								
2.5	0.5122	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0592	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0596	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1002	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 1								
2.5	4.426	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	689 0	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	1.5453	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	2.7361	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 2								
2.5	0.5863	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.2276	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.4838	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	1.8145	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 3								
2.5	2.8566	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0312	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1189	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1554	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 4								
2.5	0.3701	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0062	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0343	225	10225	101.1187421	100	30.48	9.0	4.638891224
20	0.2649	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 5								
2.5	0.0402	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0066	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.0646	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.2026	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 6								
2.5	0.1491	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.323	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.1127	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.1493	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 7								
2.5	0.2967	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.0719	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.2426	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.3879	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 8								
2.5	1.119	6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
7.5	0.3714	56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
15	0.5687	225	10225	101.1187421	100	30.48	0.5	4.638891224
20	0.4171	400	10400	101.9803903	100	30.48	0.5	7.392069161
Area 9								
LI C	* 111	100	LO 0000	+ UV 00 00 +	007		0	V 0 0 4 1 1 4 0 0 0

3	4	_		4	3	4	_		4	8	4	_		4	3	4	_	Į.	4 0	20 8	+ -	-	4		4	_		4	3	4	_	_	t c	0 4	_		4	3	4	_		4	2	+ -	_	4	3	4	_		4	2 2	t	_	4		4	F
1.64200152	4.638891224	7.39206916		0.345740084	1.64200152	4.63889122	7.39206916		0.345740084	1.64200152	4.638891224	7.39206916		0.345740084	1.64200152	4.63889122	7.392069161	000711700	1.345/40084	1.642001523	3199069-4	0.00000.7	0.34574008	1,642001523	4.63889122	7.39206916		0.34574008	1.642001523	4.63889122	7.39206916	0 34574008	1 642001523	4.63889122	7.392069161		0.345740084	1.64200152	4.63889122	7.392069161		0.345740084	1.64200152	7 202060162	7.39200910	0.34574008	1.642001523	4.63889122	7.392069161		0.345740084	1.64200152	7 20206016	7.39200910	0.34574008	1.64200152	4.63889122	7.392069161
0.5	0.5	0.5		0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5	0	0.3	0.0	5.0	2	0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5	٥,	5.0	0.5	0.5		0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.0	0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5	0.3	0.5	0.5	0.5
30.48	30.48	30.48		30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.48		30.48	30.48	30.40	2	30.48	30.48	30,48	30.48		30.48	30.48	30.48	30.48	20.48	30.40	30.48	30.48		30.48	30.48	30.48	30.48		30.48	30.48	30.40	30.40	30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.40	30.48	30.48	30.48	30.48
100	100	100		100	100	100	100		100	100	100	100		100	100	100	100	007	001	100	100	3	100	100	100	100		100	100	100	100	100	100	100	100		100	100	100	100	-	100	001	00 5	001	100	100	100	100		100	000,	00.5	001	100	100	100	100
100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903	100000	100.0312451	100.2808556	101 0803003		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903	100 0312451	100.0312431	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.116/421	101.9003903	100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.118/421	101.9803903	100.0312451	100.2808556	101.1187421	101.9803903
10056.25	10225	10400		10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400	10 00007	10006.25	10036.23	10400	000	10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400	10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400		10006.25	10056.25	10400	10400	10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400	10006.25	10056.25	10225	10400
56.25	225	400		6.25	56.25	225	400		6.25	56.25	225	400		6.25	56.25	225	400	100	6.25	36.25 22E	400	000	6.25	56.25	225	400		6.25	56.25	225	400	8.05	56.25	225	400		6.25	56.25	225	400		6.25	56.25	400	400	6.25	56.25	225	400		6.25	56.25	225	400	6.25	56.25	225	400
0.1415	0.3093	0.465		0.7131	0.0585	0.1527	0.1629		0.5134	0.0728	0.2617	0.1499		0.8128	0.346	0.3469	1.0737		0.3989	0.1825	0.0803		0.2864	0.0959	0.3364	2.6097		0.3664	0	0.012	0.0756	1 6887	1.0004	0.5939	1.1114		0.2064	0.0606	0.1931	0.4624		0.1254	0.03	0.1213	0.3303	0.0226	0	0.0194	0.1082		0.3833	0.1459	0.188	U.Z384	0.1175	0.0185	0.5	0.4904
7.5	15	20	Area 10	2.5	7.5	15	20	Area 11	2.5	7.5	15	20	Area 12	2.5	7.5	15	20	Area 13	7.5	7.5	6	Area 14	2.5	2.5	15	20	Area 15	2.5	7.5	15	20	Area 1	2.3	5. 12.	20	Area 2	2.5	7.5	15	20	Area 3	1 100	7,5	23	Area 4	2.5	7.5	15	20	Area 5	2.5	/.5 1-1-	32 32	ZU Area 6	Area o	7.5	15	20

0.1358		10006.25	100.0312451	001	30.40	0.3	0.345740084
0.0038	38 56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
0.0372		10225	101.118/421	000	30.48	0.5	7 202060161
.0		10400	101.9603903	001	30.48	0:0	7.392009101
1.5033		10006.25	100.0312451	100	30.48	0.3	0.345740084
0.3173		10056.25	100.2808556	100	30.48	0.5	1.642001523
0.5455		10225	101.1187421	100	30.48	0.5	4.638891224
0.598		10400	101.9803903	100	30.48	0.5	7.392069161
0.0392		10006.25	100.0312451	100	30.48	0.3	0.345740084
0.0001	-,	10056.25	100.2808556	100	30.48	0.5	1.642001523
0.08		10225	101.1187421	100	30.48	0.5	4.638891224
0.2599	99 400	10400	101.9803903	100	30.48	0.5	7.392069161
0.7927	27 6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
0.0943		10056.25	100.2808556	100	30.48	0.5	1.642001523
0.28		10225	101.1187421	100	30.48	0.5	4.638891224
0.3984	84 400	10400	101.9803903	100	30.48	0.5	7.392069161
0 1365		10006 25	100 0312451	100	30.48	0.3	0.345740084
0.0069		10056.25	100.3808556	200	20.70	2.0	1 642001523
0.00		100001	100.2808338	001	30.40	5.0	1.042001323
0.062	252 29	10225	101.118/421	001	30.48	0.5	4.638891224
0.10		10400	101.9803903	100	30.48	0.5	7.392069161
0.3648		10006.25	100.0312451	100	30.48	0.3	0.345740084
0.1759	_,	10056.25	100.2808556	100	30.48	0.5	1.642001523
0.517		10225	101.1187421	100	30.48	0.5	4.638891224
0.8386	86 400	10400	101.9803903	100	30.48	0.5	7.392069161
0.0408		10006.25	100.0312451	100	30.48	0.3	0.345740084
0.0348		10056.25	100.2808556	100	30.48	0.5	1.642001523
0.15	62 22E	10225	101 1187421	100	30.48	0.5	4 638891224
0.1701		10400	101 9803903	100	30.48	200	7 392069161
5		000		2	2	2	101000000
0.8678		10006.05	100 0313461	100	07.00	000	0.00007400004
0.8878	70 0.23	10006.23	100.0312431	00 00	30.40	0.5	1 640004 500
0.14		10036.23	100.2000336	001	30.40	0.0	1.042001323
0.1855	55 225	10225	101.118/421	001	30.48	0.5	4.638891224
0.49		10400	101.9803903	100	30.48	0.5	7.392069161
0.9862	62 6.25	10006.25	100.0312451	100	30.48	0.3	0.345740084
0.0835		10056.25	100.2808556	100	30.48	0.5	1.642001523
0.39		10225	101.1187421	100	30.48	0.5	4.638891224
2.3455		10400	101.9803903	100	30.48	0.5	7.392069161
0.5971		10006.25	100.0312451	100	30.48	0.3	0.345740084
0.1606	06 56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
0.15		10225	101.1187421	100	30.48	0.5	4.638891224
0.0991	91 400	10400	101.9803903	100	30.48	0.5	7.392069161
0.6855		10006.25	100.0312451	100	30.48	0.3	0.345740084
0.0629	29 56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
0.1984		10225	101.1187421	100	30.48	0.5	4.638891224
0.3729		10400	101.9803903	100	30.48	0.5	7.392069161
0.4202		10006.25	100.0312451	100	30.48	0.3	0.345740084
0.2141	41 56.25	10056.25	100.2808556	100	30.48	0.5	1.642001523
0.1		10225	101.1187421	100	30.48	0.5	4.638891224
0.053		10400	101.9803903	100	30.48	0.5	7.392069161
5		0000	000000000000000000000000000000000000000	3	2	5.	101000000
70700							
	G 1	10006 25	100 031 2451	100	30.48	80	0.345740084

101 224	169161		40084	1 642001523	301224	12127	10160	0.345740084	40004	1.642001323	391224	169161		740084	1.642001523	391224	169161	7000	40084	91 224	7.392069161		740084	1.642001523	391224 36 : 2:	169161	740084	001523	391224	7.392069161		0.345/40084	4 638891224	169161		740084	001523	4.638891224	169161	740084	1001	391224	7.392069161		0.345740084	001523	391224	169161	40084	1 642001523	391224	7.392069161		0.345740084	001523	391224
	0.5 7.392069161			0.5 1 6420				-	0.3 0.3437	Ť		0.5 7.3920			0.5 1.6420			F	0.345/40084		0.5 7.3920			0.5 1.6420	Ì				0.5 4.6388		ŀ	0.3 0.3457	T					0.5 4.6388		F	0.5 1.642001523	0.5 4.6388	T		0.3 0.3457				-	0.5 1 6420		0.5 7.3920			0.5 1.6420	
	30.48			30.48				87.05		30.48		30.48			30.48				30.48					30.48					30.48				30.48				30.48		30.48			30.48			30.48					30.48					30.48	
100	001	202	100	100	8 6	00-	001	100	001	001	100	100		100	100	100	100	007	00 5	100	100		100	100	100	100	100	100	100	100		100	100	100		100	100	100	100	100	100	100	100		100	100	100	100	100	201	100	100		100	100	100
101 1107431	101.1187421	000000000000000000000000000000000000000	100.0312451	100 2808556	101 1187421	101.101	000000000000000000000000000000000000000	100 0319451	100.0312431	0008082.001	101.118/421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903	747070000	100.0312451	100.2606336	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903	100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	101 1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903	100 0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903	100 0312451	100.0012431	101,1187421	101.9803903		100.0312451	100.2808556	101.1187421
10005	10400		10006.25	10056.25	10225	10400	00+01	10006.25	10006.23	10026.23	10225	10400		10006.25	10056.25	10225	10400	10 00001	10006.25	10255	10400		10006.25	10056.25	10225	10400	10006.25	10056.25	10225	10400		10006.25	10225	10400		10006.25	10056.25	10225	10400	10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400	10006.25	10056.25	10225	10400		10006.25	10056.25	10225
200	400	P	6.25	56.25	225	700	400	202	0.23	26.25	225	400		6.25	56.25	225	400	i c	0.23	20.23	400		6.25	56.25	225	400	6.25	56.25	225	400		6.25	20.23	400		6.25	56.25	225	400	625	56.25	225	400		6.25	56.25	225	400	625	56.25	225	400		6.25	56.25	225
0 1400	0.1460	300	0.1055	0.0207	0.0207	0.000	‡00.0	0.0541	0.234	0.038	0.054	0.0325		1.188	0.1683	0.3024	1.2859	1	7.0901	0.1280	0.0028		1.3112	0.2511	0.4336	0.6795	1,2918	0.1114	0.0235	0.0193		2.2292	1 1824	5.1614		0.0314	0.0319	0.1634	0.1014	0 1224	0.019	0.0647	0.2824		0.3886	0.0211	0.1842	0.5784	2 7681	0.001.3	2.5318	5.6798		1.1832	0.3828	0.1868
Ť.	200	Area 20	2.5	7.5	5 £	2.00	20 A.c. 01	Areazi	2.5	5.7	15	20	Area 1	2.5	7.5	15	20	Area 2	7.5	7.5	20	Area 3	2.5	7.5	15	20	2.5	7.5	15	20	Area 5	2.5	15	20	Area 6	2.5	7.5	15	20	25	7.5	15	20	Area 8	2.5	7.5	15	20	Area 9	7.5	15	20	Area 10	2.5	7.5	15

	c										c					~~	_			_		_,						_							~					_	.			. [			1		.		
0.345740084	1.642001523	4.638891224	7.392069161		0.345740084	1.642001523	4.638891224	7.392069161		0.345740084	1.642001523	4.638891224	7.392069161		0.345740084	1.642001523	4.638891224	7.392069161		0.345740084	1.642001523	4.638891224	7.392069161		0.345/40084	1.642001523	4.638891224	7.392069161	0 345740084	1.642001523	4.638891224	7.392069161		0.345740084	1.642001523	4.638891224	7.392069161		0.345/40084	1.642001523	4.638891224	7.392069161	0.0045740004	4.045041084	1.642001523	7 202060164	7.392009101	0.045740004	1.040740004	1.642001523	7 392069162
0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5		0.3	0.5	0.5	0.5	0	0.5	0.5	0.5		0.3	0.5	0.5	0.5	6	0.3	0.5	0.5	0.5	c	٥.0 د ر	0.0	0.0	0.0	0	ر د. د	0.5	0.5
30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.48	9	30.48	30.48	30.48	30.48	30.48	30.48	30.48	30.48		30.48	30.48	30.48	30.48	9	30.48	30.48	30.48	30.48	00 40	30.48	30.48	30.48	30.48	20.40	30.40	30.48	30.48
100	100	100	100		100	100	100	100		100	100	100	100		100	100	100	100		100	100	100	100		100	100	100	100	100	100	100	100		100	100	100	100		100	100	001	100	007	001	001	100	001	100	001	100	100
100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.118/421	101.9803903	100 031 9451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.1187421	101.9803903		100.0312451	100.2808556	101.118/421	101.9803903	400 004	100.0312451	100.2808556	101.116/421	101.9803903	100 001 0451	100.0312431	100.2808556	101.1187421
10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400	1	10006.25	10056.25	10225	10400	10006.25	10056.25	10225	10400		10006.25	10056.25	10225	10400		10006.25	10056.25	37701	10400	10000	10006.23	10056.25	10400	10400	10006.05	10006.23	10056.25	10225
6.25	56.25	225	400		6.25	56.25	225	400		6.25	56.25	225	400		6.25	56.25	225	400		6.25	56.25	225	400		6.25	56.25	225	400	8.05	56.25	225	400		6.25	56.25	225	400		6.25	56.25	577	400	1	6.25	56.25	622	400	90.9	6.23	56.25	225
0.3045	0.1425	0.2114	0.1214		0.4734	0.0994	0.0965	0.0766		0.6494	0.1365	0.4554	0.191		0.0219	0.0733	0.0173	0.0063		0.8079	0.112	0.1693	0.135		0.6664	0.1529	0.2198	0.07	11 1005	1.2694	1.1628	0.6172		5.4906	0.4638	0.4787	0.5298		6.3419	0.3299	0.2865	0.0648		2000	0.235	0.0904	0.0234	1 0000	0000	0.5562	0.6075
2.5	7.5	15	20	Area 12	2.5	7.5	15	20	Area 13	2.5	7.5	15	20	Area 14	2.5	7.5	15	20	Area 15	2.5	7.5	15	20	Area 16	2.5	7.5	13	20	Area I /	7.5	15	20	Area 18	2.5	7.5	15	20	Area 19	2.5	7.5	51	20	Area 20	2.3	6.7	60 00	20	Area 21	2.3	7.5	15

## USLE Calculation M2PP Pre Earthworks - Whole Catchment Area

Whareroa Wharemauku Waikanae Waimeha Ngarara Catchment 1 Catchment 2 Catchment 3 Catchment 4 Catchment 5

1600 1380 14200 120 1690 **Total Catchment Area (ha)** 

R factor based on NIWA HIRDS Data

Assumptions

K Factor based on soil samples and soils /gravels to be utilised - grass cover LS Factor based on different slopes with a uniform 100m slope length

C and P Factors based on a pastoral surface

Duration - for purposes of risk assessment has been based on 2 months total for each stage to provide comparison with earthworks scenario
Sedmentar Delivery Pation - based on a figh infiltration has and irregular surface capturing flow and sedment - 0.25 assumed figure
Efficiency - based on 0% as no control measures in place with existing situation
Assume pre earthworks surface is grass environment in all areas
Catchment Characteristics are based on project footprint and pro rata of specific areas (soil types and stope classes)

Pro Rata Sub Catchment Split	LI	Footprint Hectares	Total Catchment Footprint Area	L	*	<u> </u>	ပ	٥	time	sdr	sed eff.	Total Catchment Yield	Overall Catchment Yield Area	Proje	Project Footprint Area	Pro Rata Total Catchment Area	Slope % T. Total Catchment	Total Catchment Less Project Footprint	Pro Rata Total Catchment Area
-	Area 1																		
	Slope 0-5%	99.9	1095.034528	71	0.132	0.3457401		-	0.16	0.25	0	2.838571335				1095.034528	0.74	1088.374528	
	Slope 5-10%	4.1	236.7642223	71	0.132	1.6420015		-	0.16	0.25	0	2.914821061				236.7642223	0.16	235.3242223	
	Slope 10-20%	0.54	88.78658336	71	0.132	4.6388912		-	0.16	0.25	0	3.088046277				88.78658336	90.0	88.24658336	
	Slope >20%	0.36	59.19105557	71	0.132	7.3920692	0.05	1	0.16	0.25	0	3.280532717		6		59.19105557	0.04	58.83105557	1479.776389
	Area 2																		
	Slope 0-5%	0.5122	84.21571851	71	0.5016	0.3457401	0.02	-	0.16	0.25	0	0.829561817				84.21571851	84.21571851 0.700492341	83.70351851	
	Slope 5-10%	0.0592	9.73364025	71	0.5016	1.6420015		-	0.16	0.25	0	0.455359824				9.73364025	0.080962801	9.67444025	
	Slope 10-20%	0.0596	9.799408089	71	0.5016	4.6388912	0.05	-	0.16	0.25	0	1.295149483				9.799408089	0.081509847	9.739808089	
	Slope >20%	0.1002	16.4748438	71	0.5016	7.3920692	0.05	1	0.16	0.25	0	3.469710104	18.17175262	0.7312	9.7312	16.4748438	16.4748438 0.137035011	16.3746438	120.2236107
2	Area 1																		
	Slope 0-5%	4.426	192.9147369	71	0.132	0.3457401	0.02	-	0.16	0.25	0	0.500077603				192.9147369	92.9147369 0.471121708	188.4887369	
	Slope 5-10%	0.689	30.03123673	71	0.132	1.6420015	0.05	-	0.16	0.25	0	0.369716676				30.03123673	30.03123673 0.073340004	29.34223673	
	Slope 10-20%	1.5453	67.35452847	71	0.132	4.6388912	0.02	-	0.16	0.25	0	2.342627602				67.35452847	0.16448811	65.80922847	
	Slope >20%	2.7361	119.2575716	71	0.132	7.3920692	0.05	-	0.16	0.25	0	6.609585883	0)	9.3964		119.2575716	119.2575716 0.291241777	116.5214716	409.4796176
	Area 2																		
	Slope 0-5%	0.5863	25.54998721	71	0.1188	0.3457401	0.05	-	0.16	0.25	0	0.059608089				25.54998721	25.54998721 0.188387636	24.96368721	
	Slope 5-10%	0.2276	9.918432695	71	0.1188	1.6420015	0.05	-	0.16	0.25	0	0.109895873				9.918432695	9.918432695 0.073131547	9.690832695	
	Slope 10-20%	0.4838	21.08320623	71	0.1188	4.6388912	0.05	-	0.16	0.25	0	0.659956974				21.08320623	21.08320623 0.155452734	20.59940623	
	Slope >20%	1.8145	79.07291795	71	0.1188	7.3920692	0.05	-	0.16	0.25	0	3.944196681	69	3.1122		79.07291795	79.07291795 0.583028083	77.25841795	135.6245441
	Area 3																		
	Slope 0-5%	2.8566	124.4859176	71	0.1188			-	0.16	0.25	0	0.290425492				124.4859176	124.4859176 0.90338699	121.6293176	
	Slope 5-10%	0.0312	1.359644552		0.1188			-	0.16	0.25	0	0.015064812				1.359644552	1.359644552 0.009866861	1.328444552	
	Slope 10-20%	0.1189	5.181465938	71	0.1188			-	0.16	0.25	0	0.162192816				5.181465938	5.181465938 0.037601594	5.062565938	
	Slope >20%	0.1554	6.772075751	71	0.1188	7.3920692	0.02	1	0.16	0.25	0	0.337794524	3	3.1621		6.772075751	6.772075751 0.049144556	6.616675751	137.7991038
	Area 4																		
	Slope 0-5%	0.3701	16.12834772	71	0.1188			-	0.16	0.25	0	0.037627415				16.12834772	16.12834772 0.547890452	15.75824772	
	Slope 5-10%	0.0062	0.270185776	71	0.1188			-	0.16	0.25	0	0.002993649				0.270185776	0.270185776 0.009178386	0.263985776	
	Slope 10-20%	0.0343	1.49473744	71	0.1188			-	0.16	0.25	0	0.046789012				1.49473744	0.050777202	1.46043744	
	Slope >20%	0.2649	11.54390519	71	0.1188	7.3920692	0.02	-	0.16	0.25	0	0.575815762	0	0.6755		11.54390519	11.54390519 0.39215396	11.27900519	29.43717612
	Area 5																		
	Slope 0-5%	0.0402	1.751849712	71	0.1188			-	0.16	0.25	0	0.004087063				1.751849712	1.751849712 0.128025478	1.711649712	
	Slope 5-10%	0.0066	0.287617117	71	0.1188	1.6420015		-	0.16	0.25	0	0.003186787				0.287617117		0.281017117	
	Slope 10-20%	0.0646	2.815161477	71	0.1188			-	0.16	0.25	0	0.08812158				2.815161477		2.750561477	
	Slope >20%	0.2026	8.828973919	71	0.1188	7.3920692	0.02	1	0.16	0.25	0	0.440393633		0.314		8.828973919	0.64522293	8.626373919	13.68360222
	Area 6																		
	Slope 0-5%	0.1491	6.497532139	71	0.1188			-	0.16	0.25	0	0.015158734				6.497532139	6.497532139 0.203105844	6.348432139	
	Slope 5-10%	0.323	14.07580738	71	0.1188			-	0.16	0.25	0	0.155959433				14.07580738	14.07580738 0.439994551	13.75280738	
	Slope 10-20%	0.1127	4.911280161	71	0.1188	4.6388912		-	0.16	0.25	0	0.153735326				4.911280161		4.798580161	
	Slope >20%	0.1493	6.506247809	71	0.1188	7.3920692	0.05	1	0.16	0.25	0	0.324534894	0	0.7341		6.506247809	0.203378286	6.356947809	31.99086749
	Area 7	!																	
	Slope 0-5%	0.2967		≂ i	0.1188		0.02		0.16	0.25	o (	0.030164967				12.92969675	12.92969675 0.296967271	12.63299675	
	Slope 5-10%	0.0/19	3.133283439	-	0.1188	1.6420015		-	0.16	0.25	D	0.034/16666				3.133283439	3.133283439 0.071964768	3.061383439	

																	٠
*	Slope 10-20% Slope >20%	0.2426	10.57210796 16.90404237	71	0.1188	4.6388912 7.3920692	0.02		0.16 0.16	0.25	0	0.330933365	0.9991		10.57210796 0.242818537 16.90404237 0.388249424	10.32950796 16.51614237	43.53913052
	Area 8 Slope 0-5% Slope 5-10%	1.119	48.76417481	7.1	0.1188	0.3457401	0.02		0.16	0.25	0	0.11376676			48.76417481 0.451902108 16.18499957 0.149987885	47.64517481 15.81359957	
	Slope 10-20% Slope >20%	0.5687	24.78300823 18.17653022	17	0.1188	4.6388912 7.3920692	0.02		0.16	0.25		0.77577001	2.4762		24.78300823 0.229666424 18.17653022 0.168443583	24.21430823 17.75943022	107.9087128
	Area 9 Slope 0-5%	0.6771	29.50690148		0.1188	0.3457401	0.02		0.16	0.25		0.068839565			29.50690148 0.425073765	28.82980148	
	Slope 10-20% Slope >20%	0.3093	13.47878397		0.1188	4.6388912	0.02		0.16	0.25	000	0.421919578 0.421919578 1.010775121	1.5929		13.47878397 0.194174148 20.26393323 0.291920397	13.16948397 19.79893323	69.41595536
	Area 10 Slope 0-5%	0.7131	31.07572212	71	0.1188	0.3457401	0.02	-	0.16	0.25		0.072499621			31.07572212 0.655905077	30.36262212	
	Slope 5-10% Slope 10-20%	0.0585	2.549333535 6.654414203 7.098913383	E E E	0.1188	1.6420015 4.6388912 7.3920692	0.02		0.16	0.25	000	0.208299772 0.308299772	1 0872		2.549333535 0.053807947 6.654414203 0.140452539 7 098913383 0.149834437	2.490833535 6.501714203 6 936013383	47.37838324
	Area 11 Slope 0-5%	0.5134	22.37312542	71	0.5016	0.3457401	0.02	-	0.16	0.25		0.220385112				21.85972542	
	Slope 5-10%	0.0728	3.172503955	7.	0.5016	1.6420015	0.02		0.16	0.25	0 0	0.148416297				3.099703955	
	Slope >20%	0.1499	6.53239482	71	0.5016	7.3920692	0.02		0.16	0.25		1.375765172	0.9978			6.38249482	43.48247866
	Area 12 Slope 0-5%	0.8128	35.42048372	71	0.1188	0.3457401	0.02	-	0.16	0.25		0.082635945				34.60768372	
	Slope 5-10% Slope 10-20%	0.346	15.07810946 15.11732997	F E	0.1188	1.6420015 4.6388912	0.02		0.16	0.25	00	0.167064903				14.73210946 14.77042997	
	Slope >20%	1.0737	46.7900755	71	0.1188	7.3920692	0.02	-	0.16	0.25		2.33391236	2.5794		46.7900755 0.416259595	45.7163755	112.4059987
	Slope 0-5%	0.3989	17.38340423	71	0.5016	0.3457401	0.02	-	0.16	0.25		0.171234167				16.98450423	
	Slope 5-10% Slope 10-20%	0.1825	7.953049064 3.508057258	E E	0.5016	1.6420015 4.6388912	0.02		0.16	0.25	00	0.372060085				7.770549064 3.427557258	
	Slope >20%	0.0959	4.179163864	71	0.5016	7.3920692	0.02	-	0.16	0.25		0.880159306	0.7578		4.179163864 0.126550541	4.083263864	33.02367441
	Slope 0-5%	0.2864	12.48083974	77	0.1188	0.3457401	0.02	-	0.16	0.25		0.029117784				12.19443974	
	Slope 5-10% Slope 10-20%	0.0959	14.65975729	5 5 1	0.1188	4.6388912	0.02		0.16	0.25	000	0.45888699				14.32335729	0
	Area 15	7.6097	113.7.204227		0.1188	7.3920692	0.02	-	0.16	0.20		5.67.27.30823	3.3284		113.7264227 0.764070424	111.116/22/	143.0461836
	Slope 0-5% Slope 5-10%	0.3664	15.96710782		0.5016	0.3457401	0.02		0.16	0.25		0.157283025			15.96710782 0.807048458 0 0	15.60070782 0	
-,	Slope 10-20% Slope >20%	0.012	0.522940212		0.5016	4.6388912	0.02		0.16	0.25	00	0.069114965	<b>38.0201228</b> 0.454	31.6671	0.522940212 0.026431718 3.294523338 0.166519824	0.510940212	19.78457137
	Area 1																
	Slope 0-5% Slope 5-10%	1.6884	939.2199571	F E	0.5016	0.3457401	0.02		0.16	0.25		9.251729111			939.2199571 0.455204767 175.4501152 0.085034105	937.5315571 175.1347152	
	Slope 10-20% Slope >20%	0.5939	330.3735682	F E	0.5016	4.6388912	0.02		0.16	0.25	0 0	43.6641838	3.7091		330.3735682 0.160119706 618.2474889 0.299641422	329.7796682	2063.291129
	Area 2	70000	11.4 0150014		041	0.2457404	000		0 18	30.0		0.087986100				114 6094014	
	Slope 5-10%	0.0606	33.71045333	7 7	0.1188	1.6420015	0.02		0.16	0.25		0.373510594				33.64985333	
	Slope 10-20% Slope >20%	0.1931	107.4173026 257.222997	F E	0.1188	4.6388912 7.3920692	0.02		0.16	0.25	0 0	3.362429659	0.9225		107.4173026 0.209322493 257.222997 0.501246612	107.2242026 256.760597	513.1665544
	Area 3 Slope 0-5%	0.1254	69.75727471	71	0.1188	0.3457401	0.02	-	0.16	0.25		0.162743636			69.75727471 0.198104265	69.63187471	
	Slope 5-10%	0.03	16.68834323	7.	0.1188	1.6420015	0.02		0.16	0.25	0 0	0.184906235				16.65834323	
	Slope >20%	0.3563	198.2018898	71	0.1188	7.3920692	0.02		0.16	0.25		9.886409357	0.633		198.2018898 0.562875197	197.8455898	352.1240422
	Area 4 Slope 0-5%	0.0226	12.57188523	71	0.1188	0.3457401	0.02	-	0.16	0.25		0.029330193			12.57188523 0.150466045	12.54928523	
- 5,	Slope 5-10% Slope 10-20%	0.0194	0 10.79179529	<u> </u>	0.1188	1.6420015	0.02		0.16	0.25	0 0	0			0 0 10.79179529 0.129161119	0 10.77239529	
	Slope >20%	0.1082	60.18929125	71	0.1188	7.3920692	0.02	-	0.16	0.25		3.00227194	0.1502			60.08109125	83.55297178
	Slope 0-5%	0.3833	213.2213987		0.1188	0.3457401	0.02		0.16	0.25		0.49744526			213.2213987 0.401109251	212.8380987	
	Slope 10-20%	0.188	104.5802843		0.1188	4.6388912	0.02		0.16	0.25	000	3.273623904	9			104.3922843	524 5702507
	Area 6	0.2384	132.6167009	-	0.1100	7.3920092	0.02	-	0.10	0.73		0.01496/344	0.3330		1.32.0107.009 0.249470709	132.37.03003	1909 / 6.156
	Slope 0-5%	0.1175	65.36267766		0.1188	0.3457401	0.02		0.16	0.25		0.152491046			65.36267766 0.142182962 10.29114499 0.022386254	65.24517766	
	Slope 10-20% Slope >20%	0.2	111.2556215		0.1188	4.6388912	0.02		0.16	0.25	00	3.482578622	0.8264			111.0556215	459.7082282
	Area 7 Slope 0-5%	0.1358	75.54256703	77	0.1188	0.3457401	0.02	-	0.16	0.25	c	0.176240716			75.54256703 0.422001243	75.40676703	
	800000	3	000000000000000000000000000000000000000		3	04.00	100	-	2	0.50		0.1.02			0111001111000110001	000000000000000000000000000000000000000	

Slope 5-10% 0.0038		71		1.6420015	0.02	-			0	0.023421456		2.113856809 0.011808577	2.110056809	
.0		7	0.1188	4.6388912	0.02	_	0.16	0.25		0.647759624	1	20.69354561 0.115599751	20.65634561	
Slope >20% 0.145	80.66032562	71		7.3920692	0.02	-				4.023377369	0.3218	80.66032562 0.450590429	80.51532562	179.0102951
Area 6 Slope 0-5% 1.5033		71	0.1188	0.3457401	0.02	_			_	.950976935		836.2528793 0.507169124	834.7495793	
Slope 5-10% 0.3173		71		1.6420015	0.02	_			_	1.955691611			176.1897436	
. 0		7.		4.6388912	0.02		0.16	0.25 (	6 0	9.49873319	0	303.4497078 0.184035626	302.9042078	00000
Area 9 0.536	332.6343064		0.1100	7.3920092	0.02	_				0.59230322	7.304.1		332.0363064	1646.663939
		71		0.3457401	0.02	-				0.050873609			21.76690182	
		71	0.1188	1.6420015	0.02	<del>.</del> .				0.000616354			0.055527811	
Slope 10-20% 0.0968 Slope <20% 0.2599	3 53.84772083 144 5766802			4.6388912 7.3920692	0.02		0.16	0.25	0 0	1.685568053	968.0	53.84772083 0.24444444 144 5766802 0.656313131	53.75092083	220 2861307
			3	1000100						100				
Slope 0-5% 0.7927		71		0.3457401	0.02	_			0 1.	1.028762999		_	440.168956	
		Fi		1.6420015	0.02	<b>.</b> ,			ο ι	581221932			52.36272556	
Slope 10-20% 0.2878 Slope >20% 0.3984	160.0968394	< F	0.1188	7.3920692	0.02		0.16	0.25	0 5.	5.011430636	1.5732	160.0968394 0.182939232 221.6211981 0.2532418	221,222,7981	875.1367191
•					ļ									
		71		0.3457401	0.02	-				0.747963174			75.7954617	
J		7		1.6420015	0.02	<del>.</del> -	0.16	0.25	0 0.	0.179564499			3.831418943	
Slope 10-20% 0.062	34.48924268	- 1	0.5016	4.6388912	0.02				4 +	.558308462	0000	34.48924268 0.20064/249	34.42724268	171 0000052
Slope >20% 0.1036		1	0.5016	7.3920692	0.02	-	0.16	CS.		2.13/34255	0.309		96118975.76	171.8899353
Slope 0-5% 0.3648	3 202.9302537	71	0.1188	0.3457401	0.02	_	0.16		O	473436031		202.9302537 0.192374624	202.5654537	
. 0		71		1.6420015	0.02	-		0.25	0	1.08416689			97.67341915	
.0		71		4.6388912	0.02	-				9.002465737			287.0787817	
Slope >20% 0.8386	3 466.4948211	71	0.1188	7.3920692	0.02	1	0.16	0.25 (	0 23	23.26899491	1.8963	466.4948211 0.442229605	465.6562211	1054.870176
		i			;									
Slope 0-5% 0.0408	3 22.69614679	- 1	0.5016	0.3457401	0.02				0 0	0.223567015		22.69614679 0.10151779	22.65534679	
		- 7		1.6420015	20.0		0.16	0.70		0.905629648			19.32367613	
Slope >20% 0.1362				7.3920692	0.02					9.92820432	0.4019		94.45280612	223.5681715
Slope 0-5% 0.8678	3 482.7381419	71		0.3457401	0.02	-			0 4.	4.755182731			481.8703419	
	∞	7		1.6420015	0.02	<del>.</del> -	0.16			3.770854483			80.45979781	
Slope 10-20% 0.1855	103.189589	- 1	0.5016	4.6388912	0.02			0.25	0 0	13.63816484	0000	103.189589 0.109854317	103.004089	70707000
Area 15		-		.3920092	0.02	_				43321266	0000:		27.2.30.0304	909.00 1212/
Slope 0-5% 0.9862	548.6014698	71	0.1188	0.3457401	0.02	_				1.279886552		548.6014698 0.258716126	547.6152698	
		71		1.6420015	0.02	-				0.514655687			46.36572199	
Slope 10-20% 0.3967	7 220.6755253	7 7	0.1188	4.6388912	0.02			0.25	0 0	6.907694696	0	120.6755253 0.104068837	220.2788253	0400 476540
		-		7.3920092	0.02					00/80/00	5.8118		1302.404902	2120.476319
Slope 0-5% 0.5971	332.1536581	71	0.5016	0.3457401	0.02	-	0.16			3.271859424		332.1536581 0.58821791	331.5565581	
		71		1.6420015	0.02	-				4.179428778			89.1776641	
Slope 10-20% 0.1583	88.05882445	<u> </u>	0.5016	4.6388912	0.02			0.25 (	- ;	11.6383908	100	88.05882445 0.155945227 EE 10716047 0.00760696	87.90052445	564 6770074
Area 17				7.3920692	0.02	_				.61014138	1.015.1		55.02806047	364.67 / 307
Slope 0-5% 0.6855	381.3286428	71	0.1188	0.3457401	0.02	-	0.16			0.889639253		381.3286428 0.519436236	380.6431428	
		71		1.6420015	0.02	-				0.387686739			34.92699298	
%		71		4.6388912	0.02	_		0.25 (	0 3.	3.454717993			110.1671766	
Slope >20% 0.3729	9 207.4361064	71	0.1188	7.3920692	0.02	-	0.16			10.3470167	1.3197	207.4361064 0.282564219	207.0632064	734.1202188
Area 18	233 7480609	7.	0 1188	0.3457401	000	-	910			0 5/45333937		233 7480609 0 48337743	933 3278609	
		: =		1.6420015	0.02			0.25	0	1.319614163			118.8850429	
.0		71		4.6388912	0.02	_				3.169146546			101.0606156	
Slope >20% 0.053	3 29.48273971	71	0.1188	7.3920692	0.02	1	0.16			1.470613797	0.8693	29.48273971 0.060968595	29.42973971	483.572559
Area 19	E00 606974E	7	0 5046	0.0457404						010046600		EOO EOE 274E O 74022E427	E00 600074E	
		7.7		0.345/401	0.02				0 -	5.019646623			200.6902/43	
		7.7		1.6420013	0.02		0.10			1.361663326			82 62538243	
				7.3920692	0.02			0.25		12.44194767	1.2242		58.97053504	680.9956595
		71		0.3457401	0.02	_	0.16			0.136917493			58.58184036	
		7		1.6420015	0.02	<del>.</del> .				0.127585302			11.49425683	
Slope 10-20% 0.0083		- 1	0.1188	4.6388912	0.02			0.25	0 0	0.144527013	0000	4.617108294 0.059927798	4.608808294	77 044 E 1 700
	2.225112431	-		7.3920692	0.02	_				10989721	0.1383		2.221112431	77.04451792
Slope 0-5% 0.2541	141.3502672	71	0.5016	0.3457401	0.02	_				1.392362217		141.3502672 0.634615385	141.0961672	
0		71		1.6420015	0.02	_	0.16	0.25 (	0 1	1.55622566			33.20563084	
%	(,)	71		4.6388912	0.02	_				3.970139629		30.03901782	29.98501782	
Slope >20% 0.0325	18.0790385	71	0.5016	7.3920692	0.02	-	0.16			2 807564024	644 7245912 0 4004 25 5268	10 020000 0 0000000	100101	0707000

42.30139348	39.2644735	38.43413303	38.47209846	231.0321349	8.729388317	12.99697102	31.19006987	313.4677848	48.32957597	20.74726306	19.84532382	38.10759795	3.160778214	32.5709149
15.87851343 2.24945607 4.041803419 17.18702056	34.68546314 1.692104209 0.116282043 0.037424106	17.52517408 3.356140339 5.795390088 9.082028516	33.0776722 2.852494723 0.601738115 0.49419343	57.0806215 2.829449433 30.27638923 132.1621747	0.804024545 0.816827483 4.184000338 2.59643595	3.134159372 0.486511667 1.656700256 7.231099728	9.950443889 0.540284009 4.716602584 14.81043939	70.87962874 20.54103471 64.82895995 145.4362614	30.29687393 9.801929801 4.783177865 1.631094379	7.796989614 3.648837504 5.413082445 3.108553495	12.12182228 2.545224196 2.470967152 1.961410195	16.62845667 3.495202241 11.66091649 4.89072255	0.560768711 1.8769108 0.442981676 0.161317027	20.68698821 2.867858249 4.335075014 3.456793425
17.06651343 0.403450384 2.41775607 0.057155471 4.344203419 0.102696461 18.47292056 0.436697684	37.28056314 0.949473145 1.818704209 0.046319333 0.124982043 0.003183082 0.040224106 0.00102444	18.83637408 0.490094939 3.607240339 0.093855124 6.228990088 0.162069223 9.761528516 0.253980713	34.3694722 0.893360996 2.963894723 0.077040111 0.625238115 0.016251729 0.51349343 0.013347165	59.3098215 0.256716762 2.93949433 0.012725284 31.48678923 0.136166292 137.3235747 0.594391662	0.835424545 0.09570253 0.848727483 0.097226455 4.347400338 0.498018897 2.69783595 0.309052118	3.256559372 0.250562948 0.505511667 0.038894575 1.721400256 0.132446264 7.513499728 0.578096213	10.33904389 0.331485115 0.561384009 0.017998806 4.900802584 0.157127015 15.38883339 0.493389064	73.64772874 0.234945128 21.34223471 0.06808749 67.36075995 0.21488894 151.1160614 0.482078442	31,48007393 0.65136251 10.1847298 0.21073493 4.969977865 0.10285122 1.694794379 0.035067437	8.101489614 0.39048474 3.791337504 0.182739164 5.62482445 0.271095153 3.229953495 0.155680944	12.59522228 0.63469527 2.644624196 0.133261831 2.567467152 0.129373911 2.038010195 0.102694731	17.27785667 0.453396635 3.631702241 0.095301264 12.11631649 0.31795015 5.08172255 0.133351951	0.582668711 0.184343434 1.9502108 0.617003367 0.460281676 0.145622896 0.167617027 0.053030303	21,49488821 0.659941186 2.978858249 0.091488319 4.504375014 0.138294396 3.591793425 0.110276099
		8.3532												
2.9446	2.7332	2.6754	1.446	8.6835	0.3281	0.4885	1.1723	11.7819	1.8165	0.7798	0.7459	1.4323	0.1188	1.2242
		2.367136429												
0.039816155 0.026788649 0.135984409 0.921438513	0.367229922 0.085082745 0.016518388 0.00847146	0.043945237 0.039968092 0.194982936 0.486909923	0.338554397 0.138657126 0.082635279 0.108145083	0.13836974 0.032574533 0.984738616 6.849768563	0.008229299 0.039705227 0.574578918 0.568181937	0.03207854 0.02364881 0.227510747 1.582392297	0.101844124 0.026262705 0.647719931 3.240990455	0.17182006 0.236482263 2.108559903 7.537744698	0.310092555 0.476462726 0.656862558 0.356934806	0.018900765 0.042007881 0.176060338 0.161111695	0.124068472 0.12372099 0.339332103 0.429218307	0.040309218 0.040239128 0.379270945 0.253478861	0.005739543 0.091234895 0.060833631 0.035301245	0.21173409 0.139403932 0.595325648 0.756455241
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0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.5016 0.5016 0.5016 0.5016	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.5016 0.5016 0.5016 0.5016
17 17 17 17 17 17	17 17 17	12 T T T	17 17 17	<b>222</b>	<u> </u>	F	<u> </u>	17 17 17	17 17 17 17 17	5555	17 17 17	<u> </u>	F	F
17.06651343 2.41775607 4.344203419 18.47292056	37.28056314 1.818704209 0.124982043 0.040224106	18.83637408 3.607240339 6.228990088 9.761528516	34.3694722 2.963894723 0.625238115 0.51349343	59.3098215 2.939949433 31.45878923 137.3235747	0.835424545 0.848727483 4.347400338 2.69783595	3.256559372 0.505511667 1.721400256 7.513499728	10.33904389 0.561384009 4.900802584 15.38883939	73.64772874 21.34323471 67.36075995 151.1160614	31.48007393 10.1847298 4.969977865 1.694794379	8.101489614 3.791337504 5.624482445 3.229953495	12.59522228 2.644624196 2.567467152 2.038010195	17.27785667 3.631702241 12.11631649 5.08172255	0.582668711 1.9502108 0.460281676 0.167617027	21.49488821 2.979858249 4.504375014 3.591793425
1.188 0.1683 0.3024 1.2859	2.5951 0.1266 0.0087 0.0028	1.3112 0.2511 0.4336 0.6795	1.2918 0.1114 0.0235 0.0193	2.2292 0.1105 1.1824 5.1614	0.0314 0.0319 0.1634 0.1014	0.1224 0.019 0.0647 0.2824	0.3886 0.0211 0.1842 0.5784	2.7681 0.8022 2.5318 5.6798	1.1832 0.3828 0.1868 0.0637	0.3045 0.1425 0.2114 0.1214	0.4734 0.0994 0.0965 0.0766	0.6494 0.1365 0.4554 0.191	0.0219 0.0733 0.0173 0.0063	0.8079 0.112 0.1693 0.135
Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 2 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	<b>Area 3</b> Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 4 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 5 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 6 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	<b>Area 7</b> Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	<b>Area 8</b> Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 9 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	<b>Area 10</b> Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 11 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 12 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 13 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 14 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	<b>Area 15</b> Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%
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0.6864         17.7015668         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.0450372           0.2189         5.847971844         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.0450372           0.2189         5.847971844         71         0.1188         7.3920692         0.02         1         0.16         0.25         0         0.102187813           11.1025         295.3917519         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.1340813           11.628         30.3773403         7         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.0181781           1.1628         30.3773403         7         0.1188         7.3260692         0.02         1         0.16         0.25         0         0.019186254           1.1628         30.3773403         7         0.1188         7.3260692         0.02         1         0.16         0.25         0         0.01919643           2.4006         14.602229         7         0.018         0.022		
0.1528 4.0860386227         71         0.1188 1.6420015         0.02         1         0.16         0.25         0         0.04507372           0.0219 5.24977814         71         0.1188 7.3826882         0.02         1         0.16         0.25         0         0.102187813           11.1025 2.95.3917519         71         0.1188 7.3826882         0.02         1         0.16         0.25         0         0.102187813           11.628 3.03775103         71         0.1188 1.6420015         0.02         1         0.16         0.25         0         0.102187813           1.1628 3.03775103         71         0.1188 1.6420015         0.02         1         0.16         0.25         0         0.68914562           1.1628 3.03775103         71         0.1188 1.6420015         0.02         1         0.16         0.25         0         0.68914562           1.1628 3.0377403         71         0.1188 1.6420015         0.02         1         0.16         0.25         0         0.68914124           0.4638 1.226848         71         0.5116 1.6420015         0.02         1         0.16         0.25         0         0.619095043           0.4638 1.226834         71         0.5016 1.6420015         0.02	0.25 0	75658
0.2198         5.847971814         71         0.1188         4.6388912         0.02         1         0.16         0.25         0         0.183056113           11.1025         295.3917519         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.102187813           11.1026         295.3917519         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.102187813           1.1629         3.39373402         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.689148592           1.1629         3.39373402         71         0.1188         7.320682         0.02         1         0.16         0.25         0         0.369415141           0.6172         1.64201402015         0.02         1         0.16         0.25         0         0.1995043           0.4538         1.239806386         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         0.1996415141           0.4787         1.23806382         71         0.5016         1.6420015         0.02         1 <t< td=""><td>0.25 0</td><td>38627</td></t<>	0.25 0	38627
11.1025 295.3917519 71 0.1188 0.3457401 0.02 1 0.16 0.25 0 0.0689148592 1.2694 33.77350055 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.0589148592 1.2694 33.77350055 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.0589148592 1.26173214342 71 0.1188 4.6389912 0.02 1 0.16 0.25 0 0.0589148592 1.2617221896 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.058915134 1.273623934 71 0.5016 4.6389912 0.02 1 0.16 0.25 0 0.1439974124 0.2598 14.09579375 71 0.5016 4.6389912 0.02 1 0.16 0.25 0 0.1439974124 0.2898 14.09579375 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.1439974124 0.2898 14.09579375 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.140919261 0.25 0 0.042947124 0.2898 14.09579375 71 0.5016 1.4439912 0.02 1 0.16 0.25 0 0.140919261 0.2898 14.09579375 71 0.5016 1.4439912 0.02 1 0.16 0.25 0 0.141991241 0.2898 14.09579375 71 0.5016 1.4439912 0.02 1 0.16 0.25 0 0.141991261 0.2998 14.09579375 71 0.5016 1.4439912 0.02 1 0.16 0.25 0 0.141991261 0.2998 14.0950944 17 0.5016 1.4439912 0.02 1 0.16 0.25 0 0.042947296 0.2998 14.0950944 17 0.5016 1.4439912 0.02 1 0.16 0.25 0 0.042947296 0.2998 14.095094 14	0.25 0	71814
1.1025 295.3917519 71 0.1188 0.3457401 0.02 1 0.16 0.25 0 0.689148592   1.5894 33.77350055 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.374209155   1.1628 30.3973403 77 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.058915141   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.058915141   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.058915043   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.058915043   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.169095043   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.168229214   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.168229214   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.168229214   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.106927124   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.106927125   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.106927125   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809518   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809516   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809518   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809518   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809518   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809518   0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05809518   0.1188 1.6420015 0.02 1 0.118 0.05809518   0.1188 1.6420015 0.02 1 0.118 0.05 0.05809518   0.1188 1.6420015 0.02 1 0.1480015 0.02 1 0.1480015 0.02 1 0.14	0.25 0 0.102187813	52546 29.69481957
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1.689 33.7758.0055 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.37420155 0.05 0.05 0.05 0.05 0.05 0.05 0.05	0.25 0	32519
1,1628         30,9373403         71         0,1188         4,688912         0,02         1         0,16         0,25         0         0,619096043           6,172         16,42114742         71         0,1188         7,3920692         0,02         1         0,16         0,25         0         0,619096043           5,406         14,62114742         71         0,516         0,3457401         0,02         1         0,16         0,25         0         0,619096043           0,4638         12,33990868         71         0,5016         1,4689012         0,02         1         0,16         0,25         0         0,577281641           0,4787         12,39908686         71         0,5016         1,488912         0,02         1         0,16         0,25         0         0,58298142           0,4787         14,09579375         71         0,5016         7,3820692         0,02         1         0,16         0,25         0         0,410619281           0,529         8,777278996         71         0,5016         1,6420015         0,02         1         0,16         0,25         0         0,410619281           0,0648         1,772406084         71         0,5016         4,	0.25 0	10055
5.4906         146.082295         71         0.5161         0.3457401         0.02         1         0.16         0.25         0         0.819095043           0.4638         12.33960586         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.577281641           0.4638         12.33960586         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         0.577281641           0.4787         12.7262344         0.5016         4.638912         0.02         1         0.16         0.25         0         1.68229214           0.5298         14.09573975         71         0.5016         6.458912         0.02         1         0.16         0.25         0         1.66208488           0.2298         1.777278964         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         0.16069288           0.2898         1.72406084         71         0.5016         1.4240015         0.02         1         0.16         0.25         0         0.16049288           0.648         1.724060844         71         0.516         7.3920692 <t< td=""><td>0.25 0</td><td>51403</td></t<>	0.25 0	51403
5.4906         146.0822295         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         1.438974124           0.4638         12.33990586         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         0.57281641           0.4787         12.7362344         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         1.68328814           0.5298         14.08579375         71         0.5016         7.3820892         0.02         1         0.16         0.25         0         1.68208248           0.2898         14.08579375         71         0.5016         1.4420015         0.02         1         0.16         0.25         0         1.66208248           0.2898         1.772408044         71         0.5016         1.4420015         0.02         1         0.16         0.25         0         1.0747124           0.064         1.72408044         71         0.5016         1.4420015         0.02         1         0.16         0.25         0         0.042947266           0.089         1.72408044         71         0.1188         0.345	0.25 0 0.819095043	34742 376.5237139
6.490         146,0822295         71         0,5016         0,2457401         0,02         1         0,16         0,25         0         1,43874124           0.4638         12,33990268         71         0,516         0,25         0         0,57281641         0           0.4787         12,7362343         71         0,5016         4,688917         0,02         1         0,16         0,25         0         1,57281641           0.529         14,09579375         71         0,5016         7,3920682         0,02         1         0,16         0,25         0         2,988666668           6,349         16,007727899         71         0,5016         1,4420015         0,02         1         0,16         0,25         0         0,10619261           0,329         8,77727899         71         0,5016         1,4420015         0,02         1         0,16         0,25         0         0,10619261           0,286         7,6286         7,6286         7         0,5016         1,4420015         0,02         1         0,16         0,25         0         0,10619261           0,049         1,77278699         7         0,5016         1,4642015         0,02         1		
0.4638         12.33960586         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         0.57281641           0.4787         12.7362343         71         0.5016         4.688812         0.02         1         0.16         0.25         0         1.68298214           0.5289         4.05873975         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         1.682082468           0.3299         8.777278896         71         0.5016         1.6427401         0.02         1         0.16         0.25         0         0.10619261           0.2899         8.777278896         71         0.5016         1.6327401         0.02         1         0.16         0.25         0         0.10619261           0.289         8.777278896         71         0.5016         7.3920682         0.02         1         0.16         0.25         0         0.04244734           0.0648         1.72406844         71         0.5016         7.3920682         0.02         1         0.16         0.25         0         0.04247256           0.289         6.282381447         71         0.1188         1.6420	0.25 0 1	16295
6.3419         16.73823343         71         0.5016         4,8388912         0.02         1         0.16         0.25         0         1,683298214           0.5299         14,09579375         71         0.5016         7,3820892         0.02         1         0.16         0.25         0         2,986866658           6.3419         168,7318128         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         1.662082468           0.2829         8.77775896         71         0.5016         1,642015         0.02         1         0.16         0.25         0         0.41619281           0.0849         1.724060944         71         0.5106         7.3320692         0.02         1         0.16         0.25         0         0.042947266           0.6949         1.724060944         71         0.1188         0.3457401         0.02         1         0.16         0.25         0         0.042947266           0.0234         0.62577827         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.042947266           0.0234         0.62577827         71         0.1188 <td< td=""><td>0.25 0</td><td>0586</td></td<>	0.25 0	0586
6.3419         168.7318128         71         0.5016         7.3920682         0.02         1         0.16         0.25         0         2.988666668           6.3419         168.7318128         71         0.5016         0.3457401         0.02         1         0.16         0.25         0         1.662082468           0.3299         8.777278896         71         0.5016         1.4420015         0.02         1         0.16         0.25         0         0.40619261           0.048         1.77278896         71         0.5016         7.326692         0.02         1         0.16         0.25         0         0.40619261           0.0548         1.77278896         71         0.5016         7.326692         0.02         1         0.16         0.25         0         0.40619261           0.0648         1.772406044         71         0.518         0.345701         0.02         1         0.16         0.25         0         0.404347124           0.084         1.6604         1.6604         0.02         1         0.16         0.25         0         0.04294726           0.094         2.40517301         71         0.1188         4.5388912         0.02         1	0.25 0	53343
6.3419 168.7318128 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 1.662082468 0.2299 8.777278996 71 0.5016 1.642015 0.02 1 0.16 0.25 0 0.410619261 0.02 0.2865 7.622583824 71 0.5016 4.6388912 0.02 1 0.16 0.25 0 0.047724 0.0548 1.724060944 71 0.5016 7.3920692 0.02 1 0.16 0.25 0 0.05309516 71 0.0048 1.72406094 71 0.5016 7.3920692 0.02 1 0.16 0.25 0 0.04247256 0.23 6.25281147 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.069276155 0.023 6.25281147 71 0.1188 4.6888912 0.02 1 0.16 0.25 0 0.058776894 0.0234 0.0237527 71 0.1188 4.6888912 0.02 1 0.16 0.25 0 0.03105478 1.6668 4.3333732 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.435703199 0.05 1 0.16 0.25 0 0.04307319 0.05 1 0.516 0.25 0 0.04307319 0.05 1 0.516 0.25 0 0.04307319 0.05 1 0.516 0.25 0 0.04307319 0.05 1 0.516 0.05 0 0.0587884 1 0.0516 0.0516 0.0516 0.05 0 0.051054778 1 0.0516 0.052 0 0.051054778 1 0.0516 0.052 0 0.051054778 1 0.0516 0	0.25 0 2.968666568	99375 185.2540625
6.5349 168.7318128 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 1.662082488 6.03299 8.77728895 77 0.5016 1.620765 0.02 1 0.16 0.25 0 0.416012651 6.0289 8.77728895 77 0.5016 4.6888912 0.02 1 0.16 0.25 0 0.401612651 6.0284 1.724060844 77 0.5016 7.3920692 0.02 1 0.16 0.25 0 0.0042947256 6.0295 6.28298147 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.0042947256 6.0294 0.62577527 71 0.1188 4.6888912 0.02 1 0.16 0.25 0 0.03105478 6.0294 0.62577527 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.03105478 6.0294 0.62577527 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.03105478 6.0294 0.62577527 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.03105478 6.0295 14.7881891 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 6.0294 0.62577527 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.03105478 6.0295 14.7881891 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 6.0294 0.62577527 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 6.0295 14.7881891 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 6.0297741 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 6.0297741 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 6.0297741 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 6.0297741 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478		
0.2863         7.2298         8.777278896         71         0.5016         1.6420015         0.02         1         0.16         0.25         0         0.401619261         7           0.2863         7.22283824         71         0.5016         7.3826891         0.02         1         0.16         0.25         0         1.00744724         7           0.064         1.724060844         71         0.5016         7.3826892         0.02         1         0.16         0.25         0         0.0399816         7           0.084         1.724060844         71         0.1188         0.3452015         0.02         1         0.16         0.25         0         0.043947256         7           0.0894         2.26281147         71         0.1188         1.6420015         0.02         1         0.16         0.25         0         0.03927155         7           0.0894         2.26281147         71         0.1188         4.6388912         0.02         1         0.16         0.25         0         0.03527155         1         0.188         4.6388912         0.02         1         0.16         0.25         0         0.031054478         1         1         0.04         0.04	0.25 0 1	99128
0.0848 1,724.080844 71 0,5016 4,8388912 0,02 1 0,16 0,25 0 1,007447124 0,0648 1,724080844 71 0,5016 7,3820892 0,02 1 0,16 0,25 0 0,383089316 0,0848 1,724.080844 71 0,5016 7,3820892 0,02 1 0,16 0,25 0 0,042947256 0,23 6,25281147 71 0,1188 1,6420015 0,02 1 0,16 0,25 0 0,069276155 0,0034 2,40571301 71 0,1188 4,6388912 0,02 1 0,16 0,25 0 0,069276155 0,0034 2,40571301 71 0,1188 4,6388912 0,02 1 0,16 0,25 0 0,03105478 1 1,665 44,3333732 71 0,5016 0,3457401 0,02 1 0,16 0,25 0 0,435703199 0,0677 16,1507741 71 0,716 4,5488912 0,02 1 0,16 0,25 0 0,435703199	0.25 0	78896
0.0648 1.724060844 71 0.5016 7.3920692 0.02 1 0.16 0.25 0 0.363098516 71 0.188 0.3457401 0.02 1 0.16 0.25 0 0.042947256 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.042947256 0.0235 6.252381147 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.069276155 0.0234 0.62277527 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.03105478 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.03105478 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.436703199 0.0375 14.6398189 77 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.436703199 0.057 14.6307741 71 0.5016 1.642015 0.02 1 0.16 0.25 0 0.436703199 0.057 14.6307741 71 0.5016 1.6420175 0.02 1 0.16 0.25 0 0.436703199	0.25 0 1	33824
0.6919 18.40860645 71 0.1188 0.3457401 0.02 1 0.16 0.25 0 0.042947256 0.235 6.25238147 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.05287855 0.0304 2.405171301 71 0.1188 4.6388912 0.02 1 0.16 0.25 0 0.075287864 0.0234 0.62257327 71 0.1188 7.3820892 0.02 1 0.16 0.25 0 0.03105478 1.6663 44.3333732 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.436703199 0.6552 14.7818891 71 0.5016 1.6420175 0.02 1 0.16 0.25 0 0.436703199 0.6675 16.16307741 71 0.5016 1.6420175 0.02 1 0.16 0.25 0 0.436703199	0.25 0 0.363098516	50844 186.8557363
0.68919 18.40860645 71 0.1188 0.3457401 0.02 1 0.16 0.25 0 0.042947256 0.235 6.282381147 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.058276155 0.0304 2.40517301 71 0.1188 7.3826932 0.02 1 0.16 0.25 0 0.031054478 1.6663 44.3333722 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.436703199 0.6562 14.7981891 71 0.5016 1.64208912 0.02 1 0.16 0.25 0 0.486703199 0.6562 14.7981891 71 0.5016 1.64208918 0.02 1 0.16 0.25 0 0.692289885		
0.235 6.282381147 71 0.1188 1.6420015 0.02 1 0.16 0.25 0 0.069276155 0.0304 2.40571301 71 0.1188 4.638812 0.02 1 0.16 0.25 0 0.075287884 0.0234 0.0234 0.02277527 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.031054478 1.665 44.33337322 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.435703199 0.05 0.0455703199 0.05 0.0455703199 0.05 0.0455703199 0.05 0.045703131 71 0.5016 1.642017 0.01 0.16 0.25 0 0.043570319	0.25 0	70645
0.0904 2.405/71301 71 0.1188 4.8288912 0.02 1 0.16 0.25 0 0.07587864 0.0234 0.62257527 71 0.1188 7.3920892 0.02 1 0.16 0.25 0 0.03105478 0.03105478 0.055 1 0.0016 0.25 0 0.03105478 0.055 0.055 0 0.03105478 0.055 0 0.03105478 0.055 0 0.03105478 0.055 0 0.03105478 0.055 0 0.03105478 0.055 0 0.03105478 0.055 0 0.031054	0.25 0	31147
0.0234 0.622577527 71 0.1188 7.3920692 0.02 1 0.16 0.25 0 0.031054478 1 1.6863 44.3337722 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.435703199 0.5562 14.7981891 71 0.5016 1.642015 0.02 1 0.16 0.25 0 0.692289885 0.5652 14.7981891 71 0.5016 1.642015 0.02 1 0.16 0.25 0 0.692289885 0.56716 1.642015 0.02 1 0.16 0.25 0 0.556289885 0.56716 1.642015 0.5562 0.5	0.25 0	71301
1.6663 44.33337322 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.5552 14.79818991 71 0.5016 1.6420015 0.02 1 0.16 0.25 0 0.5552 14.79818991 71 0.5016 1.6420015 0.02 1 0.16 0.25 0 0.5552 1 0.5016 0.5552 1 0.5016 0.5552 1 0.5016 0.5552 1 0.5016 0.5552 1 0.5016 0.5552 1 0.5016 0.501	0.25 0 0.031054478	77527 27.68873643
1.6663 44.33337322 71 0.5016 0.3457401 0.02 1 0.16 0.25 0 0.05 0.05 0.05 0.05 0.05 0.05 0.		
0.5562 14.79818891 71 0.5016 1.6420015 0.02 1 0.16 0.25 0 0.00 0.00 0.00 0.00 0.00 0.00 0.	0.25 0	17322
. 0.6075 16.16307041 71 0.5016 4.6388912 0.02 1 0.16 0.25 0	0.25 0	38891
2000	1 0.16 0.25 0 2.136209871 15.55557041 16.16307041 0.189411655 15.55557041	57041
Slope >20% 0.3773 10.03839748 71 0.5016 7.3920692 0.02 1 0.16 0.25 0 2.114152314 50.55723185 3.2073	0.25 0 2.114152314 50.55723185	97476 85.33303002

TOTAL 753.841 tonnes

## USLE Calculation M2PP Whole Catchment Less Project Footprint

Whareroa Wharemauku Waikanae Waimeha Ngarara Catchment 1 Catchment 2 Catchment 3 Catchment 4 Catchment 5

1600 1380 14200 120 1890 Total Catchment Area (ha)

Assumptions

R factor based on NIWA HIRDS Data

The carbon department of samples and soils (gravels to be utilised - grass cover

I.S Factor based on soil samples and soils (gravels to be utilised - grass cover

C and P Factor shased on altered stopes with a uniform 100m slope length

C and P Factors based on a pastoral surface in the pastoral surface capturing 100m slope in the activity of the comparison with earthworks scenario

Sediment Delilivery Ratio - based on a high infiltration rate and irregular surface capturing flow and sediment - 0.25 assumed figure

Efficiency - based on 0% as no control massures in place with existing situation

Assume pre earthworks surface is grass environment in all areas

Catchment Characteristics are based on project loopprint and pro rate of specific areas (soil types and slope classes)

			Total Catchment Footprint																
Pro Rata Sub Catchment Split	u r	Footprint Hectares	Area Less Project Footprint	_	*	<u>ø</u>	ပ	۵	time	sdr	sed eff.	Total Catchment Yield	Overall Catchment Yield	Area	Project Footprint Area	Pro Rata Total Catchment Area	Slope % Total Catchment	Total Catchment Less Project Footprint	Pro Rata Total Catchment Area
-	Area 1																. — .		
	Slope 0-5%	99.9	1088.374528	7	0.132	0.3457401	0.02	<del>.</del> .	0.16	0.25	0	2.821307145				1095.034528	0.74	1088.374528	
_	Slope 5-10%	4.	235.3242223	7	0.132	1.6420015	0.05	-	0.16	0.25	0	2.897093119				236.7642223	0.16	235.3242223	
	Slope 10-20%	0.54	88.24658336	71	0.132	4.6388912	0.02	<del>.</del> -	0.16	0.25	0	3.069264779		•		88.78658336	0.06	88.24658336	
_	Slope >20%	0.36	58.83105557	71	0.132	7.3920692	0.05	1	0.16	0.25	0	3.260580517		6		59.19105557	0.04	58.83105557	1479.776389
_	Area 2																		
	Slobe 0-2%	0.5122	83.70351851	71	0.5016	0.3457401	0.05	-	0.16	0.25	0	0.824516423				84.21571851	0.700492341	83.70351851	
_	Slope 5-10%	0.0592	9.67444025	F i	0.5016	1.6420015	0.02	- ,	0.16	0.25	0 (	0.452590325				9.73364025	9.73364025 0.080962801	9.67444025	
	Slope 10-20% Slope >20%	0.0596	9.739808089	F F	0.5016	7.3920692	0.02		0.16	0.25	0 0	3.448607327	18.06123202	0.7312	9.7312	9.799408089	9.799408089 0.081509847 16.4748438 0.137035011	9.739808089	120.2236107
2	Area 1																		
	Slope 0-5%	4.426	188.4887369	71	0.132	0.3457401	0.02	-	0.16	0.25	0	0.488604434				192.9147369	92.9147369 0.471121708	188.4887369	
	Slope 5-10%	0.689	29.34223673	71	0.132	1.6420015	0.05	-	0.16	0.25	0	0.361234349				30.03123673	30.03123673 0.073340004	29.34223673	
	Slope 10-20%	1.5453	65.80922847	71	0.132	4.6388912	0.05	-	0.16	0.25	0	2.288881217				67.35452847	0.16448811	65.80922847	
	Slope >20%	2.7361	116.5214716	71	0.132	7.3920692	0.05	1	0.16	0.25	0	6.457943621		9.3964		119.2575716 0.291241777	0.291241777	116.5214716	409.4796176
	Area 2																		
	Slobe 0-5%	0.5863	24.96368721	71	0.1188	0.3457401	0.05	-	0.16	0.25	0	0.058240251				25.54998721	0.188387636	24.96368721	
	Slope 5-10%	0.2276	9.690832695	71	0.1188	1.6420015	0.05	-	0.16	0.25	0	0.107374073				9.918432695	9.918432695 0.073131547	9.690832695	
	Slope 10-20%	0.4838	20.59940623	71	0.1188	4.6388912	0.02	-	0.16	0.25	0	0.644812826				21.08320623	0.155452734	20.59940623	
_	Slope >20%	1.8145	77.25841795	71	0.1188	7.3920692	0.05	1	0.16	0.25	0	3.853688514		3.1122		79.07291795	79.07291795 0.583028083	77.25841795	135.6245441
	Area 3																		
	Slobe 0-2%	2.8566	121.6293176	71	0.1188	0.3457401	0.05	-	0.16	0.25	0	0.283761048				124.4859176	124.4859176 0.90338699	121.6293176	
	Slope 5-10%	0.0312	1.328444552	71	0.1188	1.6420015	0.05	-	0.16	0.25	0	0.014719117				1.359644552 0.009866861	0.009866861	1.328444552	
	Slope 10-20%	0.1189	5.062565938	Ε :	0.1188	4.6388912	0.02		0.16	0.25	0 (	0.158470949				5.181465938	5.181465938 0.037601594	5.062565938	
	Slope >20%	0.1554	6.6166/5/51	1	0.1188	7.3920692	0.05	-	0.16	0.25	0	0.330043095		3.1621		6.7/20/5/51	0.049144556	6.6166/5/51	137.7991038
	Area 4			i			;	,		;	,						0	1	
	Slope 0-5%	10/8/0	15.75824772	7 7	0.1188	0.345/401	0.02	- •	0.16	0.20	<b>&gt;</b> 0	0.036/639/2				16.12834772 0.547890452	6.12834772 0.547890452	15./5824//2	
	Slope 10-20%	0.0002	1 46043744	7 7	0.1188	1.6420013	20.0		0.10	0.20	o c	0.002924933				1 49473744	1 49473744 0 050777202	1 46043744	
	Slope >20%	0,2649	11.27900519		0.1188	7.3920692	0.02		0.16	0.25	0	0.562602418		0.6755		11.54390519	0.39215396	11.27900519	29,43717612
	Area 5																		
	Slope 0-5%	0.0402	1.711649712	71	0.1188	0.3457401	0.02	-	0.16	0.25	0	0.003993277				1.751849712	1.751849712 0.128025478	1.711649712	
	Slope 5-10%	0.0066	0.281017117	71	0.1188	1.6420015	0.02	-	0.16	0.25	0	0.003113659				0.287617117 0.021019108	0.021019108	0.281017117	
	Slope 10-20%	0.0646	2.750561477	71	0.1188	4.6388912	0.02	-	0.16	0.25	0	0.086099439				2.815161477	2.815161477 0.205732484	2.750561477	
_	Slope >20%	0.2026	8.626373919	71	0.1188	7.3920692	0.05	1	0.16	0.25	0	0.430287844		0.314		8.828973919 0.64522293	0.64522293	8.626373919	13.68360222
	Area 6																		
	Slope 0-5%	0.1491	6.348432139	71	0.1188	0.3457401	0.02	-	0.16	0.25	0	0.014810884				6.497532139	5.497532139 0.203105844	6.348432139	
_	Slope 5-10%	0.323	13.75280738	71	0.1188	1.6420015	0.05	-	0.16	0.25	0	0.152380605				14.07580738 0.439994551	0.439994551	13.75280738	
	Slope 10-20%	0.1127	4.798580161	71	0.1188	4.6388912	0.05	-	0.16	0.25	0	0.150207535				4.911280161	0.153521319	4.798580161	
	Slope >20%	0.1493	6.356947809	71	0.1188	7.3920692	0.05	1	0.16	0.25	0	0.317087735		0.7341		6.506247809	6.506247809 0.203378286	6.356947809	31.99086749

1052	128	536	324	998	1987	441	836	137	129	544	422	178	7651	
43.53913052	107.9087128	69.41595536	47.37838324	43.48247866	112.4059987	33.02367441	145.0461836	19.78457137	2063.291129	513.1665544	352.1240422	83.55297178	531.5793597	
12.63299675 3.061383439 10.32950796 16.51614237	47.64517481 15.81359957 24.21430823 17.75943022	28.82980148 6.024836671 13.16948397 19.79893323	30.36262212 2.490833535 6.501714203 6.936013383	21.85972542 3.099703955 11.14275447 6.38249482	34.60768372 14.73210946 14.77042997 45.7163755	16.98450423 7.770549064 3.427557258 4.083263864	12.19443974 4.083263864 14.32335729 11.1167227	15.60070782 0 0.510940212 3.218923338	937.5315571 175.1347152 329.7796682 617.1360889	114.6094014 33.64985333 107.2242026 256.760597	69.63187471 16.65834323 67.35523447 197.8455898	12.54928523 0 10.77239529 60.08109125	212.8380987 81.01507592 104.3922843 132.3783009	65.24517766 10.27264499 111.0556215
12.92969675 0.296967271 3.133283439 0.071964768 10.57210796 0.242818537 16.90404237 0.388249424	48.76417481 0.451902108 16.18499957 0.149987885 24.78300823 0.229666424 18.17653022 0.168443583	29.50690148 0.425073765 6.166336671 0.088831691 13.47878397 0.194174148 20.26393323 0.291920397	31.07572212 0.655905077 2.54933535 0.053807947 6.654414203 0.140452539 7.098913383 0.149834437	22.37312542 0.51453197 3.172503955 0.072960513 11.40445447 0.262277009 6.53239482 0.150230507	35.42048372 0.315112042 15.07810946 0.134139722 15.11732997 0.134488641 46.7900755 0.416259595	17.38340423 0.526392188 7.953049064 0.240828715 3.508057258 0.106228556 4.179163864 0.126550541	12.48083974 0.08604735 4.179163864 0.028812643 14.65975729 0.101069583 113.7264227 0.784070424	15.96710782 0.807048458 0 0 0.522940212 0.026431718 3.294523338 0.166519824	939.2199571 0.455204767 175.4501152 0.085034105 330.3735682 0.160119706 618.2474889 0.299641422	114.8158014 0.223739837 33.71045333 0.065691057 107.4173026 0.209322493 257.222997 0.501246612	59.75727471 0.198104265 16.68834323 0.047393365 57.47653447 0.191627172 198.2018898 0.562875197	12.57188523 0.150466045 0 0 10.79179529 0.129161119 60.18929125 0.720372836	213.2213987 0.401109251 81.16097592 0.152678945 104.5802843 0.196735036 132.6167009 0.249476769	65.36267766 0.142182962 10.29114499 0.022386254 111.2556215 0.242013553
12.929 3.1332 10.572 16.904	48.764 16.184 24.783 18.176	29.50690148 6.166336671 13.47878397 20.26393323	31.075 2.5493 6.6544 7.0989	22.373 3.1725 11.404 6.532	35.420 15.078 15.117 46.79	17.38340423 7.953049064 3.508057258 4.179163864	12.48083974 4.179163864 14.65975729 113.7264227	15.967 0.5229 3.2945	939.21 175.45 330.37 618.24	33.710 107.41 257.2	69.75727471 16.68834323 67.47653447 198.2018898	12.571	213.22 81.160 104.58 132.61	65.362 10.291 111.25
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0.9991	2.4762	1.5929	1.0872	0.9978	2.5794	0.7578	3.3284	0.454	3.7091	0.9225	0.633	0.1502	0.9556	
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0.029472766 0.033920017 0.323339379 0.823833439	0.111156134 0.175214107 0.757968281 0.885849258	0.067259891 0.066754971 0.412237716 0.987580688	0.07083596 0.027598345 0.203519881 0.345971815	0.215327897 0.145010562 1.472694325 1.344195249	0.080739683 0.163231236 0.462351322 2.280355667	0.167304827 0.363522357 0.453006852 0.859962137	0.028449613 0.045242415 0.448356831 5.542557683	0.153673824 0 0.067528972 0.677926356	9.23509763 8.193164217 43.58569036 129.9729059	0.267383592 0.372839149 3.356385147 12.80734695	0.162451078 0.184573836 2.108386941 9.868636934	0.029277467 0 0.337202858 2.99687487	0.496551021 0.897644089 3.267739035 6.603095833	0.152216919 0.113820532 3.476318122
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0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16	0.16 0.16 0.16	0.16 0.16 0.16
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0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912
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12.63299675 3.061383439 10.32950796 16.51614237	47.64517481 15.81359957 24.21430823 17.75943022	28.82980148 6.024836671 13.16948397 19.79893323	30.36262212 2.490833535 6.501714203 6.936013383	21.85972542 3.099703955 11.14275447 6.38249482	34.60768372 14.73210946 14.77042997 45.7163755	16.98450423 7.770549064 3.427557258 4.083263864	12.19443974 4.083263864 14.32335729 111.1167227	15.60070782 0 0.510940212 3.218923338	937.5315571 175.1347152 329.7796682 617.1360889	114.6094014 33.64985333 107.2242026 256.760597	69.63187471 16.65834323 67.35523447 197.8455898	12.54928523 0 10.77239529 60.08109125	212.8380987 81.01507592 104.3922843 132.3783009	65.24517766 10.27264499 111.0556215
0.2967 0.0719 0.2426 0.3879	0.3714 0.5687 0.4171	0.6771 0.1415 0.3093 0.465	0.7131 3 0.0585 3 0.1527 0	0.5134 0.0728 0.2617 0.1499	0.8128 0.346 0.3469 1.0737	0.3989 0.1825 0.0805 0.0959	0.2864 0.0959 0.3364 2.6097	0.3664 0 0.012 0.0756	1.6884 0.3154 0.5939 1.1114	0.2064 0.0606 0.1931 0.4624	0.1254 0.03 0.1213 0.3563	0.0226 0 0.0194 0.1082	0.3833 0.1459 0.188 0.2384	0.1175 0.0185 0.2
Area 7 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 8 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 9 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 10 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	<b>Area 11</b> Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 12 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 13 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 14 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 15 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 1 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 2 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 3 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 4 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 5 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 6 Slope 0-5% Slope 5-10% Slope 10-20%

459 7082282		179.0102951			1648.863939			700,000,000	220.2861307			875.1367191			171.8899353			27,070	1034.670176			223.5681715			939.3312127				2120.476519			564.6779071			734.1202188			483 572559				680.9956595			77.04451792		
272 308384	75.40676703	2.110056809 20.65634561 80.51532562	7407700	634.7493793 176.1897436	302.9042078 332.0563084	24 76600400	0.055527811	53.75092083	144.3167802	440.168956	52.36272556 159.8090394	221.2227981	75 7954617	3.831418943	34.42724268 57.52681196	202 565 4537	97.67341915	287.0787817	405.0504211	22.65534679	86.73444042	94.45280612	481.8703419	80.45979781	103.004089 272.308384		547.6152698	220.2788253	1302.404802	331.5565581	89.1776641	55.02806047	380 6431428	34.92699298	110.1671766 207.0632064	233.3278609	118.8850429	101.0606156		508.6902/45 29.48526752	82.62538243	58.97053504	58.58184036	11.49425683	4.606606294 2.221112431	141 0961672	33.20563084
272 798 784 0 5934 17231	75.54256703 0.422001243	2.113856809 0.011808577 20.69354561 0.115599751 80.66032562 0.450590429	0		303.4497078 0.184035626 332.6543084 0.201747579	000000000000000000000000000000000000000				_	52.45/02556 0.05994152 160.0968394 0.182939232		75 9319617 0 441747573		34.48924268 0.200647249 57.63041196 0.335275081	000 0000 507 0 100074604			466.4346211 0.442223603		19.33647613 0.066366704 86.89064042 0.388653894		482.7381419 0.513916854		103.189589 0.109854317 272.798784 0.290418098		548.6014698 0.258716126		1304.750302 0.61530995	332.1536581 0.58821791			381 3286428 - 0 519436236		110.3655766 0.150337198 207.4361064 0.282564219		_	101.2426156 0.209363856 29 48273971 0.060968595		509.6063745 0.748325437 29.53836752 0.043375265		59.07673504 0.086750531		11.51495683 0.149458484	4.617108234 0.0339 <i>277</i> 38 2.225112431 0.028880866	141 3502672 D 634615385	
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7 3920692	0.3457401	1.6420015 4.6388912 7.3920692		1.6420015	4.6388912 7.3920692	0.0457404	1.6420015	4.6388912	7.3920692	0.3457401	1.6420015	7.3920692	0.3457401	1.6420015	4.6388912 7.3920692	0.2457404	1.6420015	4.6388912	7.3920092	0.3457401	4.6388912	7.3920692	0.3457401	1.6420015	4.6388912 7.3920692		0.3457401	4.6388912	7.3920692	0.3457401	1.6420015	7.3920692	0.3457401	1.6420015	4.6388912	0.3457401	1.6420015	4.6388912		0.345/401	4.6388912	7.3920692	0.3457401	1.6420015	4.6388912 7.3920692	0.3457401	1.6420015
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272 308384	75.40676703	2.110056809 20.65634561 80.51532562	00000	834.7495793 176.1897436	302.9042078	2000000	21.76690182 0.055527811	53.75092083	144.316/802	440.168956	52.36272556	221.2227981	75 7954617	3.831418943	34.42724268	200 555 4527	97.67341915	287.0787817	465.6562211	22.65534679	19.32367613	94.45280612	481.8703419	80.45979781	103.004089 272.308384		547.6152698	220.2788253	1302.404802	331.5565581	89.1776641	55.02806047	380 6431428	34.92699298	110.1671766	233.3278609	118.8850429	101.0606156		508.6902/45	82.62538243	58.97053504	58.58184036	11.49425683	4.608808294 2.221112431	41 0961672	33.20563084
0 4904		0.0038 200.0372 200.0372 2		0.3173			0.0001		0.2599		0.0943 5		0 1365		0.062 3	0 26.40			0.8380 4		0.1562 8		0.8678 4	ω	0.1855		0.9862 5		2.3455 1	0.5971 3			0.6855		0.3729 2			0.182 1				0.1062 5		0.0207		0.2541 1	
Slope 20%	Area 7 Slope 0-5%	Slope 5-10% Slope 10-20% Slope >20%	Area 8	Slope 5-10%	Slope 10-20% Slope >20%	Area 9	Slope 0-5% Slope 5-10%	Slope 10-20%	Slope >20% Area 10	Slope 0-5%	Slope 5-10% Slope 10-20%	Slope >20%	Area 11 Slope 0-5%	Slope 5-10%	Slope 10-20% Slope >20%	Area 12	Slope 5-10%	Slope 10-20%	Area 13	Slope 0-5%	Slope 10-20%	Slope >20%	Area 14 Slope 0-5%	Slope 5-10%	Slope 10-20% Slope >20%	Area 15	Slope 0-5%	Slope 10-20%	Slope >20%	Slope 0-5%	Slope 5-10%	Slope >20%	Area 17 Slone 0-5%	Slope 5-10%	Slope 10-20% Slope >20%	Area 18 Slope 0-5%	Slope 5-10%	Slope 10-20%	Area 19	Slope 0-5%	Slope 10-20%	Slope >20%	Area 20 Slope 0-5%	Slope 5-10%	Slope 10-20% Slope >20%	Area 21 Slone 0-5%	Slope 5-10%

	85 <u>222.7337343</u> 43 07 19 42.30139348	14 09 43 06 39.2644735	08 39 88 16 38.43413303	22 23 15 43 38.47209846	15 33 23 47 231.0321349	45 83 38 95 8.729388317	72 67 56 28 12.99697102	89 09 84 39 31.19006987	74 71 95 14 313.4677848	93 01 65 79 48.32957597	14 04 45 95 20.74726306	80	96 52 19.84532382			
0	15.87851343 2.24945607 4.041803419 17.18702056	34.68546314 1.692104209 0.116282043 0.037424106	17.52517408 3.356140339 5.795390088 9.082028516	33.0776722 2.852494723 0.601738115 0.49419343	57.0806215 2.82949433 30.27638923 132.1621747	0.804024545 0.816827483 4.184000338 2.59643595	3.134159372 0.486511667 1.656700256 7.231099728	9.950443889 0.540284009 4.716602584 14.81043939	70.87962874 20.54103471 64.82895995 145.4362614	30.29687393 9.801929801 4.783177865 1.631094379	7.796989614 3.64837504 5.413082445 3.108553495	12.12182228 2.545224196 2.470967152		16.62845667 3.495202241 11.66091649 4.890722555	16.62845667 3.495202241 11.66091649 4.89072255	16.62845667 3.495202241 11.66091649 4.89072255 0.560768711 1.8769108
30.03901782 0.134865135	17.06651343 0.403450384 2.41775607 0.057156471 4.34203419 0.102696461 18.47292056 0.436697684	37.28056314 0.949473145 1.818704209 0.046319333 0.124982043 0.003183082 0.040224106 0.00102444	18.83637408 0.490094939 3.607240339 0.093855124 6.228990088 0.162069223 9.761528516 0.253980713	34,3694722 0.893360996 2.963894723 0.077040111 0.62528115 0.016251729 0.51349343 0.013347165	59.3098215 0.256716762 2.939949433 0.012725284 31.45878923 0.136166292 137.3235747 0.594391662	0.835424545 0.09570253 0.848727483 0.097226455 4.347400338 0.498018897 2.69783595 0.309052118	3.256559372 0.250562948 0.505511667 0.038894575 1.721400256 0.132446264 7.513499728 0.578096213	10.33904389 0.331485115 0.561384009 0.017998806 4.900802584 0.157127015 15.38883939 0.493389064	73.64772874 0.234945128 21.34323471 0.06808749 67.36075995 0.21488894 151.1160614 0.482078442	31.48007393 0.65136251 10.1847298 0.21073493 4.969977865 0.102835122 1.694794379 0.035067437	8.101489614 0.39048474 3.791337504 0.182733164 5.624462445 0.271095153 3.229953495 0.155680944	12.59522228 0.634669527 2.644624196 0.133261831 2.567467152 0.129373911 2.038010195 0.102694731				
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	0.4004 0.4004 2.9446	2.7332	2.202360062 2.6754	1.446	8.6835	0.3281	0.4885	1.1723	11.7819	1.8165	0.7798	0.7459		1 4323	1.4323	1.4323
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3.96300266	0.037044552 0.024923891 0.126518534 0.857297178	0.341667047 0.079160135 0.015368543 0.007881762	0.040886209 0.037185913 0.181410174 0.453016123	0.3258296 0.133445603 0.079529376 0.104080376	0.133169019 0.031350197 0.947726545 6.592315351	0.007919995 0.038212879 0.552982979 0.546826432	0.030872846 0.022760022 0.2189596 1.522917006	0.098016243 0.025275603 0.623374937 3.119175623	0.165362086 0.227593916 2.029308244 7.254433434	0.298437516 0.45855455 0.632173932 0.343519169	0.018190367 0.040428987 0.16944299 0.155056202	0.119405274 0.119070852 0.326578075 0.413085845		0.038794169 0.038726713 0.365015789	0.038794169 0.038726713 0.365015789 0.243951686	0.038794169 0.038726713 0.055015789 0.243951686 0.005523818 0.087805769 0.058547157
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0.25	0.25 0.25 0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25	0.25		0.25	0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25 0.25 0.25
0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16	0.16 0.16 0.16 0.16		0.16 0.16 0.16 0.16	0.16 0.16 0.16 31.0	0.16 0.16 0.16 0.16 0.16 0.16
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0.02	0.02 0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02	0.02		0.02	0.02 0.02 0.02 0.02	0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02
-	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692	0.3457401 1.6420015 4.6388912 7.3920692				
0.5016	0.1188 0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.5016 0.5016 0.5016 0.5016	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016	0.1188 0.1188 0.1188	0.5016 0.5016 0.5016 0.5016		0.1188 0.1188 0.1188	0.1188 0.1188 0.1188 0.1188	0.1188 0.1188 0.1188 0.5016 0.5016
77	<u> </u>	17 17 17	17 17 17	17 17 17	12 12 12	<u> </u>	F	<u> </u>	<u> </u>	17 17 17	<u> </u>	£		2222		12 12 12 12 12 12 12 12 12 12 12 12 12 1
29.98501782	15.87851343 2.24945607 4.041803419 17.18702056	34.68546314 1.692104209 0.116282043 0.037424106	17.52517408 3.356140339 5.795390088 9.082028516	33.0776722 2.852494723 0.601738115 0.49419343	57.0806215 2.829449433 30.27638923 132.1621747	0.804024545 0.816827483 4.184000338 2.59643595	3.134159372 0.486511667 1.656700256 7.231099728	9.950443889 0.540284009 4.716602584 14.81043939	70.87962874 20.54103471 64.82895995 145.4362614	30.29687393 9.801929801 4.783177865 1.631094379	7.796989614 3.648837504 5.413082445 3.108553495	12.12182228 2.545224196 2.470967152 1.961410195	00:0::	16.62845667 3.495202241 11.66091649 4.89072255	16.62845667 3.495202241 11.66091649 4.89072255	16.62845667 3.495202241 11.66091649 4.89072255 0.560768711 1.8769108 0.442981676
0.054	1.188 0.1683 0.3024 1.2859	2.5951 0.1266 0.0087 0.0028	1.3112 0.2511 0.4336 0.6795	1.2918 0.1114 0.0235 0.0193	2.2292 0.1105 1.1824 5.1614	0.0314 0.0319 0.1634 0.1014	0.1224 0.019 0.0647 0.2824	0.3886 0.0211 0.1842 0.5784	2.7681 0.8022 2.5318 5.6798	1.1832 0.3828 0.1868 0.0637	0.3045 0.1425 0.2114 0.1214	0.4734 0.0994 0.0965 0.0766		0.6494 0.1365 0.4554	0.6494 0.1365 0.4554 0.191	0.6494 0.1365 0.4554 0.191 0.0219 0.0733
Slope 10-20%	Slope >20%  Area 1  Slope 0.5%  Slope 10.20%  Slope >20%	Area 2 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 3 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 4 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 5 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 6 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 7 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 8 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 9 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 10 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 11 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%	Area 12 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20%		Area 13 Slope 0-5% Slope 5-10% Slope 10-20% Slope 3-20%	Area 13 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20% Area 14	Area 13 Slope 0-5% Slope 5-10% Slope 10-20% Slope >20% Area 14 Slope 0-5% Slope 5-10% Slope 10-20%
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Slope 5-10%	0.112	2.867858249	7	0.5016	1.6420015	0.05	-	0.16	0.25	0	0.134164341			2.979858249 0.091488319	2.867858249	
Slope 10-20%	0.1693	4.335075014	71	0.5016	4.6388912	0.05	-	0.16	0.25	0	0.572949928			4.504375014 0.138294396	4.335075014	
Slope >20%	0.135	3.456793425	71	0.5016	7.3920692	0.02	-	0.16	0.25	0	0.728023356	-	1.2242	3.591793425 0.110276099	3.456793425	32.5709149
Area 16																
Slope 0-5%	0.6664	17.06375658	71	0.1188	0.3457401	0.05	-	0.16	0.25	0	0.039809723			17.73015658 0.597079115	17.06375658	
Slope 5-10%	0.1529	3.915138627	71	0.1188	1.6420015	0.05	-	0.16	0.25	0	0.043379593			4.068038627 0.136994893	3.915138627	
Slope 10-20%	0.2198	5.628171814	71	0.1188	4.6388912	0.05	-	0.16	0.25	0	0.176175824			5.847971814 0.196935758	5.628171814	
Slope >20%	0.077	1.971652546	71	0.1188	7.3920692	0.05	-	0.16	0.25	0	0.098347015		1.1161	2.048652546 0.068990234	1.971652546	29.69481957
Area 17																
Slope 0-5%	11.1025	284.2892519	71	0.1188	0.3457401	0.05	-	0.16	0.25	0	0.663246474			295.3917519 0.784523633	284.2892519	
Slope 5-10%	1.2694	32.50410055	71	0.1188	1.6420015	0.05	-	0.16	0.25	0	0.36014425			33.77350055 0.089698203	32.50410055	
Slope 10-20%	1.1628	29.77451403	71	0.1188	4.6388912	0.05	-	0.16	0.25	0	0.932016599			30.93731403 0.082165646	29.77451403	
Slope >20%	0.6172	15.80394742	71	0.1188	7.3920692	0.05	-	0.16	0.25	0	0.788308799		14.1519	16.42114742 0.043612518	15.80394742	376.5237139
Area 18																
Slope 0-5%	5.4906	140.5916295	71	0.5016	0.3457401	0.05	-	0.16	0.25	0	1.384889302			146.0822295 0.788550748	140.5916295	
Slope 5-10%	0.4638	11.87600586	71	0.5016	1.6420015	0.05	-	0.16	0.25	0	0.555584118			12.33980586 0.066610177	11.87600586	
Slope 10-20%	0.4787	12.25753343	71	0.5016	4.6388912	0.05	-	0.16	0.25	0	1.620030305			12.73623343 0.06875009	12.25753343	
Slope >20%	0.5298	13.56599375	71	0.5016	7.3920692	0.05	-	0.16	0.25	0	2.857087215		6.9629	14.09579375 0.076088986	13.56599375	185.2540625
Area 19																
Slope 0-5%	6.3419	162.3899128	71	0.5016	0.3457401	0.05	-	0.16	0.25	0	1.599611967			168.7318128 0.903005795	162.3899128	
Slope 5-10%	0.3299	8.447378896	71	0.5016	1.6420015	0.05	-	0.16	0.25	0	0.395185857			8.777278896 0.046973559	8.447378896	
Slope 10-20%	0.2865	7.336083824	71	0.5016	4.6388912	0.05	-	0.16	0.25	0	0.969581538			7.622583824 0.040793951	7.336083824	
Slope >20%	0.0648	1.659260844	71	0.5016	7.3920692	0.05	1	0.16	0.25	0	0.349451211	7.	7.0231	1.724060844 0.009226695	1.659260844	186.8557363
Area 20																
Slope 0-5%	0.6919	17.71670645	71	0.1188	0.3457401	0.05	-	0.16	0.25	0	0.041333054			18.40860645 0.664840972	17.71670645	
Slope 5-10%	0.235	6.017381147	71	0.1188	1.6420015	0.05	-	0.16	0.25	0	0.066672364			6.252381147 0.225809551	6.017381147	
Slope 10-20%	0.0904	2.314771301	71	0.1188	4.6388912	0.05	-	0.16	0.25	0	0.072458119			2.405171301 0.08686461	2.314771301	
Slope >20%	0.0234	0.599177527	71	0.1188	7.3920692	0.05	-	0.16	0.25	0	0.029887275	_	1.0407	0.622577527 0.022484866	0.599177527	27.68873643
Area 21																
Slope 0-5%	1.6663	42.66707322	71	0.5016	0.3457401	0.05	-	0.16	0.25	0	0.420289412			44.33337322 0.519533564	42.66707322	
Slope 5-10%	0.5562	14.24198891	71	0.5016	1.6420015	0.05	-	0.16	0.25	0	0.666269699			14.79818891 0.173416893	14.24198891	
Slope 10-20%	0.6075	15.55557041	71	0.5016	4.6388912	0.05	-	0.16	0.25	0	2.055918969			16.16307041 0.189411655	15.55557041	
Slope >20%	0.3773	9.661097476	71	0.5016	7.3920692	0.05	1	0.16	0.25	0	2.034690461	48.65700388 3.	3.2073 63.5198	10.03839748 0.117637889	9.661097476	85.33303002

138.7981 Total Area (ha)